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RESEARCH MEMORANDUM

FORCE AND PRESSURE-DISTRIBUTION INVESTIGATION TO HIGH
ANGLES OF ATTACK ON ALL-MOVABLE TRIANGULAR AND
RECTANGULAR WINGS IN COMBINATION WITH A
BODY AT SUPERSONIC SPEEDS

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Approved by NASA CCO #62 Date 6-29-66
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July 10, 1956

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SUMMARY

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b7j*

In order to provide high-incidence data for all-movable triangular and rectangular wings and a body in combination, forces, moments, and load distributions were measured to combined body angles of attack and wing deflection of $\pm 45^\circ$ at a Mach number of 3.36. The ranges of aspect ratios were, for the triangular wings, $3/8$ to 4 , and, for the rectangular wings, 1 to 3. Additional measurements giving over-all combination aerodynamic coefficients were made on two smaller scale wing-body combinations at Mach numbers of 3.36, 2.44, and 1.98.

The investigation showed that the mutual interference effects of body and wing could be satisfactorily calculated in the body angle-of-attack range from at least 0° to 6° and in the wing deflection range from 0° to 10° . Nonlinear effects precluded the satisfactory application of theoretical methods of predicting force and moment coefficients at higher incidences. These effects were due to a decrease in the effect of body upwash on wing lift with an increase in angle of attack above 10° , and to an increasingly nonplanar geometrical relationship of the wing and body with increasing wing deflection angle, thus departing from the simplified planar model on which the theory was based.

INTRODUCTION

Adequate maneuverability at ever-increasing altitudes requires missiles and interceptor aircraft to operate through large ranges of angles of attack and control deflection. Since supersonic aircraft at high angles of attack can encounter highly nonlinear aerodynamic forces, experimental investigation of body-wing configurations at high incidence and at supersonic speeds is needed in order to provide useful design data and to aid in the development of applicable high-angle theories. Some high-incidence

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data on body-wing combinations at supersonic speeds are available (e.g., refs. 1 to 4), however, detailed data in the form of forces, moments, and load distributions are limited.

A program was undertaken at the Ames 1- by 3-foot wind tunnels to provide some experimental data on the aerodynamic characteristics of wings and of all-movable wing-body combinations at high angles of attack. References 5, 6, and 7 report results of force and pressure-distribution measurements on semispan wings of triangular and rectangular plan form, tested to high angles of attack in the Mach number range 1.45 to 3.36. The investigation reported herein gives the results of tests at a Mach number of 3.36 of configurations using a selection of these wings as all-movable controls in combination with a body. The tests extended over the combined angle-of-attack and wing-deflection range of 0° to $\pm 45^\circ$. The data obtained consisted of forces and moments on the body and on all of the wings. Load distributions were obtained on the body and on the wings previously employed in the investigation of reference 7. Smaller scale full-span models of two of the semispan configurations were tested to high incidences at Mach numbers of 1.98, 2.44, and 3.36 in order to indicate the effects of Mach number.

Limited comparisons of experimental force and moment coefficients with calculated values based on linear theory were made to establish the range of angles of attack and wing deflection wherein theoretical values are in satisfactory agreement with those of experiment. Factors contributing to nonlinear force and moment coefficients at higher incidences are indicated.

SYMBOLS

A aspect ratio of the exposed wing panels joined together

c local chord, in.

$$c_n \quad \text{local normal-force coefficient,} \quad \begin{cases} c_{nB}(W) = \frac{2}{D} \int_0^{\pi} P r \cos \theta \, d\theta \\ c_{nW(B)} = \int_0^1 (P_l - P_u) d(x/c) \end{cases}$$

c_r root chord at wing-body juncture, in.

\bar{c} mean aerodynamic chord of exposed wing panels, in.

$\frac{cc_n}{\bar{c}}$ span loading coefficient

C_b	bending-moment coefficient about wing root chord, <u>bending moment</u> $q_{\infty} S_w \bar{c}$
C_h	hinge-moment coefficient, <u>hinge moment</u> $q_{\infty} S_w \bar{c}$
C_m	pitching-moment coefficient about wing hinge line, <u>pitching moment</u> $q_{\infty} S_w \bar{c}$
C_D	drag coefficient, <u>drag</u> $q_{\infty} S_w$
C_L^*	component of normal-force coefficient normal to free-stream direction, $C_N \cos(\alpha_B + \delta_w)$
C_N	normal-force coefficient, <u>normal force</u> , $C_{Nw}(B)$ normal to wing chord; $\Delta C_{Nb}(W)$, C_{NbW} , and C_{Nb} normal to body axis
D	body diameter, in.
$k_B(W)$	ratio of interference lift of body in presence of wing to that of wing alone, δ_w variable, $\alpha_B = 0^\circ$
$k_W(B)$	ratio of lift of wing in presence of body to that of wing alone, δ_w variable, $\alpha_B = 0^\circ$
$K_B(W)$	ratio of interference lift of body in presence of wing to that of wing alone, α_B variable, $\delta_w = 0^\circ$
$K_W(B)$	ratio of lift of wing in presence of body to that of wing alone, α_B variable, $\delta_w = 0^\circ$
M	Mach number
p	orifice pressure
p_{∞}	free-stream static pressure
P	pressure coefficient, $\frac{p - p_{\infty}}{q_{\infty}}$
q_{∞}	free-stream dynamic pressure
r	body radius, in.

R	Reynolds number
s	combination semispan, measured from axis of body, in.
s_w	wing semispan measured from wing-body juncture, in.
S_B	body frontal area, sq in.
S_W	area of exposed wing panel, sq in.
t	local thickness of wing section
x	chordwise distance from leading edge of wing at spanwise distance y or distance along body from nose tip, in.
\bar{x}_{cr}	linear-theory distance to center of pressure from leading edge of wing-body juncture, root chords
y	spanwise distance from wing-body juncture, in.
β	$\sqrt{M^2 - 1}$
α_B	angle of attack of body with respect to free stream, deg
α_W	angle of attack of wing with respect to free stream, $\alpha_W = \alpha_B + \delta_W$, deg
δ_W	deflection angle of wing with respect to body, deg
θ	azimuthal location of body pressure orifices measured from meridional plane, deg
$\Delta(\)_{B(W)}$	body interference coefficient, $(\)_{B(W)} - (\)_B$

Subscripts

h	hinge line
l	lower surface
u	upper surface
B	body alone
B(W)	body in the presence of a wing
BW	body-wing combination, $B(W) + W(B)$

W wing alone

W(B) wing in the presence of the body

APPARATUS

Tunnel

The investigation was conducted in the Ames 1- by 3-foot supersonic wind tunnel No. 2. This nonreturn, intermittent-operation, variable-pressure wind tunnel has a Mach number range of 1.4 to 3.8. The Mach number can be changed by varying the contour of flexible steel plates which form the upper and lower walls of the nozzle.

Models

Semispan wings.- The semispan wings of the present investigation were selected from models previously employed in the wing-alone tests of references 5, 6, and 7. The geometry of these wings is summarized in figure 1(a). Three of the wings of this figure were fitted with pressure orifices. The wings, in vertical streamwise planes, had modified biconvex sections with trailing edges blunted to a height one-half the maximum thickness. The wings fitted with pressure orifices had maximum thickness ratios of 5 percent at the 50-percent-chord line and the remaining wings had maximum thickness ratios of 4 percent at the 59-percent-chord line. At the root, the wings were provided with an integral shaft, the axis of which was the hinge line. All of the wings, with the exception of the triangular wing of aspect ratio 3/8, had filleted root sections (see sketch in fig. 1(a)). The pressure orifices were made by drilling holes in one surface of the wings at the locations listed in table I. Tubing was soldered into milled grooves in the wing surface opposite the orifice holes, and led from each orifice out through a hole in the hinge shaft.

Half bodies.- Two half bodies of revolution identical in profile were employed. The bodies consisted of a pointed nose 6 inches long on a 2-inch-diameter cylindrical afterportion 20 inches long. The nose profile is defined by the Haack equation

$$r = 0.564 \sqrt{\cos^{-1}\left(1 - \frac{x}{3}\right) - \sin \frac{1}{2} \left[\cos^{-1}\left(1 - \frac{x}{3}\right)\right]}$$

r(6) = .126

In error

The first body, designated model I, was tested in combination with the pressure-distribution wings, and the other body, designated model II, was tested in combination with the remaining wings. The pressure orifices were

$$r = \frac{1}{\sqrt{\pi}} \sqrt{\cos^{-1}\left(1 - \frac{x}{3}\right) - \frac{1}{2} \sin \left[2 \cos^{-1}\left(1 - \frac{x}{3}\right)\right]}$$

A. H. Jr.

made by sweating steel tubing in drilled holes and grinding the ends of the tubes flush with the body surface. The coordinate system by which the orifices are located is presented in the sketch accompanying table II(a). Pressure tubes from the orifices were led out around the wing hinge shaft.

Full-span models.- The full-span models consisted of a body to which was attached an aspect-ratio-1 rectangular wing or an aspect-ratio-2 triangular wing. These models were geometrically the same as two semispan model combinations having $r/s = 0.2$, as denoted in figure 1(a), but were reduced in size by the ratio of 7/16. The wing panels of the full-span models were integral to a common hinge shaft which, when set in place in the body, could be rotated to the desired wing deflection angle and then secured by a friction clamp.

Balance and Supports

The semispan wings were tested in the presence of a half body of revolution which was mounted on a boundary-layer plate. The boundary-layer plate served as a flow reflection plane and as a means of eliminating the effect of tunnel wall boundary layer in much the same way as the boundary-layer plate of reference 5; however, in the present tests the plate extended 11-1/2 inches farther upstream to accommodate the long body (see fig. 1(b)). Since the plate could not be rotated, angle of attack was varied by attaching the body to the plate at the desired angles. For pressure-distribution tests the hinge shafts of the wings were supported by bearings in the body and at the tunnel wall. For balance tests of the wings, the shaft passed through a hole in the body and was supported entirely by a strain-gage balance (see ref. 8). A fairing extended between the wall of the tunnel and the back side of the boundary-layer plate to shield the support shaft from air loads. A 0.005- to 0.010-inch gap was provided between the wing and body in order to prevent mechanical interference. In addition, the operation of the balance in the force tests required an annular gap of 0.10 inch around the wing hinge shaft.

The full-span models were supported from the rear by a 13° bent sting. This bent sting was used to increase the range of positive angles of attack. Lift and drag forces acting on these models were measured by a strain-gage balance which supported the sting. Pitching moment was measured by strain gages mounted on the sting between the model and the balance. The sting was shielded from aerodynamic forces by a shroud that extended to within 0.015 inch of the base of the model. The base pressure of the models was measured by static-pressure orifices in the sting adjacent to the base.

PROCEDURE

Test Conditions

Tests of the semispan models were conducted at a Mach number of 3.36 and a Reynolds number per inch of 0.85 million. The body was set at fixed angles of attack and the wing deflection angle was varied such that the maximum wing deflection angle or the sum of the body angle of attack and wing deflection did not exceed $\pm 45^\circ$. The body angle of attack was varied from 0° to 25° . Tests of the aspect ratio $2/3$ and $3/8$ triangular wings were limited to the cases of zero body angle of attack with varying wing deflection angle, and zero wing deflection angle with varying body angle of attack.

The full-span models were tested at Mach numbers of 1.98, 2.44, and 3.36 and at a Reynolds number per inch of 0.85 million. The body angle of attack was varied through a nominal range of -4° to $+30^\circ$ with the wing set at fixed deflection angles ranging from -35° to $+40^\circ$.

Reduction of Data

Semispan models. - Comparisons of tunnel stream surveys for the conditions of tunnel empty and with the boundary-layer plate present indicated a plate-induced spanwise Mach number variation in the region occupied by the semispan models. Therefore average Mach numbers were determined according to the spanwise extent of each model:

Model	Average Mach number, \bar{M}
Body	3.36 ± 0.02
All models having $r/s = 0.4$	3.40 ± 0.02
All models having $r/s = 0.2$	3.43 ± 0.02

As it was desirable to compare the data for the wing in the presence of the body with the corresponding data for the wing alone, it was necessary to correct the data from the average Mach number, \bar{M} , to the Mach number of the wing-alone data, $M = 3.36$. The following approximation was used:

$$(\text{Coefficient at } M = 3.36) \approx \frac{\sqrt{M^2 - 1}}{\sqrt{(3.36)^2 - 1}} (\text{Coefficient at } \bar{M})$$

For the pressure-distribution wings tabular integration of the corrected values of measured pressure distribution along the wing chord provided local span loading coefficients and chordwise centers of pressure.

The spanwise load distributions were in turn integrated to obtain normal-force, hinge-moment, and root bending-moment coefficients. For the other wings, normal-force, hinge-moment, bending-moment, and drag coefficients were determined from balance measurements. The normal-force coefficient is presented for these wings in order to be consistent with the pressure-distribution-wing data since in the latter case the distribution of ori-fices and their limited number precluded an accurate measurement of chord force.

Pressure distributions around the circumference of the body were integrated to give local longitudinal loading coefficients. The difference between the local loading for the body in the presence of a wing and the body alone yielded the interference loading on the body which was then integrated to give interference normal-force and pitching-moment coefficients about the wing hinge-line reference. Reasons for presenting only interference loading on the body are discussed in more detail in a later section.

Full-span models.- Variations of Mach number from free-stream conditions were negligible at the full-span-model locations and required no corrections to the measured data. Normal-force and total drag coefficients were determined from balance measurements. The drag coefficients were corrected to a condition of free-stream pressure on the base of the body. Pitching-moment coefficients, determined from measured pitching moments, were referred to the wing hinge axis. The actual angles of attack of the body were determined by photographs because of small deflections of the sting due to aerodynamic loads on the model.

RELIABILITY OF DATA

Limits of Uncertainty

The uncertainty in the data was assessed on the basis of repeatability, estimated effects of tunnel stream asymmetry, and uncertainty in the average Mach number in the wind tunnel at the model location. The limits of uncertainty for the wings in the presence of the body were:

$$C_{Nw}(B) \quad \pm 0.015 \text{ for all wings}$$

$$C_{hW}(B) \quad \begin{cases} \pm 0.010 \text{ for rectangular wings of } A = 3 \text{ and } A = 1, r/s = 0.4; \\ \pm 0.005 \text{ for all other wings} \end{cases}$$

$$C_{bW}(B) \quad \begin{cases} \pm 0.040 \text{ for rectangular wing of } A = 1, r/s = 0.4; \\ \pm 0.020 \text{ for all other wings} \end{cases}$$

$C_{Dw}(B)$	± 0.010 for all wings
$P_w(B)$	± 0.010
$c_{n_w}(B)$	± 0.010 } for pressure-distribution wings

The limits of uncertainty for the body in the presence of the wings, which apply up to $\alpha_B = 20^\circ$ as discussed later, are given as follows:

$\Delta C_{N_B}(W)$	$\pm 0.13/S_w$	(These quantities are inversely proportional to the wing reference area and chord and are approximately equal to two of the smallest grid-line divisions on the graphs.)	
$\Delta C_m(B)(W)$	$\pm 0.34/\bar{c}S_w$		
$P_B(W)$	± 0.010		
$\Delta c_{n_B}(W)$	± 0.010		

The limits of uncertainty for the full-span models were:

$C_{N_{BW}}$	± 0.015
$C_{m_{BW}}$	± 0.030
$C_{D_{BW}}$	± 0.010
$\frac{S_w}{S_B} C_{N_B}$	± 0.08
$\frac{\bar{c}S_w}{DS_B} C_{m_B}$	± 0.50
$\frac{S_w}{S_B} C_{D_B}$	± 0.05

The uncertainty in Reynolds number per inch was ± 0.05 million.

Effects of Wing-Body Gap on Semispan Data

The effect of the annular clearance gap around the supporting shaft of the force test wings was evaluated through limited measurements on the pressure-distribution wings with and without a gap. A comparison of the data showed that the effects of the gap were insignificant. The effect of the gap between the body and the undeflected wing was assumed to be negligible for the gap-span ratios and angles of attack of the present test on the basis of the findings of references 9 and 10.

Effects of Boundary-Layer Plate on Half-Body Data

Evidence of boundary-layer effects on the half-body data was revealed by preliminary comparisons of pressure-test results of the half body alone with those of force tests on the full body alone. This comparison is presented in figure 2(a) in the form of normal-force coefficients plotted against angle of attack. Figure 2(a) shows that good agreement between the test methods occurs up to $\alpha_B = 15^\circ$. Beyond 15° an increasing loss of the normal-force coefficient of the half model is evident with increasing angle of attack. The poor agreement above 15° appears to be coincident with the fact that above $\alpha_B = 17.3^\circ$ the crossflow Mach number exceeds unity and interaction effects of the resulting crossflow shock with the plate boundary layer might be expected. In figure 2(b), which presents longitudinal loading along the cylindrical portion of the half-body model, an additional effect is shown which might be attributed to the boundary-layer plate. This is observed as a high loading near the base of the body which increases with angle of attack.

It is believed that the foregoing effects of boundary-layer interference are, to a large extent, eliminated in the interference data presented herein for the body in the presence of a wing. The procedure for determining interference, as mentioned in the data-reduction section, consisted of subtracting from the load distribution on the body in the presence of a wing, the loading distribution of the body alone at the same angle of attack. The boundary-layer plate effects, being presumably little affected by the presence of a wing, were thus minimized in the resulting interference loading.

In view of the foregoing discussion, the limits of uncertainty presented earlier for the interference force and moment coefficients on the body in the presence of a wing should apply up to $\alpha_B = 20^\circ$. Because of the large boundary-layer effects encountered at higher angles of attack, the reliability limits at $\alpha_B = 25^\circ$ are uncertain but are not expected to be in excess of ± 10 percent of the interference force and moment coefficients presented in the basic data.

Comparison of Full-Span and Semispan Data

An additional means of assessing the reliability of measurements was provided by a comparison of the results from the two independent methods employed in the investigation for the $A = 1$ rectangular wing and body combination. The data from both test methods were compared on a basis common to both; that is, the sum of the lift of the wing in the presence of the body and the interference lift on the body due to the wing, obtained from the semispan model tests, was compared with the equivalent total combination lift minus the lift of the body alone, obtained from the

full-span-model tests. A similar comparison of moment about the wing hinge line was also made. These comparisons are presented in figures 3(a) and 3(b), respectively. Figure 3(a) shows that the maximum differences between the two test methods occur at high positive and negative values of the lift component where the deviation is generally no greater than about ± 0.02 from a mean curve. This scatter substantially verifies the individual estimations of data reliability for the two test methods. As previously indicated, the degree of precision in measuring moments on the semispan models was considerably greater than that for full-span models. Therefore, the curves of figure 3(b) were drawn to favor the semispan data. The comparison thus reflects primarily the limited reliability of the full-span-model moment measurements. Errors in this quantity are inherently large for the full-span model, due to the remote location of the moment gage from the wing hinge-line reference axis.

RESULTS

All pressure data presented are in tabular form. Because of the large number of individual pressure measurements obtained, it was impractical to present a complete tabulation of all the data obtained. Tabulation of pressure coefficients was therefore restricted to cases of α_B variable, $\delta_W = 0^\circ$, and δ_W variable, $\alpha_B = 0^\circ$. However, complete loading results in terms of wing span loading and loading induced on the body by the wing are tabulated for all conditions investigated. The following index indicates the specific pressure and loading data presented in each table.

Model			Table number	
Plan form	A	r/s	Pressure coefficients	Span loading coefficients
Wing in presence of body				
Triangular	4	0.2	I(a)	III(a)
Triangular	2	.2	I(b)	III(b)
Rectangular	2	.2	I(c)	III(c)
Body in presence of wing			Pressure coefficients	Longitudinal interference loading coefficients
Triangular	4	.2	II(a)	IV(a)
	2	.2	II(b)	IV(b)
	1	.2	II(c)	IV(c)
	1	.4	II(d)	IV(d)
	2/3	.4	II(e)	^a IV(e)
	3/8	.4	II(f)	^a IV(f)
Rectangular	3	.2	II(g)	IV(g)
	2	.2	II(h)	IV(h)
	1	.2	II(i)	IV(i)
	1	.4	II(j)	IV(j)
Body alone			V	---

^aOnly for cases of α_B variable, $\delta_W = 0^\circ$, and δ_W variable, $\alpha_B = 0^\circ$.

Force and moment data obtained from the pressure measurements and from the balance measurements are presented in graphical form. A plan view of the combination tested is shown on each basic data figure, and the shaded area indicates the component of the combination for which the data applies. The following index indicates the specific data presented in each figure.

Mach number	Model			Figure number						
	Plan form	A	r/s	$C_{N_W}(B)$	$C_{h_W}(B)$	$C_{b_W}(B)$	$C_{D_W}(B)$	$\Delta C_{N_B}(W)$	$\Delta C_{m_B}(W)$	
3.36	Triangular	4	0.2	4(a)	5(a)	6(a)	(1)	8(a)	9(a)	
		2	.2	4(b)	5(b)	6(b)	(1)	8(b)	9(b)	
		1	.2	4(c)	5(c)	6(c)	7(a)	8(c)	9(c)	
		1	.4	4(d)	5(d)	6(d)	7(b)	8(d)	9(d)	
		2/3	.4	4(e)	5(e)	6(e)	7(c)	8(e)	9(e)	
	Rectangular	3/8	.4	4(f)	5(f)	6(f)	7(d)	8(f)	9(f)	
		3	.2	4(g)	5(g)	(1)	7(e)	8(g)	9(g)	
		2	.2	4(h)	5(h)	6(g)	(1)	8(h)	9(h)	
		1	.2	4(i)	5(i)	6(h)	7(f)	8(i)	9(i)	
		1	.4	4(j)	5(j)	6(i)	7(g)	8(j)	9(j)	
Mach number	Plan form	A	r/s	$C_{N_{BW}}$	$C_{m_{BW}}$	$C_{D_{BW}}$	$\frac{S_W}{S_B} C_{N_B}$	$\bar{C}_{S_W} C_{N_B}$	$\frac{S_W}{S_B} C_{m_B}$	$\frac{S_W}{S_B} C_{D_B}$
1.98	Triangular	2	.2	10(a)	11(a)	12(a)				
1.98	Rectangular	1	.2	10(b)	11(b)	12(b)				
2.44	Triangular	2	.2	10(c)	11(c)	12(c)				
2.44	Rectangular	1	.2	10(d)	11(d)	12(d)				
3.36	Triangular	2	.2	10(e)	11(e)	12(e)				
3.36	Rectangular	1	.2	10(f)	11(f)	12(f)				
1.98	Body alone						13	13	13	13
2.44	Body alone						13	13	13	13
3.36	Body alone						13	13	13	13

¹No data

DISCUSSION

In addition to the basic data figures, summary figures are presented to facilitate discussion of the principal effects of high angles of attack and wing deflection on force and moment coefficients. In order to separate the effects of angle of attack and wing deflection, plots were made of experimental data for the cases of variable angle of attack with zero wing deflection angle and variable wing deflection with zero angle of attack (hereinafter designated α_B variable and δ_W variable, respectively). These experimental data are also compared with corresponding values from available theory. The theoretical values were obtained by modifying the experimental wing-alone characteristics by the methods of references 11-14.

which involve the use of interference factors to account for the effects of body-wing interaction. The manner in which these interference factors were used in calculating lift and moment in the present report are developed in the appendix. Published experimental results for the wings alone can be found in references 5, 6, and 7. Small corrections to α_B and δ_W were applied, whenever necessary, to the experimental results presented in the summary figures to provide zero values of the force and moment coefficients at zero α_B and δ_W .

Component Characteristics at $M = 3.36$

In the wing-body interference theory utilized herein consideration is not given to the chordwise forces arising either from pressures or viscosity. Accordingly, calculations could only be made of the normal force or the lift component of normal force acting on the model components. Comparisons of theory with experiment for the wings and the body were more conveniently made on the basis of the lift component of normal force. These quantities are defined as follows:

$$C_{LW}^*(B) = C_{NW}(B) \cos \alpha_B; \quad \Delta C_{LB}^*(W) = \Delta C_{NB}(W) \cos \alpha_B \quad \alpha_B \text{ variable}$$

$$C_{LW}^*(B) = C_{NW}(B) \cos \delta_W; \quad \Delta C_{LB}^*(W) = \Delta C_{NB}(W) \quad \delta_W \text{ variable}$$

Lift of the wings in presence of the body. - Comparisons of theoretical with experimental lift are given in figure 14(a) for triangular wings and in figure 14(b) for rectangular wings. The theoretical values were computed by the following relationships:

$$C_{LW}^*(B) = K_W(B) C_{LW}^* \quad \alpha_B \text{ variable}$$

$$C_{LW}^*(B) = k_W(B) C_{LW}^* \quad \delta_W \text{ variable}$$

For triangular wings in the presence of the body, the theory is in good agreement with experiment in the range $\alpha_B = 0^\circ$ to 6° for the variable α_B case at all aspect ratios. For angles of attack greater than about 10° , a decrease of lift below the theoretical curve is indicated, particularly for the models having an r/s of 0.4. A similar result was found in references 3 and 4 for a rectangular wing tested in combination with a body at $M = 1.89$ and 2.93 . These decreases in lift result from a decrease in the effect of body upwash on the lift of the wing. The decreased effectiveness of body upwash above 10° angle of attack is believed to be due to the presence of body vortices since it is known that body vortices tend to reduce body upwash in the plane of the wing. An investigation at $M = 2.00$

of a body similar to that of the present tests, reported in reference 15, shows that such body vortices appear at about a body angle of attack of 10° . An approximate estimate was made of the effect of body vortices on the lift of the $A = 1$ triangular wing in presence of the body for an $r/s = 0.4$. The strengths and positions of the body vortices were assumed to be the same as those reported in reference 15 for the similar body alone at $M = 2.00$. The effective induced downwash field of the body vortices in the plane of the wing was evaluated by strip theory. As indicated in figure 14(a) the inclusion of the effects of vortex-induced downwash on the wing accounts for a large portion of the discrepancy between theory and experiment. It is evident that a method of defining the vortex field for a supersonic wing-body combination is needed for inclusion in a theory applicable at large angles of attack. Furthermore, such a method should consider possible effects of crossflow shock waves on the body flow field when the critical crossflow Mach number is exceeded.

In the variable δ_W case of figure 14(a), the theoretical values of lift are in good agreement with experimental in the range of δ_W from 0° to 20° for all aspect ratios except $A = 3/8$. At deflection angles above 20° the $A = 3/8$ wing provided greater lift than that of the wing alone at the same angles. This greater lift can be accounted for to a large extent by the following reasoning: For moderate wing deflections, the resulting breach between the deflected wing and the body is large compared to the wing semispan, due to large ratio of wing root chord to body radius. Under these conditions the wing panel behaves to some extent as an independent wing of reduced aspect ratio (for this case, $A = 3/16$). Wings of such slenderness partake of the characteristics of bodies and experience significant contributions of lift due to crossflow drag. This is apparent by the parabolic shape of the experimental lift curve (see ref. 16) indicated in figure 14(a) for the $A = 3/8$ wing in the presence of the body.

The rectangular wings in the presence of the body show about the same degree of agreement between theory and experiment over substantially the same range of α_B and δ_W as for the triangular wings.

Figure 4 shows that both plan forms exhibit no important adverse effects of combined angles of attack and deflection, and retain their normal-force effectiveness up to at least the maximum angle of the tests (approximately 45°).

Hinge moments of the wings in presence of the body. - Comparisons of theoretical with experimental hinge moments are given in figure 15(a) for triangular wings and in figure 15(b) for rectangular wings. The theoretical values were computed by the following relationships which are developed in the appendix:

Triangular wings

$$C_{hW}(B) = K_{W(B)} \left\{ C_{hW} + \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{NW} \right\} \quad \alpha_B \text{ variable}$$

$$C_{hW}(B) = k_{W(B)} \left\{ C_{hW} + \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{NW} \right\} \quad \delta_W \text{ variable}$$

Rectangular wings

$$C_{hW}(B) = K_{W(B)} C_{hW} \quad \alpha_B \text{ variable}$$

$$C_{hW}(B) = k_{W(B)} \left\{ C_{hW} + \left[\left(\frac{\bar{x}}{c_r} \right)_W - \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{NW} \right\} \quad \delta_W \text{ variable}$$

For the triangular wings in the presence of the body, $r/s = 0.2$, the theoretical hinge moments are within ± 20 percent of the experimental in the range of α_B from 0° to 6° in the variable α_B case. This 20-percent hinge-moment margin represents an accuracy in prediction of the chordwise center-of-pressure positions to within $\pm 0.01 \bar{c}$. The shaded areas in figure 15 represent the contribution to $C_{hW}(B)$ by a $0.01 \bar{c}$

shift in wing center-of-pressure position. For the models having $r/s = 0.4$ in the range α_B from 0° to 6° , the agreement between theoretical and experimental wing hinge moments is not as good as for the models having $r/s = 0.2$. Above $\alpha_B = 6^\circ$, and for both values of r/s , a large discrepancy between theory and experiment occurs emphasizing the need for an accurate definition of the vortex field for wing-body combinations at high angles of attack. As in the case of lift, the effects of body vortices were approximately estimated for the $A = 1$ triangular wing, $r/s = 0.4$, and are indicated in figure 15(a).

In the variable δ_W case, the theoretical hinge moments are, in general, within ± 20 percent of the experimental, representing a maximum of $\pm 0.01 \bar{c}$ error in the chordwise center-of-pressure position in the deflection-angle range of δ_W from 0° to 25° .

For the rectangular wings the theoretical hinge moments are within ± 10 percent of the experimental throughout the angle-of-attack range for the $A = 2$ and 3 wings in the variable α_B case. The agreement between the theoretical and experimental hinge moments of the $A = 1$ wings, however, is poor. The experimental values indicate at least an $0.01 \bar{c}$ shift in the center-of-pressure position forward of that of the wing alone.

In the variable δ_W case, the agreement between theory and experiment for the rectangular plan forms of $A = 2$ and 3 over the wing deflection range of δ_W from 0° to 25° was the same as in the case of the triangular

wings. The wings of $A = 1$ gave similar agreement but over the more restricted range of δ_w from 0° to 15° .

The primary effects of wing plan form at large combined angles of δ_w and α_B can be seen by a comparison of hinge moments of triangular wings (figs. 5(a) to 5(f)) with those of the rectangular wings (figs. 5(g) to 5(j)). This comparison shows that the rectangular wing hinge moments in presence of the body are more linear with δ_w than those of the triangular wings in the higher range of α_B tested. At these high angles, an inboard loading loss occurs in the wing-body juncture due to the combined effects of body vortices and the wing-body breach resulting from wing deflection. The result is an outboard shift in wing loading approximately along the midchord line causing, in the case of triangular wings of swept-back midchord line, a corresponding rearward shift in center of pressure, as pointed out in reference 17. This rearward shift in center of loading on wings with sweptback midchord lines gives a more nonlinear hinge moment than that exhibited by wings with unswept midchord lines.

Bending moments of the wings in presence of the body. - Comparisons of theoretical with experimental bending moments are given in figure 16(a) for triangular wings and figure 16(b) for rectangular wings. The theoretical values were calculated on the assumption that the spanwise center of pressure of a wing in the presence of a body is the same as that of the wing alone. Therefore, the theoretical bending moments are given by:

$$C_{bW(B)} = K_{W(B)} C_{bW} \quad \alpha_B \text{ variable}$$

$$C_{bW(B)} = k_{W(B)} C_{bW} \quad \delta_w \text{ variable}$$

In general, the wing alone bending moments are in as good agreement with experiment as the theoretical for both plan forms. For the triangular wings, the agreement between theory and experiment is poor for the $A = 1$ wing, $r/s = 0.2$, and for the $A = 3/8$ wing, $r/s = 0.4$. The agreement for the latter is especially poor for low body and wing incidences. The poor agreement for both wings must be the result of an inboard movement of the spanwise center of pressure, inasmuch as the corresponding theoretical and experimental lifts (fig. 14(a)) are in good agreement for α_B from 0° to about 10° and for δ_w from 0° to 20° . The reasons for this inboard movement, however, are not clear. Nevertheless, for the $A = 3/8$ wing a part of the disagreement is probably due to the effect of wing-root geometry, since this wing had a nonfilleted root section and theoretical calculations were based on experimental data for a wing-alone model which had a filleted root section. For both plan forms the $A = 1$ wings, $r/s = 0.4$, show higher bending moments than could be accounted for by theory, particularly in the variable δ_w case. The reasons are not clear for the apparent large outward shift in spanwise center of loading (the outward shift is again obvious since the corresponding theoretical and experimental lifts are in good agreement).

Span load distributions of three wings in the presence of the body are presented in figure 17 and are compared with the corresponding wing-alone span load distributions. For the variable α_B case the expected increased inboard loading due to body upwash is demonstrated, particularly at $\alpha_B = 6^\circ$. For the variable δ_W case the effect of the wing-body breach is noticeable as a loss of inboard loading, particularly at $\delta_W = 20^\circ$ as compared to the wing-alone values.

Drag of the wings in the presence of the body.- In the low-incidence range the predicted drag rise $(C_D - C_{D\min})_{W(B)}$ is given by:

$$(C_D - C_{D\min})_{W(B)} = K_W(B) C_{N_W} \sin \alpha_B \quad \alpha_B \text{ variable}$$

$$(C_D - C_{D\min})_{W(B)} = k_W(B) C_{N_W} \sin \delta_W \quad \delta_W \text{ variable}$$

It was found that, for wings of both plan forms, the theoretical and experimental drag rise coefficients were in good agreement in the identical angle range of α_B from 0° to 6° , and δ_W from 0° to 20° , in which the corresponding lift coefficients were also in good agreement. Therefore, no summary figures for the drag rise coefficients are presented.

At large combined angles a small decrease of drag was effected by increasing r/s from 0.2 to 0.4 for both triangular and rectangular wings of $A = 1$ (figs. 7(a), (b), (f), and (g)). The minimum drag for all wings on which drag was measured showed little change with α_B in the range 0° to 10° ; above 10° , there was a slight increase in minimum drag with increasing α_B . This increased drag is not significant for a wing-body combination but it might be an indication that the nature of the boundary layer over the wing was affected by the body at angles greater than about $\alpha_B = 10^\circ$.

Interference lift on the body due to the wings.- Comparisons of theory and experiment are given in figure 18(a) for the body in the presence of the triangular wings and in figure 18(b) for the body in the presence of the rectangular wings. The theoretical interference lifts are given by the following expressions:

$$\Delta C_{L_B^*} = K_B(W) C_{L_W^*} \quad \alpha_B \text{ variable}$$

$$\Delta C_{L_B^*} = k_B(W) C_{L_W^*} \quad \delta_W \text{ variable}$$

The theoretical values of interference lift on the body in the presence of the triangular wings in the variable α_B case are in fair accord with the experimental over the range of α_B from 0° to 25° when $r/s = 0.2$. For $r/s = 0.4$, theory is in good accord with experiment in the range of

α_B from 0° to 10° ; beyond this angle range the interference lifts given by theory are too large. This discrepancy is believed to be a result of body vortices and crossflow shock waves as was pointed out in the discussion of lift on the wings. It should be noted that the lack of agreement between theoretical and experimental wing lift in the presence of the body above $\alpha_B = 10^\circ$ was, in general, also more pronounced for the configurations having an $r/s = 0.4$ than for those with an $r/s = 0.2$.

In the variable δ_W case for triangular wings, the theoretical interference lifts on the body are generally in fair accord with experimental in the range of wing deflection angles from 0° to 10° . The δ_W range wherein theory is in satisfactory agreement with experiment tends to increase with aspect ratio for both values of r/s . At larger wing deflections, the existence of a relatively large wing-body breach violates the geometrical considerations upon which the interference factor $k_{B(W)}$ is based and hence departure of theory from experiment is to be expected. Such a departure is indicated in figure 18(a) where, at large deflection angles, a decrease in interference lift occurs, resulting in negative values for some cases.

In the case of variable α_B for the body in the presence of the rectangular wings, good agreement results over the angle range between the theoretical and experimental interference lifts on the body for all aspect ratios and r/s investigated.

The comparison of the theoretical and experimental interference lift on the body due to the rectangular wings in the variable δ_W case gave essentially the same results as found for the case of the triangular wings. As indicated in figure 18, theoretical values based on a modified theory (see eq. (A1) in appendix) are generally in better agreement with experiment and the range of agreement is extended to higher deflection angles, particularly for the rectangular wings. This modified theory in effect extends slender-body interference factors to the case of a non-slender configuration.

Distributions of interference normal force on the body due to the presence of the wings are presented in figure 19. Three wing-body models are considered, among which are included combinations having the largest and smallest values of the ratio c_r/r . The theoretical loading distribution on the body computed for $\alpha_B = 6^\circ$ demonstrates a fair agreement of total loading and its distribution along the body for all three models. At $\alpha_B = 20^\circ$ the total loading was increased approximately in proportion to the angle-of-attack increase in each case; however, some change in the load distribution is indicated, particularly for the models having small c_r/r values (2.67 and 4).

For $\delta_W = 6^\circ$ the theoretical body load distribution for the long chord triangular wing model ($c_r/r = 16$) is uniformly higher than the experimental. This disagreement is due to the effect of the wing-body

breach evidenced by the small region of negative loading developed on the body near the wing leading edge. For the short chord wings the theoretical loading is in good agreement with the experimental for the triangular wing but is in poor agreement for the rectangular wing. It is notable that the use of the modified theory materially improves the agreement with the experimental load distribution for the rectangular wing case but does not alter the good agreement of slender-body theory with experiment for the triangular wing case. At $\delta_w = 30^\circ$ the distribution of load on the body for models of small c_r/r is not materially altered by the increase in wing deflection. For the model with large c_r/r , however, the large wing-body breach apparently allows a large negative loading to develop on the body forward of the wing hinge axis due to the bleeding of positive pressures on the bottom of the wing to the top of the body.

The effects of high combined angles on normal force are apparent from an examination of figure 8. The general nonlinearity of $\Delta C_{N_B}(W)$ with variation in δ_w is evident, and is only slightly affected by body angle of attack up to 25° .

Interference moment on the body due to the wings.- Comparisons of theory and experiment are given in figure 20(a) for the body in the presence of the triangular wings and in figure 20(b) for the body in the presence of the rectangular wings. The theoretical interference moments are given by the following expressions:

Triangular wings

$$\Delta C_{m_B}(W) = \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{N_W} \quad \alpha_B \text{ variable}$$

$$\Delta C_{m_B}(W) = \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{L_W^*} \quad \delta_w \text{ variable}$$

Rectangular wings

$$\Delta C_{m_B}(W) = \left[\frac{1}{2} - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{N_W} \quad \alpha_B \text{ variable}$$

$$\Delta C_{m_B}(W) = \left[\frac{1}{2} - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{L_W^*} \quad \delta_w \text{ variable}$$

In the variable α_B case, good agreement between theoretical and experimental interference moments on the body due to wings of both plan forms is found over the entire range of α_B , except for combinations having wings with the smallest ratio of root chord to body radius.

For both plan forms in the variable δ_W case, interference moments on the body given by theory are in good agreement with those of experiment in the range of wing deflection angles from 0° to 10° . Except for the two models having the smallest c_r/r , the modified theory again provided somewhat better agreement with experiment than did the slender-body theory. At large deflection angles, except for the models having large c_r/r , a decrease in the magnitude of interference moment on the body occurred due to a decrease of body loading. For the models having the largest c_r/r , however, a stabilizing couple, resulting from the large negative loading developed on the body ahead of the wing hinge line (see fig. 19(f)), compensated for the effect of the load loss on the moment. Thus, in the case of the two models of largest c_r/r , the agreement at large deflection angles between experiment and theory is good, though fortuitous.

Complete Configuration at $M = 1.98, 2.44$, and 3.36

Combined lifts of the wing-body configurations. - The configuration lift component of normal force less that of the body alone, $C_{LBW}^* - C_{LB}^*$, is compared with theory in figure 21. The equivalent theoretical values are given by the quantity $C_{LW(B)}^* + \Delta C_{LB(W)}^*$. The theoretical combined lifts are in good agreement with the experimental in the angle-of-attack range 0° to 6° with zero wing deflection for both plan forms.

In the case of variable wing deflection with zero body incidence, theory and experiment are in satisfactory agreement in the wing deflection range 0° to 10° for both plan forms at all test Mach numbers for which experimental data were available. At large deflection angles the effect of the resulting breach between the wing and body is to reduce the lift of the wing-body combination (excluding the body nose) to values below that of the wing alone.

No comparisons of experimental $C_{LBW} - C_{LB}$ with theoretical were made since it was found that the resulting small quantities would be of the same order as the accuracy of the experimental values.

Effects of Mach number. - The full-span models tested at the Mach numbers 1.98, 2.44, and 3.36 were not instrumented to give the division of force and moments on the body and wing. Therefore, direct comparisons of Mach number could not be made on the ranges of agreement of theoretical and experimental lifts of the wings in the presence of the body and the body in the presence of the wings. However, an examination of figure 21 shows that for the combined lifts, $C_{LW(B)}^* + \Delta C_{LB(W)}^*$, or the equivalent value, $C_{LBW}^* - C_{LB}^*$, there is no significant effect of Mach number on the ranges of angles of attack and wing deflection wherein theory and

experiment are in good agreement. Some effects of Mach number might be expected due to the fact that with decreasing Mach number, critical cross-flow Mach numbers with their attendant effects on crossflow occur at increasing angles of attack. No direct information is available in regard to the effect of Mach number on the angles of attack at which body vortices become important. Figure 13 shows, however, that the normal-force curves for the body alone are approximately linear to about $\alpha_B = 6^\circ$ at the test Mach numbers. At higher angles, the normal-force curves become approximately parabolic in shape due to the contribution of crossflow drag (see ref. 16), implying the presence of body vortices.

CONCLUSIONS

The following conclusions are based on data from semispan triangular and rectangular wing and body combinations tested at a Mach number of 3.36.

1. The mutual interference effects of wing and body in combination can be estimated with good accuracy by means of theoretical interference factors applied to experimental wing-alone characteristics. The good agreement, however, was limited to ranges of body angles of attack α_B and wing deflections δ_W that varied with wing geometry. The minimum ranges of agreement are given as follows:

Coefficient	α_B variable, $\delta_W = 0$	δ_W variable, $\alpha_B = 0$
Wings in the presence of the body		
Lift coefficient	0° to 6°	0° to 20°
Hinge-moment coefficient		
Triangular plan form	0° to 6°	0° to 25°
Rectangular plan form	0° to 6°	0° to 15°
Body in the presence of the wings		
Interference lift coefficient	0° to 10°	0° to 10°
Interference moment coefficient	0° to 15°	0° to 15°

2. A decrease of lift below the theoretical for the undeflected wings in the presence of the body occurred at body angles of attack greater than about 10° . This decrease of lift, particularly affecting the inboard wing sections, resulted from a decrease in the effect of body upwash which is believed to be due to the combined effects of body-nose vortices and transonic crossflow.

3. In combination with a body, the triangular wings of aspect ratios $2/3$ and $3/8$, which have large root chords compared to the body radius, showed approximately parabolic curves of lift as a function of wing deflection angle. This parabolic shape indicates significant contributions of lift due to crossflow drag of the wing at large deflection angles.

4. At large body angles of attack, the variation of hinge moments of the triangular wings in the presence of the body were more nonlinear with wing deflection than those for the rectangular wings. This was a consequence of a rearward movement of the center of pressure for the triangular wings which accompanied an outward shift occurring at high wing deflections.

5. For the triangular wing and body combinations having a large ratio of wing root chord to body radius, the opening of a relatively large wing-body gap due to wing deflection produced a large negative interference load distribution on the body forward of the wing hinge axis. This resulted in highly nonlinear interference force and moment coefficients.

On the basis of data measured at Mach numbers 1.98, 2.44, and 3.36 on two smaller scale full-span models of two of the semispan configurations, the following conclusion was evident:

1. The ranges of angles of attack and wing deflection wherein the theoretical and experimental values of the lift component of normal force of the configuration less that of the body alone were in good agreement, were insignificantly affected by Mach number.

Ames Aeronautical Laboratory
National Advisory Committee for Aeronautics
Moffett Field, Calif., Mar. 12, 1956

APPENDIX A

INTERFERENCE FACTORS

The interference factors used to compute the theoretical curves of force and moment coefficients presented in the summary figures were obtained either from slender-body theory or linear-theory solutions. In cases where both solutions were available, linear-theory factors were generally used, when applicable. The following table summarizes the particular references from which the interference factors were determined. (The superscripts S and L refer, respectively, to slender-body theory and linear theory.)

Wing in the presence of the body			Body in the presence of the wing				
α_B variable, $\delta_W = 0^\circ$							
$K_W(B)$				$K_B(W)$			
Triangular	Rectangular	Triangular	Rectangular	Slender-body	Linear	Slender-body	Linear
Linear	Slender-body	Linear	Slender-body	Linear	Slender-body	Linear	Slender-body
---	Ref. 14, fig. 2	---	Ref. 14, fig. 2	Ref. 11, fig. 4 or Ref. 12, fig. 4 Ref. 13, fig. 2 Ref. 14, fig. 5(a)	Ref. 14, fig. 2	Ref. 11, fig. 4 or Ref. 12, fig. 4 Ref. 13, fig. 2 Ref. 14, fig. 5(a) for $SA \geq 2$ and $[K_B(W)]^S > [K_B(W)]^L$	Ref. 14, fig. 2
δ_W variable, $\alpha_B = 0^\circ$							
$K_W(B)$				$K_B(W)$			
---	Ref. 14, fig. 2	Ref. 13, fig. 3 for $SA \geq 2$	Ref. 14, fig. 2	Eq. (A1) present report	Ref. 14, fig. 2	Eq. (A1) present report	Ref. 14, fig. 2

An estimate for a linear-theory value of $k_B(W)$ for both triangular and rectangular wings was made by the following:

$$[k_B(W)]^L = \frac{[k_B(W)]^L}{[k_B(W)]^S} [k_B(W)]^S \quad (A1)$$

In figures which involved the use of $k_B(W)$, both the slender-body value and the above modification were used.

HINGE MOMENTS OF THE WINGS IN THE PRESENCE OF THE BODY

The following general equations were used to calculate wing hinge moments:

$$C_{hW}(B) = k_W(B) \left\{ \frac{C_{hW}}{C_{NW}} + \frac{c_r}{c} \left[\left(\frac{\bar{x}}{c_r} \right)_W - \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] \right\} C_{NW} \quad \alpha_B \text{ variable} \quad (A2)$$

$$C_{hW}(B) = k_W(B) \left\{ \frac{C_{hW}}{C_{NW}} + \frac{c_r}{c} \left[\left(\frac{\bar{x}}{c_r} \right)_W - \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] \right\} C_{NW} \quad \delta_W \text{ variable} \quad (A3)$$

The term in the braces represents the center of pressure of the wing in the presence of the body obtained, as suggested in reference 13, by adding to the experimental wing-alone center of pressure, $\frac{C_{hW}}{C_{NW}}$, the theoretical shift in center of pressure, $\frac{c_r}{c} \left[\left(\frac{\bar{x}}{c_r} \right)_W - \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right]$. For triangular wings,

$\left(\frac{\bar{x}}{c_r} \right)_W = \frac{2}{3}$ and $\left(\frac{\bar{x}}{c_r} \right)_{W(B)}$ for both variable α_B and δ_W are determined from

figure 4 of reference 13. For rectangular wings, linear-theory values of $\left(\frac{\bar{x}}{c_r} \right)_W$ are given in figure 6 of reference 12; for variable α_B ,

$\left(\frac{\bar{x}}{c_r} \right)_{W(B)} = \left(\frac{\bar{x}}{c_r} \right)_W$ (see ref. 13), and for variable δ_W , values of $\left(\frac{\bar{x}}{c_r} \right)_{W(B)}$ based on linear theory for wings with $\beta A \geq 2$ are given in figure 6 of

reference 13. Rewriting equations (A2) and (A3) for specific cases:

Triangular wings

$$C_{hW}(B) = K_W(B) \left\{ C_{hW} + \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{N_W} \right\} \quad \alpha_B \text{ variable} \quad (A4)$$

$$C_{hW}(B) = k_W(B) \left\{ C_{hW} + \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{N_W} \right\} \quad \delta_W \text{ variable} \quad (A5)$$

Rectangular wings

$$C_{hW}(B) = K_W(B) C_{hW} \quad \alpha_B \text{ variable} \quad (A6)$$

$$C_{hW}(B) = k_W(B) \left\{ C_{hW} + \left[\left(\frac{\bar{x}}{c_r} \right)_W - \left(\frac{\bar{x}}{c_r} \right)_{W(B)} \right] C_{N_W} \right\} \quad \delta_W \text{ variable} \quad (A7)$$

INTERFERENCE MOMENT ON BODY DUE TO WING

The body interference moment coefficients were calculated by the following equations:

$$\Delta C_{mB}(W) = \frac{c_r}{c} \left[\left(\frac{x}{c_r} \right)_h - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] K_{B(W)} C_{N_W} \quad \alpha_B \text{ variable} \quad (A8)$$

$$\Delta C_{mB}(W) = \frac{c_r}{c} \left[\left(\frac{x}{c_r} \right)_h - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{L_W^*} \quad \delta_W \text{ variable} \quad (A9)$$

where for both variable α_B and δ_W , values of $\left(\frac{\bar{x}}{c_r} \right)_{B(W)}$ based on linear theory are given in figure 7 of reference 12 or figure 20 of reference 14. For specific cases equations (A8) and (A9) become:

Triangular wings

$$\Delta C_{mB}(W) = \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] K_{B(W)} C_{N_W} \quad \alpha_B \text{ variable} \quad (A10)$$

$$\Delta C_{mB}(W) = \left[1 - \frac{3}{2} \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{LW}^* \quad \delta_w \text{ variable} \quad (\text{Al1})$$

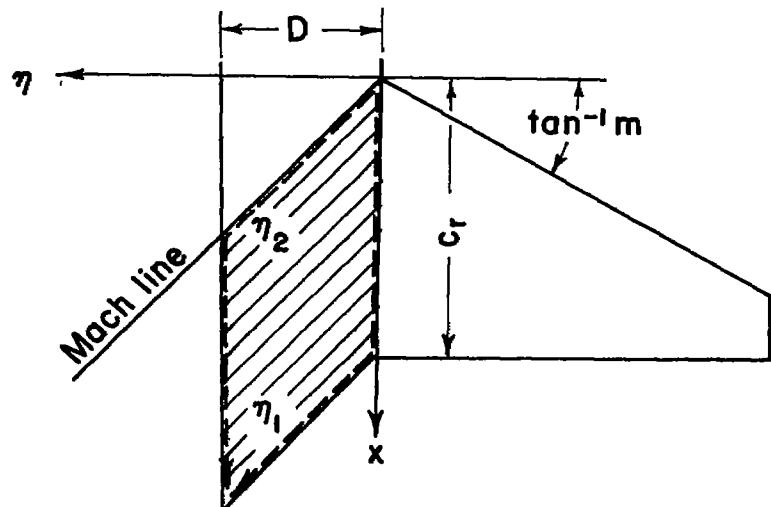
Rectangular wings

$$\Delta C_{mB}(W) = \left[\frac{1}{2} - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{NW} \quad \alpha_B \text{ variable} \quad (\text{Al2})$$

$$\Delta C_{mB}(W) = \left[\frac{1}{2} - \left(\frac{\bar{x}}{c_r} \right)_{B(W)} \right] k_{B(W)} C_{LW}^* \quad \delta_w \text{ variable} \quad (\text{Al3})$$

DISTRIBUTION OF INTERFERENCE NORMAL FORCE
ON THE BODY DUE TO THE WINGS

The theoretical body interference loading coefficient as a function of x , the distance along the body from the juncture of the body and the wing leading edge, calculated for variable α_B by the following integrals from reference 11. The variables of integration are defined in the accompanying sketch.



Supersonic-leading-edge wing

$$\Delta c_{nB(W)} = \frac{8m\alpha_B}{\pi D \sqrt{\beta^2 m^2 - 1}} \int_{\eta_1}^{\eta_2} \cos^{-1} \frac{x/\beta - \beta m \eta}{\eta + mx} d\eta$$

$$= \frac{8m\alpha_B}{\pi D \sqrt{\beta^2 m^2 - 1}} \left[\frac{\pi}{2} \eta - (\eta + mx) \sin^{-1} \left(\frac{x/\beta + \beta m \eta}{\eta + mx} \right) + \sqrt{\beta^2 m^2 - 1} \frac{x}{\beta} \sin^{-1} \frac{\eta}{x/\beta} \right]_{\eta_1}^{\eta_2}$$
(A14)

Subsonic-leading-edge wing

$$\Delta c_{nB(W)} = \frac{16(\beta m)^{3/2} \alpha_B}{\pi D \beta (\beta m + 1)} \int_{\eta_1}^{\eta_2} \frac{\sqrt{x/\beta - \eta}}{\sqrt{mx + \eta}} d\eta$$

$$= \frac{16(\beta m)^{3/2} \alpha_B}{\pi D \beta (\beta m + 1)} \left[\sqrt{(x/\beta - \eta)(mx + \eta)} + \frac{x/\beta(\beta m + 1)}{2} \tan^{-1} \sqrt{\frac{mx + \eta}{x/\beta - \eta}} \right]_{\eta_1}^{\eta_2}$$
(A15)

The loading for variable δ_W was then obtained by:

$$\left[\Delta c_{nB(W)} \right]_{\delta_W \text{ variable}} = \frac{\delta_W}{\alpha_B} \left[\frac{k_{B(W)}}{K_{B(W)}} \right] \left[\Delta c_{nB(W)} \right]_{\alpha_B \text{ variable}}$$
(A16)

wherein both the slender-body value of $k_{B(W)}$ and the linear-theory approximation (modified theory) given by equation (A1) were used.

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NACA RM A56C12

TABLE I.- PRESSURE COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY
 (a) $A = \frac{1}{4}$ triangular wing, $r/s = 0.2$

y/s	x/s	$\delta_w, \alpha_B = 0^\circ$										$\alpha_B, \delta_w = 0^\circ$									
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°			
.025	103	.085	.076	.085	.078	.070	.059	.047	.014	.180	.105	.070	.028	.037	.066	.074	.081	.078			
	331	.081	.071	.076	.079	.073	.059	.049	.034	.004	.131	.093	.063	.016	.049	.074	.083	.085			
	378	.083	.071	.076	.074	.068	.054	.038	.009	.109	.076	.047	.009	.017	.054	.069	.079	.085			
	487	.080	.069	.075	.075	.067	.059	.045	.019	.081	.050	.028	.009	.021	.053	.065	.075	.085			
	798	.090	.085	.092	.091	.085	.080	.075	.071	.055	.051	.054	.051	.063	.071	.098	.095				
	878	.081	.075	.087	.083	.082	.074	.069	.068	.049	.044	.042	.042	.067	.071	.088	.091				
	975	.085	.068	.080	.089	.080	.073	.061	.053	.013	.005	.038	.042	.064	.075	.087					
	186	.087	.079	.089	.087	.078	.069	.060	.035	.173	.114	.066	.014	.030	.063	.074	.076	.076			
	360	.087	.078	.089	.088	.081	.071	.065	.044	.149	.091	.047	.000	.034	.064	.076	.079	.081			
	375	.085	.077	.090	.088	.088	.074	.068	.051	.123	.071	.032	.000	.038	.070	.078	.088	.087			
.250	500	.086	.080	.090	.091	.089	.088	.076	.068	.056	.097	.049	.017	.048	.068	.083	.089	.091			
	685	.090	.087	.090	.091	.086	.077	.074	.062	.051	.081	.037	.009	.051	.073	.089	.095				
	750	.087	.084	.091	.089	.081	.073	.067	.061	.056	.086	.030	.002	.067	.081	.087	.091				
	875	.080	.070	.088	.088	.078	.067	.064	.061	.053	.015	.004	.038	.068	.074	.080	.089				
	966	.080	.077	.088	.087	.079	.070	.068	.058	.000	.037	.035	.015	.076	.088						
	185	.088	.084	.090	.090	.079	.070	.065	.040	.180	.097	.065	.010	.080	.054	.067	.068	.069			
	250	.082	.076	.089	.087	.078	.071	.068	.047	.141	.080	.043	.002	.027	.050	.068	.071	.075			
	500	.088	.077	.088	.087	.078	.068	.055	.058	.099	.046	.018	.000	.041	.061	.077	.088	.088			
	750	.080	.076	.088	.087	.081	.078	.068	.067	.081	.031	.003	.035	.055	.061	.071	.076	.080			
	900	.078	.071	.087	.085	.074	.065	.054	.068	.061	.010	.009	.035	.055	.061	.071	.076				
.500	375	.076	.074	.086	.088	.075	.067	.061	.050	.099	.055	.028	.007	.055	.049	.065	.067	.066			
	685	.076	.071	.086	.083	.076	.068	.066	.053	.096	.056	.028	.008	.059	.070	.073	.073	.076			
	900	.078	.077	.086	.087	.076	.069	.063	.063	.041	.003	.038	.040	.055	.068	.070	.070	.066			
	103	1.360	1.171	1.001	.812	.639	.503	.355	.205	.015	.045	.070	.131	.210	.347	.498	.504	.504			
	331	1.581	1.252	.998	.806	.624	.519	.388	.246	.010	.043	.063	.112	.207	.358	.476	.558	.576			
	378	1.184	.997	.864	.667	.501	.441	.307	.197	.010	.047	.087	.104	.174	.307	.436	.587	.596			
	487	1.509	1.181	.998	.761	.587	.360	.247	.149	.008	.011	.088	.069	.121	.193	.319	.441	.536			
	798	.689	.682	.431	.988	.174	.094	.029	.011	.061	.058	.034	.043	.166	.286	.379	.416	.444			
	878	.806	.650	.498	.389	.194	.105	.039	.011	.047	.042	.034	.016	.166	.291	.379	.416	.444			
	975	.888	.637	.441	.286	.174	.093	.026	.004	.048	.030	.023	.000	.335	.578	.677	.777	.850			
.750	185	1.430	1.997	1.093	.910	.519	.565	.415	.278	.005	.025	.066	.185	.305	.487	.604	.661				
	360	1.315	1.165	1.118	.574	.538	.495	.358	.246	.017	.010	.047	.108	.208	.358	.487	.582				
	375	1.848	1.058	.947	.810	.638	.477	.338	.203	.006	.028	.068	.118	.208	.358	.476	.583				
	500	1.183	1.038	.819	.588	.530	.401	.279	.174	.014	.017	.058	.117	.208	.358	.476	.583				
	685	1.094	.954	.513	.339	.179	.301	.145	.140	.040	.019	.045	.117	.208	.358	.476	.583				
	750	1.036	.837	.718	.586	.440	.184	.018	.040	.081	.008	.031	.073	.148	.286	.382	.486				
	875	.985	.808	.582	.501	.378	.180	.086	.086	.041	.004	.031	.073	.148	.286	.382	.486				
	975	.905	.757	.597	.433	.381	.188	.049	.076	.035	.015	.036	.060	.148	.286	.382	.486				
	185	1.361	1.920	1.112	.958	.761	.896	.417	.080	.013	.016	.055	.099	.196	.307	.497	.563	.934			
	360	1.309	1.181	1.058	.941	.783	.558	.393	.187	.021	.015	.043	.088	.174	.287	.437	.564	.874			
.900	500	1.195	1.068	.905	.763	.603	.459	.307	.141	.009	.038	.015	.016	.056	.130	.260	.509	.712			
	685	1.108	.958	.820	.646	.507	.306	.164	.111	.016	.028	.003	.034	.107	.211	.296	.410	.503			
	975	1.263	1.136	1.008	.863	.681	.523	.340	.187	.028	.006	.022	.053	.130	.261	.438	.518	.851			
	185	1.198	1.057	.987	.771	.597	.450	.269	.150	.011	.023	.005	.020	.058	.164	.364	.517	.784			
	375	1.030	.900	.773	.618	.465	.333	.224	.147	.009	.023	.005	.018	.057	.164	.364	.517	.784			

TABLE I.- PRESSURE COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - Continued
 (b) $A = 2$ triangular wing, $r/s = 0.2$

y/s	z/c	$\delta_w, \delta_B = 0^\circ$											$\delta_B, \delta_w = 0^\circ$					
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°
103	-0.90	-0.85	-0.91	-0.80	-0.88	-0.69	-0.41	-0.34	-0.04	0.10	0.32	-0.08	-0.63	-0.91	-0.50	-0.68	-0.61	
231	-0.95	-0.88	-0.88	-0.76	-0.71	-0.64	-0.47	-0.30	-0.10	0.01	0.17	-0.14	-0.49	-0.73	-0.52	-0.75	-0.74	
348	-0.93	-0.86	-0.86	-0.82	-0.70	-0.63	-0.49	-0.37	-0.15	0.03	0.13	-0.09	-0.46	-0.76	-0.49	-0.75	-0.74	
455	-0.98	-0.89	-0.86	-0.73	-0.70	-0.63	-0.57	-0.41	-0.17	0.05	0.07	-0.10	-0.44	-0.76	-0.52	-0.76	-0.79	
562	-0.89	-0.86	-0.97	-0.86	-0.78	-0.82	-0.74	-0.61	-0.43	0.14	0.00	-0.07	-0.03	-0.33	-0.63	-0.54	-0.76	
670	-0.77	-0.74	-0.86	-0.78	-0.81	-0.74	-0.64	-0.51	-0.38	0.15	0.02	-0.17	-0.57	-0.82	-0.53	-0.82	-0.81	
778	-0.67	-0.65	-0.82	-0.74	-0.78	-0.69	-0.58	-0.44	-0.30	0.19	0.00	-0.15	-0.50	-0.75	-0.25	-0.76	-0.73	
886	-0.67	-0.65	-0.82	-0.74	-0.78	-0.69	-0.58	-0.44	-0.30	0.19	0.00	-0.15	-0.44	-0.75	-0.25	-0.78	-0.74	
994	-0.94	-0.89	-0.95	-0.87	-0.91	-0.85	-0.71	-0.58	-0.16	0.11	0.51	-0.07	-0.67	-0.90	-0.57	-0.76	-0.81	
109	-0.93	-0.90	-0.95	-0.88	-0.92	-0.86	-0.76	-0.64	-0.51	0.26	0.01	-0.21	-0.67	-0.94	-0.60	-0.79	-0.81	
218	-0.76	-0.84	-0.84	-0.78	-0.80	-0.76	-0.64	-0.51	0.25	0.06	0.11	-0.14	-0.67	-0.95	-0.74	-0.74	-0.87	
326	-0.86	-0.81	-0.93	-0.90	-0.94	-0.93	-0.82	-0.76	-0.63	0.37	0.25	-0.14	-0.77	-0.95	-0.84	-0.86	-0.85	
434	-0.91	-1.00	-0.98	-0.93	-0.94	-0.90	-0.82	-0.76	-0.61	0.40	0.25	-0.10	-0.85	-0.96	-0.94	-0.89	-0.85	
542	-0.86	-0.76	-0.89	-0.82	-0.89	-0.82	-0.73	-0.65	-0.53	0.37	0.29	-0.17	-0.85	-0.96	-0.94	-0.88	-0.83	
650	-0.77	-0.78	-0.89	-0.81	-0.91	-0.85	-0.76	-0.65	-0.53	0.39	0.32	-0.17	-0.85	-0.96	-0.94	-0.89	-0.83	
758	-0.66	-0.66	-0.86	-0.86	-0.88	-0.87	-0.76	-0.65	-0.53	0.40	0.32	-0.17	-0.85	-0.96	-0.94	-0.89	-0.83	
866	-0.66	-0.66	-0.86	-0.86	-0.88	-0.87	-0.76	-0.65	-0.53	0.40	0.32	-0.17	-0.85	-0.96	-0.94	-0.89	-0.83	
974	-0.55	-0.89	-0.97	-0.89	-0.91	-0.88	-0.76	-0.56	-0.20	0.06	0.57	-0.08	-0.77	-0.94	-0.67	-0.81	-0.81	
083	-0.89	-0.88	-0.97	-0.89	-0.92	-0.89	-0.78	-0.68	-0.30	0.03	0.38	-0.04	-0.80	-0.96	-0.78	-0.89	-0.89	
191	-0.87	-0.86	-0.97	-0.89	-0.93	-0.93	-0.82	-0.67	-0.38	0.13	0.21	-0.14	-0.82	-0.96	-0.81	-0.87	-0.87	
299	-0.86	-0.87	-0.97	-0.90	-0.93	-0.93	-0.83	-0.69	-0.48	0.19	0.19	-0.17	-0.81	-0.96	-0.81	-0.86	-0.86	
407	-0.87	-0.97	-0.98	-0.90	-0.95	-0.95	-0.87	-0.75	-0.47	0.27	0.10	-0.05	-0.81	-0.96	-0.81	-0.86	-0.86	
515	-0.88	-0.98	-0.98	-0.98	-0.95	-0.95	-0.86	-0.75	-0.51	0.32	0.16	-0.04	-0.81	-0.96	-0.81	-0.86	-0.86	
623	-0.81	-0.87	-0.86	-0.76	-0.82	-0.82	-0.74	-0.61	-0.37	0.08	0.06	-0.04	-0.57	-0.91	-0.66	-0.75	-0.75	
731	-0.73	-0.76	-0.86	-0.76	-0.82	-0.82	-0.74	-0.61	-0.37	0.16	0.16	-0.04	-0.69	-0.94	-0.43	-0.80	-0.80	
839	-0.76	-0.76	-0.87	-0.87	-0.89	-0.89	-0.81	-0.69	-0.34	0.16	0.16	-0.04	-0.74	-0.94	-0.43	-0.80	-0.80	
947	-0.76	-0.76	-0.87	-0.87	-0.89	-0.89	-0.81	-0.69	-0.34	0.16	0.16	-0.04	-0.74	-0.94	-0.43	-0.80	-0.80	
055	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	-0.75	0.57	0.14	-0.44	-0.75	-0.95	-0.55	-0.78	-0.77	
163	-0.80	-0.81	-0.95	-0.89	-0.92	-0.85	-0.72	-0.58	-0.18	0.10	0.57	-0.14	-0.44	-0.75	-0.55	-0.78	-0.77	
271	-0.81	-0.81	-0.98	-0.94	-0.97	-0.95	-0.85	-0.65	-0.29	0.03	0.44	-0.08	-0.44	-0.77	-0.65	-0.87	-0.77	
379	-0.79	-0.81	-0.94	-0.91	-0.92	-0.90	-0.80	-0.64	-0.24	0.11	0.31	-0.05	-0.56	-0.75	-0.49	-0.78	-0.77	
487	-0.78	-0.80	-0.93	-0.89	-0.93	-0.93	-0.82	-0.67	-0.24	0.11	0.28	-0.05	-0.57	-0.80	-0.50	-0.79	-0.77	
595	-0.75	-0.78	-0.98	-0.90	-0.91	-0.89	-0.83	-0.73	-0.57	0.05	0.28	-0.07	-0.64	-0.77	-0.51	-0.77	-0.77	
703	-0.70	-0.75	-0.90	-0.87	-0.90	-0.88	-0.81	-0.70	-0.57	0.05	0.28	-0.07	-0.64	-0.77	-0.47	-0.80	-0.77	
811	-0.70	-0.76	-0.76	-0.92	-0.90	-0.89	-0.81	-0.70	-0.57	0.05	0.28	-0.07	-0.64	-0.77	-0.47	-0.80	-0.77	
919	-0.70	-0.75	-0.90	-0.87	-0.90	-0.88	-0.81	-0.70	-0.57	0.05	0.28	-0.07	-0.64	-0.77	-0.47	-0.80	-0.77	
500	-0.70	-0.76	-0.89	-0.88	-0.92	-0.90	-0.81	-0.70	-0.57	0.14	0.25	-0.07	-0.54	-0.74	-0.49	-0.80	-0.79	
588	-0.70	-0.75	-0.90	-0.91	-0.90	-0.88	-0.88	-0.70	-0.46	0.10	0.18	-0.09	-0.77	-0.53	-0.82	-0.79	-0.79	

TABLE I.- PRESSURE COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - Continued
 (b) $A = 2$ triangular wing, $r/s = 0.2$ - Concluded

V_s	V_c	$\delta_w, \alpha_b = 0^\circ$												$\alpha_b, \delta_w = 0^\circ$							
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°			
.025	103	1.236	1.074	.897	.785	.545	.408	.284	.152	.095	.059	.038	.063	.138	.209	.311	.494	.695			
	1131	1.194	1.044	.833	.667	.499	.350	.231	.125	.075	.040	.017	.057	.109	.184	.289	.457	.645			
	1122	1.184	1.048	.776	.619	.461	.356	.239	.100	.058	.032	.013	.042	.082	.147	.240	.391	.561			
	1130	1.193	1.033	.664	.746	.581	.331	.185	.079	.046	.026	.007	.035	.073	.128	.211	.314	.514			
	1144	1.190	1.051	.716	.513	.348	.228	.139	.063	.034	.018	.007	.086	.059	.111	.197	.326	.476			
	1148	1.174	1.044	.485	.346	.228	.137	.071	.007	.020	-	.004	.000	.080	.064	.104	.173	.278	.478		
	1178	1.196	1.049	.688	.457	.369	.241	.141	.061	-.004	-	.013	.010	.041	.093	.159	.299	.443			
	1176	1.196	1.090	.761	.461	.345	.212	.039	.011	.000	.000	.000	.026	.057	.110	.189	.283	.470			
	104	1.006	1.047	.888	.741	.583	.439	.384	.203	.144	.094	.051	.118	.165	.235	.330	.499	.673			
	1139	1.108	1.087	.836	.661	.511	.373	.263	.168	.105	.064	.029	.076	.119	.184	.281	.433	.609			
.250	1154	1.169	1.034	.636	.488	.359	.248	.148	.087	.047	.017	.017	.041	.089	.152	.244	.408	.583			
	1100	1.198	1.068	.717	.572	.436	.319	.201	.090	.047	.017	.011	.086	.065	.122	.208	.344	.508			
	1175	1.193	1.088	.837	.688	.551	.405	.294	.148	.070	.044	.008	.010	.015	.051	.103	.186	.319	.476		
	1175	1.193	1.074	.601	.467	.346	.235	.150	.061	.037	.007	-.001	.016	.045	.103	.176	.305	.479			
	1175	1.198	1.066	.660	.461	.351	.231	.158	.049	.019	.001	-.015	.011	.048	.104	.179	.305	.444			
	1169	1.193	1.034	.693	.507	.343	.238	.134	.046	.017	-.001	.017	.011	.039	.144						
	1155	1.083	1.093	.836	.661	.573	.449	.338	.228	.164	.110	.057	.129	.168	.256	.349	.561				
	1150	1.047	.972	.911	.686	.535	.401	.291	.179	.128	.078	.038	.095	.136	.209	.311	.451	.685			
	1170	1.070	.874	.805	.689	.549	.398	.280	.156	.105	.059	.026	.169	.115	.174	.219	.384	.584			
	1165	1.081	.976	.807	.651	.507	.370	.258	.136	.085	.043	.013	.043	.092	.164	.240	.404	.576			
.500	1163	1.063	.877	.757	.515	.467	.330	.200	.109	.069	.037	.017	.010	.026	.075	.136	.227	.372	.538		
	1121	1.181	.880	.740	.562	.440	.309	.199	.093	.060	.031	.017	.019	.068	.132	.213	.359	.528			
	1100	1.096	.926	.709	.561	.417	.299	.185	.066	.031	.017	.006	.010	.040	.131	.174	.316	.501			
	1118	1.075	.686	.548	.400	.269	.171	.068	.037	.005	-.016	.007	.042	.105	.189						
	1173	.970	.834	.786	.640	.503	.395	.269	.199	.138	.057	.143	.181	.241	.304	.404	.560				
	1153	1.012	.861	.766	.636	.491	.371	.246	.186	.111	.044	.142	.194	.276	.383	.488	.679				
	1166	1.046	.987	.742	.506	.467	.336	.201	.141	.087	.031	.103	.144	.240	.340	.489	.685				
	1164	1.038	.984	.751	.599	.461	.317	.179	.118	.071	.028	.083	.114	.217	.317	.473	.688				
	1107	1.059	.908	.684	.541	.407	.286	.147	.098	.041	.008	.050	.097	.171	.279	.438	.688				
	1104	.867	.716	.589	.466	.341	.237	.128	.066	.026	-.003	.003	.050	.145	.239	.388	.561				
.750	1121	1.090	.865	.740	.626	.498	.374	.241	.163	.082	.025	.101	.147	.229	.384	.540	.697				
	1139	1.086	.837	.709	.574	.449	.331	.198	.134	.070	.010	.052	.149	.229	.349	.501	.660				

TABLE I.- PRESSURE COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - Concluded
 (c) $A = 2$ rectangular wing, $r/s = 0.2$

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TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS
 (a) $A = 4$ triangular wing, $r/s = 0.2$

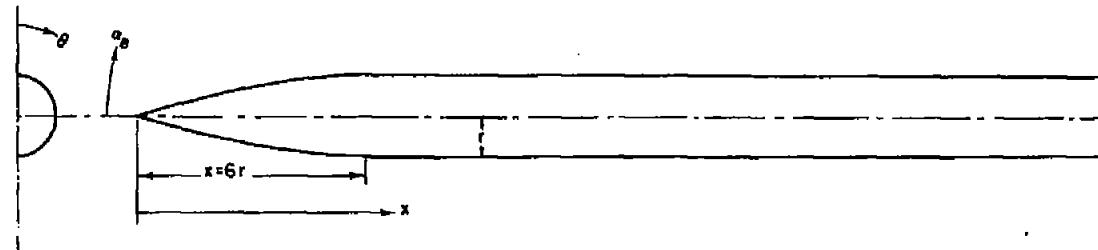


TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (a) $A = 4$ triangular wing, $r/s = 0.2$ - Concluded

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (b) A = 2 triangular wing, $r/s = 0.2$

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (b) $A = 2$ triangular wing, $r/s = 0.2$ - Concluded

θ	x/r	$\delta_w, \alpha_B = 0^\circ$												$\alpha_B, \delta_w = 0^\circ$						
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°		
120°	1134	-0.023	-0.024	-0.022	-0.023	-0.023	-0.023	-0.023	-0.023	-0.023	-0.023	-0.023	-0.025	-0.027	-0.026	-0.026	-0.026	-0.026	0.011	108
	1259	-0.020	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019	-0.015	-0.015	-0.014	-0.014	-0.014	-0.014	0.013	118
	1384	-0.024	-0.025	-0.015	-0.015	-0.018	-0.014	-0.015	-0.015	-0.015	-0.015	-0.015	-0.009	-0.009	-0.014	-0.014	-0.014	-0.014	0.013	143
	1509	-0.022	-0.023	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.014	-0.014	-0.005	-0.005	-0.005	-0.005	0.019	151
	1634	-0.026	-0.024	-0.014	-0.016	-0.013	-0.009	-0.013	-0.017	-0.017	-0.013	-0.013	-0.008	-0.008	-0.004	-0.004	-0.004	-0.004	0.026	156
	1756	-0.028	-0.029	-0.010	-0.010	-0.008	-0.009	-0.028	-0.028	-0.028	-0.016	-0.020	-0.018	-0.018	-0.011	-0.013	-0.013	-0.013	0.026	157
	1884	-0.026	-0.028	-0.009	-0.009	-0.008	-0.008	-0.024	-0.024	-0.024	-0.012	-0.029	-0.029	-0.009	-0.011	-0.011	-0.011	-0.011	0.026	157
	2009	-0.021	-0.029	-0.003	-0.003	-0.003	-0.003	-0.057	-0.057	-0.048	-0.014	-0.008	-0.014	-0.008	-0.011	-0.011	-0.011	-0.011	0.025	158
	2134	-0.026	-0.024	-0.008	-0.008	-0.005	-0.005	-0.021	-0.021	-0.016	-0.014	-0.016	-0.016	-0.009	-0.009	-0.006	-0.006	-0.006	0.025	159
	2259	-0.027	-0.024	-0.006	-0.006	-0.005	-0.005	-0.023	-0.023	-0.018	-0.013	-0.018	-0.018	-0.013	-0.013	-0.006	-0.006	-0.006	0.026	159
150°	1384	-0.024	-0.024	-0.002	-0.002	-0.005	-0.005	-0.021	-0.021	-0.014	-0.014	-0.014	-0.014	-0.012	-0.012	-0.006	-0.006	-0.006	0.025	160
	1539	-0.020	-0.021	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.025	160
	1634	-0.026	-0.026	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.025	160
	1756	-0.028	-0.028	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.025	160
	1884	-0.026	-0.028	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.025	160
	2009	-0.028	-0.028	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.025	160
	2134	-0.026	-0.026	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.025	160
	2259	-0.027	-0.027	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.025	160
	2384	-0.028	-0.028	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.025	160
	2509	-0.029	-0.029	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.025	160
165°	1384	-0.024	-0.024	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.026	166
	1539	-0.020	-0.021	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.026	166
	1634	-0.026	-0.026	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.026	166
	1756	-0.028	-0.028	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.026	166
	1884	-0.026	-0.028	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.026	166
	2009	-0.028	-0.028	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.026	166
	2134	-0.026	-0.026	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.026	166
	2259	-0.027	-0.027	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.026	166
	2384	-0.028	-0.028	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.026	166
	2509	-0.029	-0.029	-0.001	-0.001	-0.001	-0.001	-0.021	-0.021	-0.011	-0.011	-0.011	-0.011	-0.009	-0.009	-0.006	-0.006	-0.006	0.026	166
174°	1384	-0.024	-0.024	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.019	-0.018	-0.018	-0.019	-0.020	-0.020	-0.013	-0.013	-0.013	0.026	175
	1539	-0.021	-0.021	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.019	-0.018	-0.018	-0.019	-0.020	-0.020	-0.015	-0.015	-0.015	0.026	175
	1634	-0.026	-0.026	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.019	-0.018	-0.018	-0.019	-0.020	-0.020	-0.016	-0.016	-0.016	0.026	175
	1756	-0.028	-0.028	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.019	-0.018	-0.018	-0.019	-0.020	-0.020	-0.017	-0.017	-0.017	0.026	175
	1884	-0.026	-0.028	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.019	-0.018	-0.018	-0.019	-0.020	-0.020	-0.017	-0.017	-0.017	0.026	175
	2009	-0.028	-0.028	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.019	-0.018	-0.018	-0.019	-0.020	-0.020	-0.017	-0.017	-0.017	0.026	175
	2134	-0.026	-0.026	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.019	-0.018	-0.018	-0.019	-0.020	-0.020	-0.017	-0.017	-0.017	0.026	175
	2259	-0.027	-0.027	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.019	-0.018	-0.018	-0.019	-0.020	-0.020	-0.017	-0.017	-0.017	0.026	175
	2384	-0.028	-0.028	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.019	-0.018	-0.018	-0.019	-0.020	-0.020	-0.017	-0.017	-0.017	0.026	175
	2509	-0.029	-0.029	-0.017	-0.017	-0.018	-0.019	-0.020	-0.020	-0.019	-0.018	-0.018	-0.019	-0.020	-0.020	-0.017	-0.017	-0.017	0.026	175

TABLE II.-- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (c) $A = 1$ triangular wing, $r/s = 0.2$

θ	x/r	$\delta_w, \alpha_B = 0^\circ$												$\alpha_B, \delta_w = 0^\circ$						
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°		
6°	6.94	-0.028	-0.027	-0.026	-0.025	-0.025	-0.027	-0.027	-0.029	-0.028	-0.027	-0.027	-0.026	-0.037	-0.039	-0.050	-0.047	-0.079	-0.067	
	8.37	-0.022	-0.022	-0.022	-0.023	-0.022	-0.022	-0.021	-0.022	-0.021	-0.019	-0.019	-0.018	-0.032	-0.041	-0.049	-0.078	-0.066		
	9.81	-0.015	-0.017	-0.017	-0.018	-0.017	-0.017	-0.017	-0.017	-0.018	-0.014	-0.014	-0.014	-0.023	-0.030	-0.036	-0.053	-0.077	-0.091	
	11.95	0.005	-0.016	-0.019	-0.019	-0.017	-0.017	-0.017	-0.017	-0.018	-0.014	-0.014	-0.014	-0.021	-0.029	-0.034	-0.057	-0.087	-0.095	
	12.69	0.009	-0.014	-0.018	-0.018	-0.017	-0.017	-0.017	-0.017	-0.018	-0.014	-0.014	-0.014	-0.023	-0.031	-0.036	-0.057	-0.084	-0.096	
	14.12	0.010	-0.014	-0.016	-0.017	-0.017	-0.017	-0.017	-0.017	-0.018	-0.014	-0.014	-0.014	-0.023	-0.034	-0.037	-0.058	-0.084	-0.096	
	15.56	0.006	-0.016	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.014	-0.014	-0.014	-0.021	-0.030	-0.034	-0.057	-0.087	-0.098	
	17.00	0.014	-0.015	-0.016	-0.017	-0.017	-0.017	-0.017	-0.018	-0.018	-0.014	-0.014	-0.014	-0.021	-0.031	-0.034	-0.056	-0.087	-0.096	
	18.44	-0.005	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.014	-0.014	-0.014	-0.021	-0.030	-0.034	-0.056	-0.087	-0.098	
	19.87	-0.006	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.014	-0.014	-0.014	-0.021	-0.030	-0.034	-0.056	-0.087	-0.098	
	21.31	-0.005	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.014	-0.014	-0.014	-0.021	-0.030	-0.034	-0.056	-0.087	-0.098	
	22.75	-0.006	-0.017	-0.017	-0.017	-0.018	-0.018	-0.018	-0.019	-0.019	-0.015	-0.015	-0.015	-0.022	-0.031	-0.035	-0.057	-0.087	-0.098	
	24.19	-0.006	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.014	-0.014	-0.014	-0.021	-0.030	-0.034	-0.056	-0.087	-0.098	
	25.53	0.014	-0.016	-0.017	-0.017	-0.018	-0.018	-0.018	-0.019	-0.019	-0.015	-0.015	-0.015	-0.021	-0.030	-0.034	-0.056	-0.087	-0.098	
15°	6.94	-0.028	-0.028	-0.028	-0.029	-0.029	-0.027	-0.027	-0.028	-0.028	-0.027	-0.027	-0.027	-0.035	-0.047	-0.059	-0.081	-0.082		
	8.37	-0.022	-0.022	-0.022	-0.023	-0.023	-0.022	-0.022	-0.023	-0.023	-0.022	-0.022	-0.022	-0.032	-0.053	-0.072	-0.083	-0.085		
	9.81	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.017	-0.018	-0.018	-0.016	-0.016	-0.016	-0.025	-0.047	-0.074	-0.084	-0.089		
	11.25	0.005	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.025	-0.047	-0.073	-0.084	-0.089		
	12.69	0.011	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.026	-0.048	-0.073	-0.084	-0.089		
	14.12	0.012	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.026	-0.049	-0.074	-0.084	-0.089		
	15.56	0.004	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.026	-0.048	-0.073	-0.084	-0.089		
	17.00	0.011	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.026	-0.049	-0.073	-0.084	-0.089		
	18.44	0.016	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.026	-0.049	-0.074	-0.085	-0.090		
	19.87	-0.006	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.026	-0.049	-0.074	-0.085	-0.090		
	21.31	-0.005	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.026	-0.049	-0.073	-0.084	-0.089		
	22.75	-0.006	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.026	-0.049	-0.073	-0.084	-0.089		
	24.19	-0.006	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.026	-0.049	-0.073	-0.084	-0.089		
	25.53	0.001	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.026	-0.049	-0.073	-0.084	-0.089		
30°	6.94	-0.032	-0.034	-0.033	-0.034	-0.038	-0.038	-0.035	-0.033	-0.032	-0.031	-0.031	-0.031	-0.043	-0.058	-0.067	-0.087	-0.087		
	8.37	-0.024	-0.026	-0.025	-0.025	-0.028	-0.028	-0.026	-0.027	-0.026	-0.026	-0.026	-0.026	-0.036	-0.053	-0.063	-0.086	-0.086		
	9.81	-0.019	-0.019	-0.019	-0.019	-0.020	-0.020	-0.019	-0.020	-0.020	-0.017	-0.017	-0.017	-0.028	-0.051	-0.062	-0.085	-0.088		
	11.25	0.016	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
	12.69	0.011	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
	14.12	0.012	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
	15.56	0.007	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
	17.00	0.010	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
	18.44	0.017	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
	19.87	-0.004	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
	21.31	-0.004	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
	22.75	-0.005	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
	24.19	-0.005	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
	25.53	0.009	-0.016	-0.016	-0.016	-0.017	-0.017	-0.017	-0.018	-0.018	-0.015	-0.015	-0.015	-0.028	-0.051	-0.062	-0.085	-0.088		
60°	6.94	-0.026	-0.030	-0.028	-0.031	-0.028	-0.028	-0.028	-0.029	-0.028	-0.018	-0.018	-0.018	-0.027	-0.037	-0.051	-0.062	-0.087		
	8.37	-0.026	-0.026	-0.026	-0.027	-0.024	-0.027	-0.024	-0.024	-0.024	-0.024	-0.024	-0.024	-0.026	-0.037	-0.051	-0.062	-0.087		
	9.81	-0.025	-0.026	-0.026	-0.026	-0.026	-0.027	-0.024	-0.024	-0.024	-0.024	-0.024	-0.024	-0.026	-0.037	-0.051	-0.062	-0.087		
	11.25	0.023	-0.026	-0.026	-0.026	-0.027	-0.024	-0.024	-0.025	-0.025	-0.024	-0.024	-0.024	-0.026	-0.037	-0.051	-0.062	-0.087		
	12.69	0.011	-0.026	-0.026	-0.026	-0.027	-0.024	-0.024	-0.025	-0.025	-0.024	-0.024	-0.024	-0.026	-0.037	-0.051	-0.062	-0.087		
	14.12	0.012	-0.026	-0.026	-0.026	-0.027	-0.024	-0.024	-0.025	-0.025	-0.024	-0.024	-0.024	-0.026	-0.037	-0.051	-0.062	-0.087		
	15.56	0.006	-0.026	-0.026	-0.026	-0.027	-0.024	-0.024	-0.025	-0.025	-0.024	-0.024	-0.024	-0.026	-0.037	-0.051	-0.062	-0.087		
	17.00	0.010	-0.026	-0.026	-0.026	-0.027	-0.024	-0.024	-0.025	-0.025	-0.024	-0.024	-0.024	-0.026	-0.037	-0.051	-0.062	-0.087		
	18.44	0.017	-0.026	-0.026	-0.026	-0.027	-0.024	-0.024	-0.025	-0.025	-0.024	-0.024	-0.024	-0.026	-0.037	-0.051	-0.062	-0.087		
	19.87	-0.005	-0.026	-0.026	-0.026	-0.027	-0.024	-0.024	-0.025	-0.025	-0.024	-0.024	-0.024	-0.026	-0.037	-0.051	-0.062	-0.087		
	21.31	-0.005	-0.026	-0.026	-0.026	-0.02														

TABLE III.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (c) $A = 1$ triangular wing, $r/s = 0.2$ - Concluded

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TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
(d) $A = 1$ triangular wing, $r/s = 0.4$

θ	x/r	$\delta_w, \alpha_b = 0^\circ$											$\alpha_b, \delta_w = 0^\circ$						
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°	
6°	6.94	- .023	- .028	- .027	- .024	- .029	- .029	.001	- .028	- .026	- .031	- .039	- .047	- .047	- .079	- .077			
	8.37	- .018	- .023	- .020	- .017	- .021	- .033	- .003	- .021	- .019	- .028	- .031	- .038	- .045	- .077	- .078			
	9.81	- .013	- .017	- .017	- .014	- .017	- .018	- .004	- .018	- .016	- .015	- .018	- .026	- .049	- .075	- .081			
	11.25	- .013	- .019	- .018	- .015	- .019	- .018	- .004	- .018	- .017	- .019	- .017	- .016	- .055	- .075	- .076			
	12.69	- .012	- .016	- .015	- .012	- .017	- .021	- .007	- .015	- .014	- .016	- .018	- .014	- .057	- .071	- .076			
	14.12	- .006	- .010	- .010	- .005	- .011	- .017	- .006	- .009	- .008	- .011	- .011	- .020	- .061	- .076	- .080			
	15.56	- .094	- .033	- .036	- .042	- .015	- .010	- .007	- .005	- .003	- .008	- .010	- .021	- .057	- .080	- .078			
	17.00	- .157	- .113	- .063	- .080	- .020	- .023	- .007	- .005	- .003	- .008	- .005	- .006	- .067	- .074	- .080			
	18.44	- .087	- .048	- .057	- .053	- .023	- .019	- .004	- .006	- .003	- .008	- .004	- .005	- .069	- .078				
	19.87	- .069	- .075	- .056	- .059	- .023	- .018	- .006	- .004	- .002	- .007	- .011	- .030	- .067	- .069	- .078			
	21.31	- .047	- .044	- .037	- .026	- .032	- .027	- .001	- .016	- .011	- .014	- .011	- .021	- .043	- .051	- .059			
	22.75	- .018	- .020	- .016	- .014	- .018	- .009	- .005	- .008	- .003	- .007	- .014	- .017	- .029	- .043	- .056			
	24.19	- .015	- .005	- .006	- .010	- .007	- .005	- .005	- .005	- .007	- .014	- .010	- .006	- .004	- .008	- .036			
	25.63	.030	.024	.020	.028	.017	.013	.018	.000	.018	.021	.018	.010	.007	.025	.055	.081		
15°	6.94	- .025	- .027	- .027	- .025	- .030	- .029	.001	- .028	- .027	- .026	- .028	- .037	- .045	- .069	- .084	- .076		
	8.37	- .018	- .020	- .018	- .021	- .021	- .021	- .002	- .021	- .019	- .019	- .021	- .033	- .073	- .083	- .078			
	9.81	- .015	- .020	- .018	- .015	- .019	- .020	- .004	- .019	- .017	- .020	- .030	- .045	- .072	- .076	- .079			
	11.25	- .019	- .023	- .023	- .015	- .023	- .028	- .008	- .023	- .023	- .023	- .026	- .045	- .073	- .070	- .068			
	12.69	- .013	- .017	- .015	- .013	- .017	- .018	- .004	- .018	- .015	- .015	- .028	- .039	- .067	- .070	- .075			
	14.12	- .006	- .010	- .009	- .006	- .013	- .011	- .005	- .014	- .010	- .009	- .017	- .034	- .066	- .070	- .079			
	15.56	- .115	- .087	- .089	- .085	- .056	- .010	- .008	- .006	- .006	- .007	- .017	- .034	- .056	- .079	- .080			
	17.00	- .147	- .101	- .053	- .059	- .026	- .023	- .009	- .004	- .003	- .008	- .014	- .042	- .084	- .080	- .080			
	18.44	- .027	.048	- .060	- .061	- .037	- .028	- .016	- .008	- .004	- .003	- .012	- .048	- .065	- .077	- .080			
	19.87	- .088	- .068	- .069	- .043	- .037	- .031	- .027	- .001	- .016	- .013	- .012	- .009	- .084	- .047	- .066	- .081		
	21.31	- .050	- .047	- .039	- .034	- .031	- .025	- .016	- .018	- .018	- .014	- .011	- .028	- .044	- .069	- .076			
	22.75	- .016	- .020	- .020	- .020	- .014	- .015	- .016	- .011	- .008	- .009	- .005	- .019	- .014	- .029	- .058			
	24.19	- .013	- .001	- .001	- .005	- .003	- .003	- .001	- .008	- .006	- .009	- .012	- .009	- .003	- .020	- .041			
	25.63	.026	.018	.019	.022	.017	.012	.010	.001	.011	.022	.017	.005	.015	.020	.070	.068		
30°	6.94	- .089	- .033	- .038	- .031	- .034	- .034	- .006	- .038	- .028	- .033	- .035	- .044	- .057	- .083	- .090	- .079		
	8.37	- .019	- .019	- .018	- .018	- .018	- .025	- .028	- .019	- .021	- .019	- .036	- .055	- .083	- .079	- .077			
	9.81	- .015	- .019	- .018	- .016	- .016	- .020	- .019	- .019	- .018	- .023	- .032	- .067	- .089	- .073	- .075			
	11.25	- .013	- .018	- .018	- .017	- .016	- .018	- .018	- .006	- .018	- .016	- .026	- .049	- .064	- .072	- .074			
	12.69	- .014	- .018	- .018	- .017	- .016	- .018	- .018	- .006	- .018	- .015	- .027	- .064	- .074	- .075	- .075			
	14.12	- .005	- .009	- .007	- .006	- .008	- .009	- .017	- .017	- .007	- .006	- .010	- .035	- .061	- .071	- .075			
	15.56	- .120	- .103	- .134	- .065	- .007	- .017	- .004	- .004	- .005	- .003	- .011	- .035	- .061	- .071	- .075			
	17.00	- .157	- .103	- .001	- .006	- .030	- .027	- .019	- .004	- .005	- .001	- .011	- .037	- .064	- .070	- .080			
	18.44	- .049	- .965	- .071	- .067	- .035	- .025	- .019	- .001	- .013	- .006	- .003	- .014	- .054	- .069	- .085			
	19.87	- .076	- .067	- .046	- .041	- .037	- .035	- .024	- .008	- .013	- .006	- .003	- .014	- .045	- .066	- .084			
	21.31	- .054	- .046	- .038	- .031	- .028	- .025	- .018	- .008	- .008	- .005	- .013	- .040	- .058	- .069				
	22.75	- .012	- .022	- .021	- .018	- .017	- .013	- .005	- .009	- .005	- .003	- .012	- .015	- .039	- .063				
	24.19	- .012	- .003	- .001	- .007	- .006	- .006	- .007	- .006	- .006	- .010	- .011	- .012	- .025	- .056				
	25.63	.031	.013	.018	.014	.006	.007	.002	.002	.002	.011	.013	.011	.007	.025	.056			
60°	6.94	- .027	- .029	- .029	- .029	- .030	- .029	- .001	- .029	- .028	- .033	- .050	- .075	- .086	- .083	- .078			
	8.37	- .024	- .027	- .027	- .028	- .026	- .029	- .001	- .028	- .026	- .032	- .050	- .074	- .078	- .077				
	9.81	- .024	- .026	- .028	- .024	- .027	- .028	- .000	- .028	- .026	- .030	- .048	- .065	- .068	- .071	- .073			
	11.25	- .018	- .028	- .028	- .020	- .022	- .022	- .002	- .028	- .020	- .023	- .037	- .054	- .068	- .072	- .074			
	12.69	- .013	- .016	- .016	- .016	- .016	- .018	- .003	- .018	- .016	- .021	- .029	- .044	- .061	- .073	- .074			
	14.12	- .013	- .014	- .013	- .014	- .015	- .014	- .005	- .013	- .007	- .015	- .029	- .048	- .065	- .073	- .091			
	15.56	- .133	- .129	- .111	- .085	- .082	- .081	- .056	- .003	- .003	- .003	- .002	- .013	- .038	- .063	- .080			
	17.00	- .125	.019	.011	.026	.016	.026	.054	- .003	- .003	- .012	- .007	- .019	- .041	- .066	- .078			
	18.44	- .083	.091	.087	.073	.053	.067	.051	- .001	- .001	- .011	- .026	- .034	- .068	- .074	- .081			
	19.87	- .059	.065	.060	.054	.051	.058	.048	- .003	- .003	- .001	- .001	- .009	- .045	- .070	- .065			
	21.31	- .038	.049	.050	.041	.037	.038	.030	- .001	- .001	- .001	- .001	- .009	- .048	- .064	- .069			
	22.75	- .028	.020	.018	.016	.022	.038	.027	- .005	- .005	- .007	- .007	- .008	- .043	- .060	- .067			
	24.19	- .006	.010	.010	.011	.014	.018	.011	- .006	- .006	- .006	- .009	- .005	- .011	- .041	- .048			
	25.63	.015	.017	.013	.016	.014	.014	.018	- .001	- .006	- .009	- .007	- .007	- .011	- .025	- .052			

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
(e) $A = 2/3$ triangular wing, $r/s = 0.4$

θ	x/s	$\delta_w, \delta_B = 0^\circ$										$\delta_B, \delta_w = 0^\circ$							
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°	
6°	6.94	-0.28	-0.33	-0.30	-0.28	-0.29	-0.30	-0.27	-0.29	-0.30	-0.26	-0.29	-0.42	-0.45	-0.47	-0.46	-0.48	-0.46	
	8.37	-0.21	-0.24	-0.25	-0.22	-0.22	-0.25	-0.20	-0.21	-0.20	-0.21	-0.21	-0.31	-0.36	-0.38	-0.50	-0.78	-0.83	
	9.81	-0.15	-0.21	-0.20	-0.17	-0.17	-0.20	-0.17	-0.17	-0.20	-0.14	-0.19	-0.26	-0.34	-0.36	-0.51	-0.76	-0.89	
	11.25	-0.15	-0.20	-0.16	-0.17	-0.17	-0.19	-0.16	-0.17	-0.19	-0.14	-0.19	-0.21	-0.24	-0.26	-0.57	-0.78	-0.82	
	12.69	-0.15	-0.16	-0.14	-0.15	-0.15	-0.17	-0.15	-0.17	-0.18	-0.14	-0.17	-0.19	-0.24	-0.26	-0.57	-0.78	-0.79	
	14.13	-0.15	-0.14	-0.16	-0.10	-0.10	-0.15	-0.15	-0.07	-0.15	-0.16	-0.16	-0.11	-0.14	-0.16	-0.60	-0.88	-0.85	
	15.56	-0.15	-0.14	-0.16	-0.10	-0.10	-0.15	-0.15	-0.07	-0.15	-0.16	-0.16	-0.11	-0.14	-0.16	-0.63	-0.88	-0.84	
	17.00	-0.15	-0.15	-0.16	-0.07	-0.07	-0.14	-0.15	-0.08	-0.15	-0.16	-0.16	-0.11	-0.14	-0.16	-0.63	-0.88	-0.86	
	18.44	-0.15	-0.14	-0.16	-0.07	-0.07	-0.14	-0.15	-0.08	-0.15	-0.16	-0.16	-0.11	-0.14	-0.16	-0.63	-0.88	-0.86	
	19.87	-0.15	-0.14	-0.16	-0.07	-0.07	-0.14	-0.15	-0.08	-0.15	-0.16	-0.16	-0.11	-0.14	-0.16	-0.63	-0.88	-0.86	
15°	21.31	-0.15	-0.14	-0.16	-0.07	-0.07	-0.14	-0.15	-0.08	-0.15	-0.16	-0.16	-0.11	-0.14	-0.16	-0.63	-0.88	-0.86	
	22.75	-0.15	-0.17	-0.28	-0.13	-0.13	-0.14	-0.15	-0.06	-0.15	-0.16	-0.16	-0.11	-0.14	-0.16	-0.63	-0.88	-0.86	
	24.19	-0.10	-0.11	-0.14	-0.10	-0.10	-0.15	-0.10	-0.07	-0.15	-0.16	-0.16	-0.11	-0.14	-0.16	-0.64	-0.88	-0.86	
	25.62	-0.15	-0.15	-0.15	-0.12	-0.12	-0.15	-0.15	-0.15	-0.15	-0.12	-0.11	-0.13	-0.15	-0.16	-0.64	-0.88	-0.86	
	6.94	-0.27	-0.32	-0.31	-0.30	-0.28	-0.31	-0.27	-0.29	-0.30	-0.26	-0.27	-0.38	-0.45	-0.48	-0.69	-0.83	-0.83	
	8.37	-0.22	-0.27	-0.27	-0.23	-0.23	-0.27	-0.22	-0.24	-0.24	-0.21	-0.21	-0.30	-0.36	-0.43	-0.73	-0.85	-0.84	
	9.81	-0.16	-0.23	-0.21	-0.17	-0.17	-0.22	-0.16	-0.18	-0.18	-0.15	-0.15	-0.26	-0.32	-0.39	-0.73	-0.78	-0.85	
	11.25	-0.16	-0.24	-0.22	-0.17	-0.17	-0.21	-0.16	-0.17	-0.17	-0.15	-0.15	-0.26	-0.32	-0.39	-0.67	-0.71	-0.79	
	14.13	-0.16	-0.18	-0.18	-0.13	-0.13	-0.15	-0.17	-0.09	-0.17	-0.17	-0.17	-0.13	-0.21	-0.35	-0.66	-0.74	-0.81	
	15.56	-0.16	-0.18	-0.18	-0.13	-0.13	-0.15	-0.17	-0.09	-0.17	-0.17	-0.17	-0.13	-0.21	-0.35	-0.66	-0.74	-0.81	
30°	17.00	-0.16	-0.1	-0.46	-0.07	-0.07	-0.17	-0.17	-0.08	-0.17	-0.17	-0.17	-0.12	-0.17	-0.21	-0.67	-0.84	-0.87	
	18.44	-0.16	-0.1	-0.46	-0.07	-0.07	-0.17	-0.17	-0.08	-0.17	-0.17	-0.17	-0.12	-0.17	-0.21	-0.67	-0.84	-0.87	
	19.87	-0.16	-0.1	-0.46	-0.07	-0.07	-0.17	-0.17	-0.08	-0.17	-0.17	-0.17	-0.12	-0.17	-0.21	-0.67	-0.84	-0.87	
	21.31	-0.16	-0.1	-0.46	-0.07	-0.07	-0.17	-0.17	-0.08	-0.17	-0.17	-0.17	-0.12	-0.17	-0.21	-0.67	-0.84	-0.87	
	22.75	-0.16	-0.1	-0.46	-0.07	-0.07	-0.17	-0.17	-0.08	-0.17	-0.17	-0.17	-0.12	-0.17	-0.21	-0.67	-0.84	-0.87	
	24.19	-0.16	-0.1	-0.46	-0.07	-0.07	-0.17	-0.17	-0.08	-0.17	-0.17	-0.17	-0.12	-0.17	-0.21	-0.67	-0.84	-0.87	
	25.62	-0.16	-0.1	-0.46	-0.07	-0.07	-0.17	-0.17	-0.08	-0.17	-0.17	-0.17	-0.12	-0.17	-0.21	-0.67	-0.84	-0.87	
	6.94	-0.38	-0.37	-0.34	-0.38	-0.32	-0.35	-0.34	-0.35	-0.34	-0.33	-0.34	-0.44	-0.48	-0.55	-0.87	-0.87	-0.87	
	8.37	-0.23	-0.28	-0.21	-0.18	-0.18	-0.21	-0.16	-0.18	-0.18	-0.15	-0.15	-0.36	-0.46	-0.56	-0.84	-0.84	-0.84	
	9.81	-0.16	-0.23	-0.21	-0.18	-0.18	-0.21	-0.16	-0.17	-0.17	-0.15	-0.15	-0.36	-0.46	-0.56	-0.84	-0.84	-0.84	
60°	11.25	-0.16	-0.21	-0.21	-0.19	-0.19	-0.21	-0.17	-0.18	-0.18	-0.15	-0.15	-0.36	-0.46	-0.56	-0.84	-0.84	-0.84	
	14.13	-0.16	-0.11	-0.10	-0.10	-0.07	-0.07	-0.07	-0.08	-0.08	-0.05	-0.05	-0.36	-0.46	-0.56	-0.84	-0.84	-0.84	
	15.56	-0.16	-0.14	-0.14	-0.13	-0.13	-0.15	-0.14	-0.08	-0.14	-0.14	-0.14	-0.11	-0.17	-0.24	-0.84	-0.84	-0.84	
	17.00	-0.16	-0.14	-0.14	-0.13	-0.13	-0.15	-0.14	-0.08	-0.14	-0.14	-0.14	-0.11	-0.17	-0.24	-0.84	-0.84	-0.84	
	18.44	-0.16	-0.14	-0.14	-0.13	-0.13	-0.15	-0.14	-0.08	-0.14	-0.14	-0.14	-0.11	-0.17	-0.24	-0.84	-0.84	-0.84	
	19.87	-0.16	-0.14	-0.14	-0.13	-0.13	-0.15	-0.14	-0.08	-0.14	-0.14	-0.14	-0.11	-0.17	-0.24	-0.84	-0.84	-0.84	
	21.31	-0.16	-0.14	-0.14	-0.13	-0.13	-0.15	-0.14	-0.08	-0.14	-0.14	-0.14	-0.11	-0.17	-0.24	-0.84	-0.84	-0.84	
	22.75	-0.16	-0.14	-0.14	-0.13	-0.13	-0.15	-0.14	-0.08	-0.14	-0.14	-0.14	-0.11	-0.17	-0.24	-0.84	-0.84	-0.84	
	24.19	-0.16	-0.14	-0.14	-0.13	-0.13	-0.15	-0.14	-0.08	-0.14	-0.14	-0.14	-0.11	-0.17	-0.24	-0.84	-0.84	-0.84	
	25.62	-0.16	-0.14	-0.14	-0.13	-0.13	-0.15	-0.14	-0.08	-0.14	-0.14	-0.14	-0.11	-0.17	-0.24	-0.84	-0.84	-0.84	

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (e) $A = 2/3$ triangular wing, $r/s = 0.4$ - Concluded

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (f) $A = \frac{3}{8}$ triangular wing, $r/s = 0.4$

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (f) $A = 3/8$ triangular wing, $r/s = 0.4$ - Concluded

θ	x_f	$\delta_W, a_B = 0^\circ$													$a_B, \delta_W = 0^\circ$							
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°				
60°	-0.38	-0.33	-0.50	-0.89	-0.99	-0.31	-0.32	-0.31	-0.29	-0.28	-0.27	-0.27	-0.23	-0.13	-0.07	-0.46	-0.63	-0.80	-0.99	-1.05	-1.10	
	-0.37	-0.30	-0.53	-0.59	-0.85	-0.87	-0.14	-0.27	-0.28	-0.29	-0.28	-0.27	-0.26	-0.20	-0.13	-0.05	-0.44	-0.59	-0.73	-0.85	-0.95	-1.04
	-0.31	-0.24	-0.52	-0.59	-0.80	-0.87	-0.13	-0.20	-0.20	-0.22	-0.21	-0.20	-0.20	-0.14	-0.07	-0.01	-0.43	-0.58	-0.72	-0.83	-0.93	-1.02
	-0.26	-0.15	-0.49	-0.55	-0.74	-0.84	-0.13	-0.14	-0.16	-0.18	-0.17	-0.16	-0.15	-0.06	-0.01	-0.01	-0.42	-0.57	-0.71	-0.82	-0.92	-1.01
	-0.22	-0.14	-0.46	-0.52	-0.64	-0.78	-0.12	-0.18	-0.11	-0.16	-0.15	-0.14	-0.13	-0.05	-0.01	-0.01	-0.41	-0.56	-0.70	-0.81	-0.91	-1.00
	-0.19	-0.10	-0.44	-0.50	-0.61	-0.72	-0.11	-0.17	-0.10	-0.15	-0.14	-0.13	-0.12	-0.04	-0.01	-0.01	-0.40	-0.55	-0.69	-0.79	-0.89	-0.98
	-0.16	-0.08	-0.41	-0.47	-0.56	-0.67	-0.10	-0.15	-0.14	-0.17	-0.16	-0.15	-0.14	-0.03	-0.01	-0.01	-0.39	-0.54	-0.68	-0.78	-0.88	-0.97
	-0.14	-0.07	-0.40	-0.45	-0.54	-0.65	-0.09	-0.14	-0.13	-0.16	-0.15	-0.14	-0.13	-0.02	-0.01	-0.01	-0.38	-0.53	-0.67	-0.77	-0.87	-0.96
	-0.12	-0.06	-0.37	-0.43	-0.51	-0.62	-0.08	-0.13	-0.12	-0.15	-0.14	-0.13	-0.12	-0.01	-0.01	-0.01	-0.37	-0.52	-0.66	-0.76	-0.86	-0.95
	-0.10	-0.05	-0.36	-0.41	-0.49	-0.59	-0.07	-0.12	-0.11	-0.14	-0.13	-0.12	-0.11	-0.00	-0.01	-0.01	-0.36	-0.51	-0.65	-0.75	-0.85	-0.94
120°	-0.38	-0.33	-0.50	-0.89	-0.99	-0.31	-0.32	-0.31	-0.29	-0.28	-0.27	-0.27	-0.23	-0.13	-0.07	-0.46	-0.63	-0.79	-0.90	-1.05	-1.10	
	-0.37	-0.30	-0.53	-0.59	-0.85	-0.87	-0.14	-0.27	-0.28	-0.29	-0.28	-0.27	-0.26	-0.20	-0.13	-0.05	-0.44	-0.59	-0.74	-0.85	-0.95	-1.04
	-0.31	-0.24	-0.52	-0.59	-0.74	-0.84	-0.13	-0.18	-0.11	-0.16	-0.15	-0.14	-0.13	-0.06	-0.01	-0.01	-0.43	-0.58	-0.72	-0.83	-0.93	-1.02
	-0.26	-0.15	-0.49	-0.55	-0.64	-0.78	-0.12	-0.18	-0.10	-0.16	-0.15	-0.14	-0.13	-0.05	-0.01	-0.01	-0.42	-0.57	-0.71	-0.82	-0.92	-1.01
	-0.22	-0.14	-0.46	-0.52	-0.61	-0.72	-0.11	-0.17	-0.10	-0.15	-0.14	-0.13	-0.12	-0.04	-0.01	-0.01	-0.41	-0.56	-0.70	-0.81	-0.91	-1.00
	-0.19	-0.10	-0.44	-0.50	-0.58	-0.69	-0.10	-0.15	-0.14	-0.17	-0.16	-0.15	-0.14	-0.03	-0.01	-0.01	-0.40	-0.55	-0.69	-0.79	-0.89	-0.98
	-0.16	-0.08	-0.41	-0.47	-0.56	-0.67	-0.09	-0.14	-0.13	-0.16	-0.15	-0.14	-0.13	-0.02	-0.01	-0.01	-0.39	-0.54	-0.68	-0.78	-0.88	-0.97
	-0.14	-0.07	-0.40	-0.45	-0.54	-0.65	-0.08	-0.13	-0.12	-0.15	-0.14	-0.13	-0.12	-0.01	-0.01	-0.01	-0.38	-0.53	-0.67	-0.77	-0.87	-0.96
	-0.12	-0.06	-0.37	-0.43	-0.51	-0.62	-0.07	-0.12	-0.11	-0.14	-0.13	-0.12	-0.11	-0.00	-0.01	-0.01	-0.37	-0.52	-0.66	-0.76	-0.86	-0.95
	-0.10	-0.05	-0.36	-0.41	-0.49	-0.59	-0.06	-0.11	-0.10	-0.13	-0.12	-0.11	-0.10	-0.01	-0.01	-0.01	-0.36	-0.51	-0.65	-0.75	-0.85	-0.94
150°	-0.38	-0.33	-0.50	-0.89	-0.99	-0.31	-0.32	-0.31	-0.29	-0.28	-0.27	-0.27	-0.23	-0.13	-0.07	-0.46	-0.63	-0.80	-0.90	-1.05	-1.10	
	-0.37	-0.30	-0.53	-0.59	-0.85	-0.87	-0.14	-0.27	-0.28	-0.29	-0.28	-0.27	-0.26	-0.20	-0.13	-0.05	-0.44	-0.59	-0.74	-0.85	-0.95	-1.04
	-0.31	-0.24	-0.52	-0.59	-0.74	-0.84	-0.13	-0.18	-0.12	-0.16	-0.15	-0.14	-0.13	-0.06	-0.01	-0.01	-0.43	-0.58	-0.72	-0.83	-0.93	-1.02
	-0.26	-0.15	-0.49	-0.55	-0.64	-0.78	-0.12	-0.18	-0.10	-0.15	-0.14	-0.13	-0.12	-0.05	-0.01	-0.01	-0.42	-0.57	-0.71	-0.82	-0.92	-1.01
	-0.22	-0.14	-0.46	-0.52	-0.61	-0.72	-0.11	-0.17	-0.10	-0.15	-0.14	-0.13	-0.12	-0.04	-0.01	-0.01	-0.41	-0.56	-0.70	-0.81	-0.91	-1.00
	-0.19	-0.10	-0.44	-0.50	-0.58	-0.69	-0.10	-0.15	-0.14	-0.17	-0.16	-0.15	-0.14	-0.03	-0.01	-0.01	-0.40	-0.55	-0.69	-0.79	-0.89	-0.98
	-0.16	-0.08	-0.41	-0.47	-0.56	-0.67	-0.09	-0.14	-0.13	-0.16	-0.15	-0.14	-0.13	-0.02	-0.01	-0.01	-0.39	-0.54	-0.68	-0.78	-0.88	-0.97
	-0.14	-0.07	-0.40	-0.45	-0.54	-0.65	-0.08	-0.13	-0.12	-0.15	-0.14	-0.13	-0.12	-0.01	-0.01	-0.01	-0.38	-0.53	-0.67	-0.77	-0.87	-0.96
	-0.12	-0.06	-0.37	-0.43	-0.51	-0.62	-0.07	-0.12	-0.11	-0.14	-0.13	-0.12	-0.11	-0.00	-0.01	-0.01	-0.37	-0.52	-0.66	-0.76	-0.86	-0.95
	-0.10	-0.05	-0.36	-0.41	-0.49	-0.59	-0.06	-0.11	-0.10	-0.13	-0.12	-0.11	-0.10	-0.01	-0.01	-0.01	-0.36	-0.51	-0.65	-0.75	-0.85	-0.94
174°	-0.38	-0.33	-0.50	-0.89	-0.99	-0.31	-0.32	-0.31	-0.29	-0.28	-0.27	-0.27	-0.23	-0.13	-0.07	-0.46	-0.63	-0.80	-0.90	-1.05	-1.10	
	-0.37	-0.30	-0.53	-0.59	-0.85	-0.87	-0.14	-0.27	-0.28	-0.29	-0.28	-0.27	-0.26	-0.20	-0.13	-0.05	-0.44	-0.59	-0.74	-0.85	-0.95	-1.04
	-0.31	-0.24	-0.52	-0.59	-0.74	-0.84	-0.13	-0.18	-0.12	-0.16	-0.15	-0.14	-0.13	-0.06	-0.01	-0.01	-0.43	-0.58	-0.72	-0.83	-0.93	-1.02
	-0.26	-0.15	-0.49	-0.55	-0.64	-0.78	-0.12	-0.18	-0.10	-0.15	-0.14	-0.13	-0.12	-0.05	-0.01	-0.01	-0.42	-0.57	-0.71	-0.82	-0.92	-1.01
	-0.22	-0.14	-0.46	-0.52	-0.61	-0.72	-0.11	-0.17	-0.10	-0.15	-0.14	-0.13	-0.12	-0.04	-0.01	-0.01	-0.41	-0.56	-0.70	-0.81	-0.91	-1.00
	-0.19	-0.10	-0.44	-0.50	-0.58	-0.69	-0.10	-0.15	-0.14	-0.17	-0.16	-0.15	-0.14	-0.03	-0.01	-0.01	-0.40	-0.55	-0.69	-0.79	-0.89	-0.98
	-0.16	-0.08	-0.41	-0.47	-0.56	-0.67	-0.09	-0.14	-0.13	-0.16	-0.15	-0.14	-0.13	-0.02	-0.01	-0.01	-0.39	-0.54	-0.68	-0.78	-0.88	-0.97
	-0.14	-0.07	-0.40	-0.45	-0.54	-0.65	-0.08	-0.13	-0.12	-0.15	-0.14	-0.13	-0.12	-0.01	-0.01	-0.01	-0.38	-0.53	-0.67	-0.77	-0.87	-0.96
	-0.12	-0.06	-0.37	-0.43	-0.51	-0.62	-0.07	-0.12	-0.11	-0.14	-0.13	-0.12	-0.11	-0.00	-0.01	-0.01	-0.37	-0.52	-0.66	-0.76	-0.86	-0.95
	-0.10	-0.05	-0.36	-0.41	-0.49	-0.59	-0.06	-0.11	-0.10	-0.13	-0.12	-0.11	-0.10	-0.01	-0.01	-0.01	-0.36	-0.51	-0.65	-0.75	-0.85	-0.94

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (g) $A = 3$ rectangular wing, $r/s = 0.2$

θ	x/r	$\delta_w, \alpha_w = 0^\circ$												$\alpha_b, \delta_w = 0^\circ$						
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°		
6°	6.94	-0.28	-0.27	-0.26	-0.26	-0.26	-0.25	-0.24	-0.27	-0.21	-0.31	-0.38	-0.37	-0.45	-0.47	-0.81	-0.81			
	8.37	-0.21	-0.23	-0.28	-0.20	-0.21	-0.22	-0.20	-0.22	-0.17	-0.25	-0.30	-0.37	-0.27	-0.48	-0.80	-0.81			
	9.81	-0.16	-0.17	-0.18	-0.16	-0.19	-0.18	-0.17	-0.18	-0.15	-0.21	-0.25	-0.30	-0.25	-0.51	-0.81	-0.84	-0.76		
	11.25	-0.20	-0.19	-0.19	-0.16	-0.17	-0.16	-0.16	-0.18	-0.15	-0.21	-0.25	-0.20	-0.17	-0.21	-0.71	-0.74	-0.75		
	12.69	-0.17	-0.18	-0.14	-0.10	-0.12	-0.09	-0.12	-0.10	-0.16	-0.19	-0.18	-0.16	-0.10	-0.12	-0.77	-0.77	-0.75		
	14.13	-0.09	-0.03	-0.04	-0.01	-0.06	-0.02	-0.06	-0.06	-0.06	-0.08	-0.11	-0.06	-0.06	-0.05	-0.85	-0.85	-0.76		
	15.56	-0.40	-0.37	-0.31	-0.10	-0.04	-0.03	-0.07	-0.06	-0.06	-0.09	-0.09	-0.06	-0.06	-0.05	-0.77	-0.73	-0.71		
	15.84	-0.23	-0.15	-0.10	-0.04	-0.05	-0.01	-0.01	-0.08	-0.04	-0.04	-0.04	-0.03	-0.01	-0.15	-0.80	-0.80	-0.78		
	19.87	-0.38	-0.37	-0.27	-0.23	-0.15	-0.08	-0.08	-0.04	-0.04	-0.04	-0.04	-0.03	-0.01	-0.15	-0.78	-0.78	-0.71		
	21.31	-0.47	-0.45	-0.37	-0.37	-0.31	-0.21	-0.23	-0.18	-0.17	-0.14	-0.10	-0.10	-0.17	-0.28	-0.64	-0.64	-0.64		
	22.75	-0.25	-0.19	-0.16	-0.06	-0.14	-0.12	-0.04	-0.04	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.57	-0.57	-0.57		
	24.19	-0.03	-0.07	-0.06	-0.00	-0.08	-0.04	-0.02	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.50	-0.50	-0.48		
	25.63	0.04	0.12	0.09	0.00	0.07	0.02	0.01	0.04	0.14	0.19	0.08	0.04	0.01	0.19	0.53	0.53	0.46		
15°	6.94	-0.28	-0.26	-0.21	-0.24	-0.26	-0.28	-0.24	-0.28	-0.29	-0.34	-0.36	-0.34	-0.16	-0.28	-0.79	-0.87	-0.83		
	8.37	-0.23	-0.21	-0.17	-0.20	-0.23	-0.24	-0.19	-0.24	-0.23	-0.29	-0.34	-0.37	-0.26	-0.45	-0.84	-0.80	-0.80		
	9.81	-0.17	-0.26	-0.23	-0.19	-0.24	-0.25	-0.17	-0.23	-0.24	-0.34	-0.44	-0.47	-0.24	-0.57	-0.79	-0.73	-0.73		
	11.25	-0.24	-0.17	-0.17	-0.18	-0.18	-0.16	-0.16	-0.16	-0.16	-0.24	-0.34	-0.37	-0.23	-0.53	-0.72	-0.72	-0.73		
	12.69	-0.17	-0.19	-0.17	-0.18	-0.18	-0.16	-0.16	-0.16	-0.16	-0.24	-0.34	-0.37	-0.23	-0.53	-0.72	-0.72	-0.73		
	14.13	-0.18	-0.15	-0.10	-0.12	-0.12	-0.12	-0.14	-0.12	-0.12	-0.24	-0.34	-0.37	-0.23	-0.53	-0.72	-0.72	-0.73		
	15.56	-0.47	-0.07	-0.06	-0.09	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.11	-0.81	-0.81	-0.79		
	17.00	-0.30	-0.19	-0.19	-0.06	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.14	-0.80	-0.80	-0.78		
	18.44	-0.26	-0.19	-0.19	-0.08	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.14	-0.79	-0.79	-0.78		
	19.87	-0.50	-0.48	-0.48	-0.38	-0.31	-0.28	-0.28	-0.28	-0.28	-0.28	-0.28	-0.28	-0.01	-0.18	-0.81	-0.81	-0.79		
	21.31	-0.51	-0.50	-0.44	-0.36	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.01	-0.21	-0.82	-0.82	-0.80		
	22.75	-0.25	-0.11	-0.02	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.01	-0.19	-0.73	-0.73	-0.70		
	24.19	-0.13	-0.02	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.01	-0.19	-0.69	-0.69	-0.67		
	25.63	0.06	0.04	-0.04	-0.09	-0.09	-0.16	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.01	-0.24	-0.44	-0.44	-0.47		
30°	6.94	-0.34	-0.27	-0.26	-0.27	-0.35	-0.35	-0.34	-0.34	-0.34	-0.35	-0.37	-0.37	-0.30	-0.40	-0.83	-0.83	-0.83		
	8.37	-0.26	-0.21	-0.19	-0.20	-0.21	-0.20	-0.19	-0.20	-0.19	-0.21	-0.26	-0.26	-0.21	-0.38	-0.86	-0.86	-0.86		
	9.81	-0.21	-0.24	-0.23	-0.19	-0.24	-0.25	-0.17	-0.23	-0.24	-0.24	-0.34	-0.37	-0.26	-0.57	-0.76	-0.76	-0.75		
	11.25	-0.16	-0.17	-0.18	-0.18	-0.16	-0.16	-0.18	-0.17	-0.17	-0.17	-0.24	-0.24	-0.21	-0.57	-0.75	-0.75	-0.75		
	12.69	-0.17	-0.18	-0.18	-0.18	-0.16	-0.16	-0.18	-0.17	-0.17	-0.17	-0.24	-0.24	-0.21	-0.57	-0.75	-0.75	-0.75		
	14.13	-0.10	-0.09	-0.09	-0.09	-0.07	-0.07	-0.07	-0.09	-0.09	-0.09	-0.24	-0.24	-0.21	-0.57	-0.75	-0.75	-0.75		
	15.56	-0.95	-0.80	-0.80	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.01	-0.13	-0.68	-0.68	-0.68		
	17.00	-0.37	-0.31	-0.31	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.14	-0.68	-0.68	-0.68		
	18.44	-0.36	-0.34	-0.34	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.14	-0.68	-0.68	-0.68		
	19.87	-0.47	-0.49	-0.44	-0.46	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.31	-0.01	-0.14	-0.77	-0.77	-0.76		
	21.31	-0.51	-0.50	-0.47	-0.46	-0.37	-0.37	-0.37	-0.37	-0.37	-0.37	-0.37	-0.37	-0.01	-0.14	-0.77	-0.77	-0.76		
	22.75	-0.25	-0.11	-0.02	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.01	-0.19	-0.69	-0.69	-0.68		
	24.19	-0.13	-0.02	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.01	-0.19	-0.69	-0.69	-0.68		
	25.63	0.06	0.04	-0.04	-0.09	-0.09	-0.16	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.01	-0.24	-0.44	-0.44	-0.47		
60°	6.94	-0.30	-0.27	-0.29	-0.30	-0.28	-0.27	-0.21	-0.31	-0.32	-0.31	-0.32	-0.32	-0.38	-0.47	-0.80	-0.80	-0.80		
	8.37	-0.29	-0.27	-0.27	-0.26	-0.24	-0.24	-0.26	-0.27	-0.27	-0.35	-0.38	-0.38	-0.36	-0.67	-0.78	-0.78	-0.78		
	9.81	-0.27	-0.27	-0.26	-0.26	-0.24	-0.24	-0.26	-0.26	-0.27	-0.35	-0.42	-0.42	-0.36	-0.67	-0.78	-0.78	-0.78		
	11.25	-0.23	-0.23	-0.21	-0.21	-0.19	-0.19	-0.20	-0.20	-0.20	-0.35	-0.42	-0.42	-0.36	-0.67	-0.78	-0.78	-0.78		
	12.69	-0.17	-0.17	-0.17	-0.17	-0.16	-0.16	-0.18	-0.18	-0.18	-0.35	-0.42	-0.42	-0.36	-0.67	-0.78	-0.78	-0.78		
	14.13	-0.12	-0.14	-0.14	-0.13	-0.13	-0.13	-0.15	-0.15	-0.15	-0.35	-0.43	-0.43	-0.36	-0.67	-0.78	-0.78	-0.78		
	15.56	-0.50	-0.15	-0.04	-0.06	-0.06	-0.06	-0.09	-0.09	-0.09	-0.10	-0.14	-0.14	-0.09	-0.41	-0.68	-0.68	-0.68		
	17.00	-0.38	-0.21	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.01	-0.15	-0.68	-0.68	-0.68		
	18.44	-0.77	-0.84	-0.88	-0.83	-0.78	-0.67	-0.59	-0.49	-0.38	-0.28	-0.16	-0.05	-0.01	-0.53	-0.98	-0.98	-0.98		
	19.87	-0.76	-0.75	-0.69	-0.73	-0.68	-0.64	-0.50	-0.40	-0.30	-0.21	-0.11	-0.05	-0.01	-0.13	-0.98	-0.98	-0.98		
	21.31	-0.34	-0.19	-0.19	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.01	-0.17	-0.98	-0.98	-0.98		
	22.75	-0.27	-0.11	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.17	-0.98	-0.98		
	24.19	-0.13	-0.02	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.17	-0.98	-0.98		
	25.63	0.03	0.09	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.24	-0.44	-0.44		

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (g) $A = 3$ rectangular wing, $r/s = 0.2$ - Concluded

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
(h) A = 2 rectangular wing, r/s = 0.2

θ	x/r	$\delta_w, \alpha_B = 0^\circ$												$\alpha_B, \delta_w = 0^\circ$											
		40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°								
6°	1.134	-0.13	-0.11	-0.12	-0.10	-0.11	-0.13	-0.12	-0.11	-0.12	-0.13	-0.12	-0.11	-0.15	-0.19	-0.64	-0.63	-0.91							
	1.259	-0.08	-0.07	-0.08	-0.09	-0.09	-0.10	-0.10	-0.08	-0.08	-0.08	-0.08	-0.08	-0.13	-0.17	-0.67	-0.62	-0.83							
	1.384	-0.08	-0.07	-0.07	-0.05	-0.08	-0.08	-0.08	-0.08	-0.07	-0.07	-0.07	-0.07	-0.10	-0.19	-0.67	-0.67	-0.87							
	1.509	-0.23	-0.18	-0.01	-0.04	-0.02	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.08	-0.23	-0.67	-0.67	-0.88							
	1.634	-0.18	-0.08	-0.05	-0.04	-0.02	-0.02	-0.05	-0.04	-0.05	-0.05	-0.04	-0.04	-0.05	-0.38	-0.62	-0.62	-0.88							
	1.756	-0.09	-0.03	-0.00	-0.12	-0.06	-0.07	-0.16	-0.12	-0.09	-0.08	-0.08	-0.08	-0.01	-0.31	-0.76	-0.76	-0.88							
	1.884	-0.11	-0.08	-0.03	-0.31	-0.27	-0.16	-0.12	-0.12	-0.08	-0.08	-0.08	-0.08	-0.01	-0.35	-0.76	-0.76	-0.88							
	2.009	-0.09	-0.05	-0.56	-0.45	-0.37	-0.26	-0.20	-0.14	-0.14	-0.14	-0.14	-0.14	-0.01	-0.42	-0.81	-0.81	-0.91							
	2.134	-0.11	-0.05	-0.57	-0.45	-0.37	-0.32	-0.27	-0.14	-0.14	-0.14	-0.14	-0.14	-0.01	-0.43	-0.82	-0.82	-0.91							
	2.259	-0.11	-0.05	-0.53	-0.45	-0.30	-0.34	-0.29	-0.18	-0.24	-0.21	-0.20	-0.20	-0.01	-0.40	-0.51	-0.51	-0.76							
15°	2.384	-0.09	-0.05	-0.50	-0.24	-0.18	-0.24	-0.21	-0.11	-0.09	-0.08	-0.08	-0.08	-0.01	-0.29	-0.67	-0.67	-0.88							
	2.509	-0.11	-0.06	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.05	-0.05	-0.05	-0.05							
	1.134	-0.14	-0.11	-0.14	-0.15	-0.12	-0.16	-0.15	-0.13	-0.12	-0.13	-0.12	-0.12	-0.01	-0.16	-0.68	-0.68	-0.87							
	1.259	-0.11	-0.06	-0.09	-0.11	-0.07	-0.10	-0.09	-0.03	-0.07	-0.07	-0.07	-0.07	-0.01	-0.18	-0.69	-0.69	-0.87							
	1.384	-0.11	-0.06	-0.06	-0.06	-0.02	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.07	-0.01	-0.23	-0.68	-0.68	-0.87							
	1.509	-0.11	-0.06	-0.06	-0.06	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.05	-0.61	-0.61	-0.87							
	1.756	-0.09	-0.04	-0.04	-0.05	-0.05	-0.19	-0.11	-0.08	-0.08	-0.08	-0.08	-0.08	-0.01	-0.05	-0.41	-0.41	-0.61							
	1.884	-0.06	-0.04	-0.40	-0.37	-0.32	-0.42	-0.31	-0.25	-0.25	-0.25	-0.25	-0.25	-0.01	-0.19	-0.49	-0.49	-0.64							
	2.009	-0.06	-0.04	-0.56	-0.52	-0.42	-0.44	-0.37	-0.38	-0.38	-0.38	-0.38	-0.38	-0.01	-0.19	-0.49	-0.49	-0.64							
	2.134	-0.06	-0.04	-0.59	-0.51	-0.44	-0.39	-0.39	-0.39	-0.39	-0.39	-0.39	-0.39	-0.01	-0.19	-0.49	-0.49	-0.64							
30°	2.259	-0.06	-0.04	-0.52	-0.50	-0.42	-0.46	-0.46	-0.46	-0.46	-0.46	-0.46	-0.46	-0.01	-0.19	-0.49	-0.49	-0.64							
	2.384	-0.06	-0.04	-0.50	-0.49	-0.40	-0.49	-0.49	-0.49	-0.49	-0.49	-0.49	-0.49	-0.01	-0.19	-0.49	-0.49	-0.64							
	2.509	-0.06	-0.04	-0.50	-0.49	-0.40	-0.49	-0.49	-0.49	-0.49	-0.49	-0.49	-0.49	-0.01	-0.19	-0.49	-0.49	-0.64							
	1.134	-0.15	-0.15	-0.15	-0.15	-0.15	-0.15	-0.15	-0.15	-0.15	-0.15	-0.15	-0.15	-0.01	-0.16	-0.51	-0.51	-0.61							
	1.259	-0.11	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.01	-0.17	-0.44	-0.44	-0.61							
	1.384	-0.11	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.01	-0.17	-0.44	-0.44	-0.61							
	1.509	-0.11	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.08	-0.01	-0.17	-0.44	-0.44	-0.61							
	1.756	-0.09	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.01	-0.07	-0.31	-0.31	-0.47							
	1.884	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							
	2.009	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							
60°	2.134	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							
	2.259	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							
	2.384	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							
	2.509	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							
	1.134	-0.19	-0.11	-0.10	-0.14	-0.10	-0.18	-0.12	-0.12	-0.12	-0.12	-0.12	-0.12	-0.01	-0.19	-0.51	-0.51	-0.61							
	1.259	-0.11	-0.06	-0.12	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.01	-0.19	-0.44	-0.44	-0.61							
	1.384	-0.10	-0.06	-0.12	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.01	-0.19	-0.44	-0.44	-0.61							
	1.509	-0.10	-0.06	-0.12	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.01	-0.19	-0.44	-0.44	-0.61							
	1.756	-0.10	-0.06	-0.12	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.01	-0.19	-0.44	-0.44	-0.61							
	1.884	-0.10	-0.06	-0.12	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.14	-0.01	-0.19	-0.44	-0.44	-0.61							
	2.009	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							
	2.134	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							
	2.259	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							
	2.384	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							
	2.509	-0.06	-0.04	-0.06	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	-0.01	-0.07	-0.31	-0.31	-0.47							

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (h) $A = 2$ rectangular wing, $r/s = 0.2$ - Concluded

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (i) $A = 1$ rectangular wing, $r/s = 0.2$

TABLE III.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Continued
 (j) A = 1 rectangular wing, r/s = 0.4

θ	x/r	$\delta_w, \alpha_B = 0^\circ$									$\alpha_B, \delta_w = 0^\circ$									
		35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°				
6°	6.94	- .028	- .027	- .027	- .029	- .028	.001	- .026	- .028	- .026	- .040	- .048	- .044	- .047	- .081	- .093				
	8.37	- .023	- .023	- .023	- .023	- .023	.003	- .021	- .021	- .021	- .031	- .032	- .036	- .047	- .079	- .086				
	9.81	- .020	- .017	- .020	- .019	- .019	.004	- .018	- .019	- .017	- .024	- .030	- .025	- .050	- .079	- .090				
	11.25	- .019	- .018	- .017	- .019	- .019	.004	- .015	- .015	- .015	- .022	- .021	- .015	- .056	- .085	- .097				
	12.69	- .016	- .014	- .014	- .015	- .015	.007	- .015	- .015	- .012	- .018	- .021	- .015	- .057	- .079	- .082				
	14.12	- .008	- .008	- .009	- .009	- .010	.006	- .009	- .009	- .006	- .010	- .012	- .016	- .058	- .084	- .086				
	15.56	- .005	- .004	- .004	- .005	- .007	.007	- .005	- .005	- .007	- .004	- .009	- .008	- .057	- .075	- .084				
	17.00	- .029	- .013	- .000	- .004	- .006	.006	- .005	- .005	- .007	- .004	- .009	- .006	- .027	- .054	- .080	- .081			
	18.44	- .015	- .007	- .005	- .006	- .005	.004	- .001	- .001	- .004	- .001	- .001	- .001	- .020	- .061	- .086	- .080			
	19.87	- .034	- .023	- .016	- .011	- .007	.001	- .008	- .003	- .007	- .009	- .018	- .020	- .063	- .089	- .092	- .086			
	21.31	- .044	- .037	- .031	- .027	- .083	.001	- .015	- .010	- .002	- .017	- .030	- .037	- .076	- .073	- .076	- .086			
	22.75	- .033	- .026	- .021	- .081	- .019	.005	- .009	- .001	- .006	- .010	- .020	- .024	- .053	- .042	- .066	- .066			
	24.19	- .003	- .001	- .008	- .014	- .012	.005	- .007	- .011	- .005	- .005	- .013	- .013	- .033	- .030	- .069	- .069			
	25.68	.010	.014	.011	.008	.006	.000	.014	.017	.020	.014	.010	.002	.040	.051	.089				
15°	6.94	- .030	- .027	- .030	- .028	- .028	.001	- .030	- .030	- .028	- .038	- .037	- .039	- .068	- .090	- .087				
	8.37	- .024	- .024	- .023	- .023	- .028	.002	- .028	- .021	- .024	- .031	- .034	- .044	- .072	- .086	- .087				
	9.81	- .020	- .018	- .017	- .019	- .019	.004	- .019	- .018	- .018	- .024	- .029	- .041	- .071	- .087	- .086				
	11.25	- .024	- .022	- .022	- .024	- .024	.005	- .025	- .024	- .023	- .023	- .026	- .042	- .072	- .080	- .088				
	12.69	- .016	- .014	- .015	- .015	- .016	.004	- .016	- .015	- .015	- .019	- .020	- .036	- .068	- .071	- .079				
	14.12	- .012	- .010	- .009	- .011	- .010	.005	- .011	- .012	- .010	- .011	- .017	- .033	- .066	- .071	- .082				
	15.56	- .008	- .006	- .007	- .007	- .007	.006	- .006	- .006	- .007	- .009	- .017	- .036	- .065	- .075	- .082				
	17.00	.017	.010	.003	.001	.004	.004	- .003	- .003	- .002	- .007	- .011	- .035	- .055	- .082	- .081				
	18.44	- .016	- .014	- .010	- .006	- .004	.002	- .002	- .005	- .005	- .003	- .010	- .036	- .057	- .086	- .083				
	19.87	- .048	- .038	- .032	- .026	- .022	.001	- .014	- .010	- .004	- .015	- .028	- .041	- .065	- .093	- .091				
	21.31	- .047	- .039	- .035	- .031	- .026	.002	- .018	- .012	- .003	- .019	- .036	- .049	- .080	- .077	- .081				
	22.75	- .031	- .027	- .021	- .026	- .026	.008	- .011	- .004	- .003	- .016	- .021	- .056	- .089	- .066	- .066				
	24.19	- .001	.003	- .006	- .017	- .014	.006	- .006	- .008	- .005	- .005	- .003	- .003	- .043	- .029	- .067	- .067			
	25.68	.011	.015	.014	.009	.010	.001	- .017	- .016	- .019	- .010	- .005	- .005	- .039	- .054	- .059				
30°	6.94	- .026	- .033	- .033	- .033	- .033	.006	- .035	- .035	- .031	- .042	- .047	- .061	- .085	- .094	- .092				
	8.37	- .024	- .028	- .037	- .037	- .037	.008	- .029	- .029	- .027	- .037	- .051	- .087	- .086	- .085	- .085				
	9.81	- .017	- .021	- .022	- .019	- .020	.001	- .021	- .019	- .019	- .026	- .033	- .062	- .087	- .083	- .084				
	11.25	- .013	- .021	- .019	- .017	- .018	.002	- .020	- .019	- .018	- .024	- .029	- .062	- .088	- .075	- .080				
	12.69	- .010	- .019	- .015	- .016	- .016	.006	- .017	- .017	- .016	- .026	- .036	- .063	- .073	- .073	- .082				
	14.12	- .008	- .010	- .009	- .008	- .009	.005	- .009	- .009	- .008	- .013	- .026	- .057	- .070	- .075	- .078				
	15.56	- .005	- .006	- .008	- .007	- .007	.004	- .008	- .008	- .007	- .011	- .026	- .058	- .066	- .079	- .079				
	17.00	- .005	- .005	- .008	- .003	- .003	.004	- .004	- .003	- .002	- .003	- .022	- .038	- .069	- .070	- .070				
	18.44	- .031	- .034	- .027	- .017	- .011	.001	- .030	- .030	- .028	- .041	- .050	- .069	- .084	- .092	- .092				
	19.87	- .050	- .044	- .037	- .029	- .024	.008	- .012	- .005	- .005	- .021	- .031	- .076	- .082	- .087	- .087				
	21.31	- .055	- .048	- .041	- .036	- .032	.008	- .019	- .010	- .001	- .016	- .030	- .037	- .055	- .074	- .076				
	22.75	- .014	- .013	- .033	- .038	- .035	.005	- .015	- .007	- .001	- .007	- .010	- .016	- .061	- .062	- .067				
	24.19	- .001	.005	- .006	.001	- .000	.007	- .008	- .005	- .008	- .003	- .007	- .017	- .032	- .072	- .068				
	25.68	.003	.006	.008	.009	.008	.003	- .008	- .008	- .008	.009	.009	.000	- .015	- .029	- .067	- .061			
60°	6.94	- .031	- .029	- .032	- .030	- .030	.001	- .032	- .030	- .029	- .042	- .053	- .065	- .079	- .086	- .089				
	8.37	- .027	- .027	- .028	- .026	- .027	.001	- .030	- .028	- .026	- .036	- .051	- .061	- .076	- .082	- .084				
	9.81	- .026	- .025	- .026	- .026	- .025	.000	- .027	- .026	- .026	- .033	- .045	- .053	- .065	- .075	- .082				
	11.25	- .019	- .018	- .018	- .018	- .018	.003	- .020	- .019	- .019	- .029	- .038	- .051	- .063	- .074	- .078				
	12.69	- .017	- .016	- .017	- .017	- .016	.003	- .017	- .018	- .018	- .021	- .030	- .045	- .061	- .071	- .079				
	14.12	- .014	- .012	- .014	- .013	- .013	.004	- .014	- .015	- .014	- .017	- .024	- .042	- .054	- .069	- .077				
	15.56	- .009	- .008	- .010	- .007	- .010	.003	- .010	- .009	- .010	- .014	- .018	- .036	- .049	- .064	- .076				
	17.00	- .093	- .043	- .047	- .038	- .035	.003	- .019	- .011	- .003	- .005	- .023	- .059	- .066	- .077	- .081	- .085			
	18.44	- .080	- .080	- .077	- .070	- .061	.001	- .028	- .013	- .005	- .015	- .020	- .048	- .053	- .067	- .074	- .103	- .100		
	19.87	- .025	- .075	- .077	- .069	- .062	.003	- .034	- .020	- .010	- .006	- .020	- .026	- .048	- .053	- .060	- .086	- .077		
	21.31	- .016	- .021	- .031	- .046	- .042	.003	- .020	- .013	- .006	- .006	- .020	- .023	- .036	- .048	- .051	- .073	- .073		
	22.75	- .020	- .006	- .012	- .011	- .012	.005	- .006	- .005	- .003	- .007	- .009	- .004	- .011	- .038	- .041	- .048	- .074	- .061	
	24.19	- .003	.003	- .005	.005	.007	.008	.001	.006	.006	.007	.009	.004	- .011	- .038	- .041	- .048	- .053	- .053	
	25.68	.026	.005	.005	.007	.008	.008	.001	.006	.006	.007	.009	.004	- .011	- .038	- .041	- .048	- .074	- .061	

TABLE II.- PRESSURE COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE WINGS - Concluded
 (j) $A = 1$ rectangular wing, $r/s = 0.4$ - Concluded

θ	x/r	$\delta_w, \alpha_8 = 0^\circ$										$a_B, \delta_w = 0^\circ$							
		35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°			
120°	6.94	- .033	- .032	- .031	- .032	.001	-.033	-.031	-.031	-.029	-.028	-.009	.011	.048	109				
	8.37	- .027	- .027	- .026	- .027	.001	-.026	-.027	-.027	-.025	-.025	-.013	.006	.045	101				
	9.81	- .027	- .026	- .026	- .027	.000	-.027	-.028	-.026	-.027	-.026	-.018	.004	.049	107				
	11.25	- .088	- .021	- .081	- .022	.003	-.023	-.022	-.022	-.026	-.026	-.015	.001	.040	108				
	12.69	- .019	- .016	- .018	- .020	.018	-.003	-.018	-.017	-.018	-.022	-.015	.004	.048	119				
	14.13	- .015	- .014	- .013	- .014	.014	-.004	-.014	-.015	-.014	-.020	-.018	.006	.051	125				
	15.56	- .067	- .012	- .011	- .011	.011	-.004	-.011	-.011	-.010	-.009	-.023	-.000	.048	188				
	17.00	- .015	- .053	- .048	- .011	.033	-.003	-.011	-.008	-.011	-.013	-.026	.074	159	287				
	18.44	- .094	- .043	- .077	- .020	.073	-.004	-.014	-.004	-.011	-.008	-.035	.080	147	213	141			
	19.87	- .064	- .043	- .028	- .043	.029	-.003	-.009	-.009	-.010	-.011	-.024	.114	129	281	216			
	21.31	- .018	- .016	- .011	- .003	.008	-.004	-.004	-.006	-.006	-.007	-.015	.067	024	062	104	315		
	22.75	- .011	- .007	- .000	- .007	.003	-.005	-.006	-.006	-.008	-.001	-.011	-.020	039	043	173			
	24.19	- .004	- .016	- .008	- .005	.009	-.006	-.004	-.004	-.014	-.004	-.003	-.013	004	099	171	260		
	25.62	- .003	- .013	- .003	- .001	.000	-.004	-.011	-.014	-.014	-.007	-.001	-.028						
150°	6.94	- .034	- .030	- .030	- .031	.006	-.031	-.032	-.031	-.022	-.023	-.023	-.087	.162	899				
	8.37	- .023	- .024	- .020	- .020	.020	-.028	-.028	-.028	-.017	-.011	-.024	-.078	.374					
	9.81	- .020	- .020	- .020	- .020	.019	-.020	-.021	-.020	-.019	-.020	-.015	-.009	.249					
	11.25	- .019	- .015	- .015	- .015	.016	-.018	-.016	-.016	-.017	-.019	-.020	-.065	.227					
	12.69	- .017	- .007	- .007	- .009	.010	-.005	-.009	-.008	-.012	-.012	-.005	-.016	.186					
	14.13	- .007	- .007	- .009	- .009	.010	-.004	-.009	-.011	-.010	-.011	-.004	-.020	.156					
	15.56	- .089	- .009	- .009	- .006	.065	-.044	-.004	-.005	-.011	-.010	-.004	-.024	.119					
	17.00	- .009	- .009	- .006	- .006	.065	-.004	-.015	-.007	-.003	-.014	-.004	-.049	.106					
	18.44	- .068	- .009	- .005	- .014	.063	-.007	-.018	-.007	-.003	-.013	-.006	-.067	.148					
	19.87	- .008	- .004	- .004	- .004	.016	-.003	-.005	-.004	-.005	-.015	-.008	-.068	.183					
	21.31	- .031	- .014	- .000	- .000	.003	-.005	-.007	-.009	-.002	-.006	-.024	-.008	.140					
	22.75	- .014	- .014	- .000	- .000	.002	-.005	-.006	-.009	-.002	-.005	-.024	-.010	.101					
	24.19	- .002	- .002	- .000	- .000	.008	-.013	-.002	-.023	-.008	-.022	-.027	-.050	.168					
	25.62	- .002	- .002	- .000	- .000	.008	-.002	-.023	-.008	-.022	-.027	-.050							
165°	6.94	- .030	- .031	- .030	- .030	.031	-.031	-.030	-.029	-.030	-.017	-.005	.322	.999	137				
	8.37	- .024	- .024	- .023	- .023	.019	-.021	-.023	-.023	-.024	-.011	-.007	.335						
	9.81	- .021	- .024	- .024	- .023	.023	-.023	-.021	-.023	-.023	-.011	-.005	.331						
	11.25	- .024	- .016	- .016	- .014	.014	-.017	-.004	-.016	-.016	-.015	-.011	.027						
	12.69	- .015	- .016	- .016	- .014	.014	-.017	-.004	-.016	-.016	-.011	-.005	.026						
	14.13	- .010	- .012	- .009	- .010	.010	-.006	-.008	-.009	-.010	-.009	-.003	.007	.078					
	15.56	- .019	- .008	- .008	- .008	.008	-.008	-.008	-.008	-.010	-.009	-.001	.026						
	17.00	- .023	- .017	- .018	- .018	.066	-.011	-.004	-.018	-.010	-.010	-.006	.077						
	18.44	- .069	- .069	- .057	- .110	.071	-.002	-.018	-.007	-.004	-.015	-.014	.017	.074					
	19.87	- .039	- .026	- .117	.104	.081	-.001	-.027	-.013	-.003	-.016	-.036	.055	.095					
	21.31	- .004	- .010	- .005	- .010	.006	-.008	-.002	-.003	-.002	-.002	-.022	-.026	.072	.113				
	22.75	- .012	- .003	- .001	- .001	.010	-.014	-.008	-.010	-.010	-.024	-.046	.071	.113					
	24.19	- .010	- .001	- .001	- .001	.008	-.007	-.013	-.001	-.021	-.024	-.059	.086	.168					
	25.62	- .004	- .001	- .001	- .001	.008	-.007	-.013	-.001	-.021	-.024	-.059	.117	.194					
174°	6.94	- .032	- .032	- .025	- .033	.032	-.001	-.032	-.031	-.031	-.015	-.008	.335	.111					
	8.37	- .028	- .028	- .025	- .028	.024	-.003	-.024	-.023	-.024	-.010	-.006	.340	.100					
	9.81	- .017	- .021	- .021	- .019	.018	-.004	-.018	-.017	-.017	-.010	-.006	.337	.092					
	11.25	- .019	- .019	- .021	- .019	.020	-.004	-.019	-.016	-.016	-.010	-.006	.314	.084					
	12.69	- .013	- .014	- .014	- .011	.014	-.011	-.013	-.007	-.013	-.013	-.006	.311	.073					
	14.13	- .009	- .012	- .011	- .011	.011	-.011	-.006	-.012	-.012	-.008	-.006	.234	.074					
	15.56	- .013	- .006	- .006	- .006	.035	-.006	-.007	-.005	-.005	-.003	-.003	.229	.071					
	17.00	- .062	- .034	- .166	.134	.093	-.004	-.004	-.018	-.007	-.006	-.003	.228	.075					
	18.44	- .064	- .093	- .066	.055	.068	-.001	-.023	-.016	-.005	-.005	-.003	.219	.071					
	19.87	- .068	- .092	- .066	.031	.032	-.001	-.014	-.014	-.005	-.005	-.003	.243	.066					
	21.31	- .035	- .017	- .022	.007	.007	-.005	-.005	-.011	-.004	-.004	-.003	.084	.199					
	22.75	- .009	- .001	- .001	.009	.014	-.005	-.005	-.011	-.004	-.004	-.003	.118						
	24.19	- .011	- .001	- .001	.003	.003	-.007	-.007	-.011	-.004	-.004	-.003							
	25.62	- .004	- .000	- .000	.007	.014	-.000	-.000	-.006	-.006	-.006	-.003							

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL
 (a) $A = 4$ triangular wing, $r/s = 0.2$

a_B	y/s	δ_w											
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	
0°	Upper	.025	-1.45	-1.32	-1.44	-1.39	-1.25	-1.11	-0.93	-0.61	-0.30	-0.06	0.19
		.250	-1.11	-1.02	-1.17	-1.14	-1.06	-0.94	-0.87	-0.68	-0.38	-0.07	0.33
		.500	-0.72	-0.67	-0.76	-0.75	-0.67	-0.71	-0.51	-0.48	-0.30	-0.10	0.19
	Lower	.750	-0.33	-0.32	-0.37	-0.36	-0.24	-0.30	-0.26	-0.23	-0.15	-0.07	0.05
		.025	1.798	1.512	1.244	947	587	516	321	175	102	52	0.19
		.250	1.529	1.325	1.120	916	705	538	377	231	138	76	0.33
	Total	.500	1.027	.910	.795	667	523	401	281	168	93	46	0.19
		.750	.517	.463	.408	344	270	205	134	0.72	0.37	37	0.05
		.025	1.943	1.644	1.388	1.086	812	627	414	236	132	58	0.00
3°	Upper	.250	1.640	1.427	1.237	1.030	811	632	464	299	176	83	0.00
		.500	1.099	.977	.871	.742	590	472	332	210	123	56	0.00
		.750	.550	.495	.445	380	294	235	160	0.95	0.52	44	0.00
	Lower	.025	-1.42	-1.40	-1.49	-1.39	-1.13	-1.21	-1.04	-0.82	-0.61	-0.44	-0.00
		.250	-1.11	-1.09	-1.21	-1.13	-0.95	-1.07	-0.98	-0.84	-0.67	-0.46	-0.21
		.500	-0.73	-0.72	-0.79	-0.74	-0.64	-0.70	-0.65	-0.56	-0.44	-0.31	-0.13
	Total	.750	-0.35	-0.35	-0.39	-0.36	-0.30	-0.34	-0.31	-0.26	-0.20	-0.15	-0.06
		.025	1.707	1.663	1.429	1.187	921	680	461	303	197	132	0.77
		.250	1.614	1.448	1.248	1.072	858	655	487	337	227	154	0.88
6°	Upper	.500	1.089	.979	.865	.750	625	490	360	241	153	99	0.51
		.750	.546	.500	.444	386	322	254	179	110	65	40	0.17
		.025	1.849	1.803	1.578	1.326	1.034	.801	.565	.385	.258	176	0.97
	Lower	.250	1.725	1.557	1.369	1.185	.953	.772	.585	.421	.294	200	1.09
		.500	1.162	1.051	.944	.824	.689	.560	.425	.297	.197	130	0.64
		.750	.581	.535	.483	.422	.358	.288	.210	.136	.085	.055	0.23
	Total	.025	-1.51	-1.45	-1.46	-1.33	-1.21	-1.09	-0.89	-0.82	-0.67	-0.40	-0.00
		.250	-1.17	-1.16	-1.19	-1.12	-1.05	-1.06	-0.91	-0.80	-0.60	-0.36	-0.21
		.500	-0.76	-0.75	-0.78	-0.73	-0.69	-0.69	-0.58	-0.49	-0.34	-0.21	-0.14
10°	Upper	.025	1.218	1.290	1.079	847	662	461	336	248	169	0.78	0.00
		.250	1.339	1.159	965	784	610	443	326	244	178	1.20	0.00
		.500	.953	.833	.708	585	460	334	241	173	120	0.73	0.49
	Lower	.750	.486	.427	.365	306	238	167	108	73	49	24	0.14
		.025	1.368	1.435	1.225	980	783	570	427	330	236	136	0.00
		.250	1.456	1.275	1.084	896	715	549	417	324	238	1.54	0.00
	Total	.500	1.029	.908	.786	658	529	403	299	228	154	0.63	0.00
		.750	.583	.464	.402	340	270	199	134	.94	0.63	0.22	0.00
		.025	-1.41	-1.33	-1.50	-1.45	-1.34	-1.32	-1.22	-1.07	-1.06	-0.88	-0.00
15°	Upper	.250	-1.10	-1.05	-1.19	-1.18	-1.10	-1.13	-1.03	-0.90	-0.88	-0.88	-0.00
		.500	-0.74	-0.69	-0.78	-0.77	-0.71	-0.71	-0.61	-0.55	-0.53	-0.52	-0.22
		.750	-0.34	-0.32	-0.38	-0.36	-0.33	-0.33	-0.29	-0.23	-0.22	-0.21	-0.01
	Lower	.025	1.480	1.574	1.673	1.440	1.591	1.477	1.381	1.323	1.34	1.34	0.00
		.250	1.675	1.190	1.008	839	674	501	372	313	237	179	0.00
		.500	.973	.868	.753	630	514	387	302	243	179	1.79	0.00
	Total	.750	.497	.451	.391	329	278	203	155	113	0.79	0.79	0.00
		.025	.621	.707	823	885	725	609	503	430	340	340	0.00
		.250	1.765	1.295	1.187	957	784	614	475	403	325	231	0.00
20°	Upper	.500	1.047	.937	.831	.707	585	458	343	298	231	1.71	0.00
		.750	.531	.483	.429	365	305	236	184	136	1.01	0.00	0.00

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (a) $A = 4$ triangular wing, $r/s = 0.2$ - Continued

α_B	y/s	δ_w										
		-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°	
0°	Upper	.025										
	Lower	.025										
	Total	.025										
	Upper	.025										
	Lower	.025										
	Total	.025										
	Upper	.025										
	Lower	.025										
	Total	.025										
	Upper	.025										
3°	Upper	.025	.004	.019	.077	.178	.324	.498	.723	.1010	.1299	.1545
	Lower	.025	.016	.055	.134	.251	.390	.554	.729	.944	.1141	.1342
	Total	.025	.010	.037	.096	.188	.303	.426	.551	.689	.816	.918
	Upper	.025	.017	.013	.033	.041	.041	.041	.041	.049	.063	.069
	Lower	.025	.005	.016	.043	.087	.149	.223	.291	.362	.421	.468
	Total	.025	.003	.009	.016	.018	.018	.031	.036	.034	.030	.033
	Upper	.025	.037	-.064	-.039	-.070	-.082	-.114	-.131	-.132	-.121	-.133
	Lower	.025	.038	-.006	-.043	-.064	-.069	-.095	-.104	-.109	-.096	-.105
	Total	.025	.007	-.050	-.129	-.229	-.344	-.490	-.635	-.760	-.879	-.987
	Upper	.025	.002	-.025	-.059	-.105	-.167	-.254	-.327	-.396	-.451	-.501
6°	Upper	.025	.057	-.037	-.012	.053	.177	.334	.544	.783	.1045	.1375
	Lower	.025	.041	-.010	.037	.130	.257	.399	.569	.751	.950	.1176
	Total	.025	.020	.005	.038	.110			.452	.580	.717	.853
	Upper	.025	.006	.006	.021	.057	.108	.178	.251	.317	.384	.448
	Lower	.025	.113	.066	.007	-.045	-.071	-.096	-.115	-.127	-.106	-.126
	Total	.025	.119	.073	.010	-.041	-.060	-.079	-.094	-.100	-.082	-.098
	Upper	.025	.075	.044	.001	-.031	-.041	-.052	-.068	-.065	-.047	-.029
	Lower	.025	.030	.018	-.002	-.016	-.019	-.025	-.029	-.031	-.026	-.029
	Total	.025	.170	.103	.019	-.098	-.248	-.430	-.659	-.910	-.1151	-.1501
	Upper	.025	.160	.083	-.027	-.171	-.317	-.478	-.663	-.851	-.1032	-.1274
10°	Upper	.025	.095	.039	-.037	-.141	-.254	-.380	-.514	-.645	-.764	-.911
	Lower	.025	.036	.012	-.003	-.073	-.127	-.203	-.380	-.348	-.410	-.477
	Total	.025	.101	-.101	-.080	-.030	.073	.212	.389		.818	1.064
	Upper	.025	.085	-.078	-.039	.050	.129	.242	.385		.719	.902
	Lower	.025	.044	-.035	-.004	.053	.135	.235	.346		.569	.688
	Total	.025	.017	-.014	-.003	.038	.073	.129	.199		.322	.381
	Upper	.025	.160	.092	.033	-.022	-.081	-.102	-.117		-.142	-.136
	Lower	.025	.179	.115	.047	-.008	-.066	-.084	-.097		-.114	-.109
	Total	.025	.132	.082	.038	-.006	-.043	-.054	-.062		-.075	-.072
	Upper	.025	.056	.032	.010	-.005	-.020	-.025	-.030		-.035	-.034
Total	Upper	.025	.261	.193	.113	.008	-.154	-.314	-.506		.960	-.1200
	Lower	.025	.264	.193	.086	-.038	-.195	-.326	-.482		.833	-.1011
	Total	.025	.176	.117	.036	-.059	-.178	-.289	-.408		.544	-.760
	Upper	.025	.073	.046	.007	-.037	-.093	-.154	-.229		.357	-.415

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE
 BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (a) A = 4 triangular wing, r/s = 0.2 - Continued

α_B	y_s	8W											
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	
15°	Upper	.025				- .149	- .148	- .140	- .147	- .143	- .134	- .141	- .127
		.250				- .117	- .116	- .108	- .116	- .110	- .102	- .111	- .101
		.500				- .076	- .075	- .069	- .074	- .069	- .064	- .070	- .063
		.750				- .036	- .035	- .033	- .035	- .033	- .030	- .033	- .029
	Lower	.025				- .495	- 1.753	- .474	- .733	- .667	- .580	- .502	- .391
		.250				- 1.597	- 1.346	- 1.142	- .983	- .763	- .611	- .509	- .407
		.500				- .094	- .960	- .889	- .730	- .573	- .464	- .391	- .315
		.750				- .565	- .506	- .439	- .389	- .312	- .252	- .211	- .168
	Total	.025				- .644	- 1.901	- .614	- .880	- .810	- .714	- .643	- .518
		.250				- 1.714	- 1.462	- 1.250	- 1.099	- .873	- .713	- .620	- .508
		.500				- 1.170	- 1.035	- .898	- .804	- .642	- .528	- .461	- .378
		.750				- .601	- .541	- .472	- .424	- .345	- .282	- .244	- .197
20°	Upper	.025				- .126	- .141	- .157	- .149	- .157	- .155	- .156	- .141
		.250				- .096	- .105	- .119	- .112	- .117	- .119	- .121	- .107
		.500				- .061	- .067	- .076	- .074	- .076	- .084	- .085	- .065
		.750				- .028	- .031	- .036	- .035	- .036	- .036	- .039	- .029
	Lower	.025				- .704	- .716	- .762	- .960	- .888	- .798	- .770	- .565
		.250				- 1.944	- 1.680	- 1.460	- 1.211	- .990	- .806	- .693	- .569
		.500				- 1.314	- 1.179	- 1.042	- .886	- .733	- .605	- .527	- .440
		.750				- .653	- .605	- .537	- .462	- .388	- .327	- .304	- .240
	Total	.025				- .830	- .857	- .919	- 1.109	- 1.039	- .953	- .926	- .706
		.250				- 2.040	- 1.785	- 1.559	- 1.323	- 1.107	- .925	- .814	- .676
		.500				- 1.375	- 1.246	- 1.118	- .960	- .809	- .689	- .607	- .505
		.750				- .681	- .636	- .573	- .497	- .424	- .363	- .343	- .269
25°	Upper	.025				- .142	- .148	- .168	- .168	- .155	- .139	- .149	
		.250				- .110	- .114	- .134	- .134	- .122	- .113	- .119	
		.500				- .071	- .073	- .088	- .088	- .078	- .074	- .068	
		.750				- .034	- .034	- .041	- .041	- .036	- .034	- .029	
	Lower	.025				- 1.240	- 1.466	- 1.305	- 1.257	- 1.120	- .839		
		.250				- 1.849	- 1.584	- 1.325	- 1.125	- .976	- .830		
		.500				- 1.323	- 1.141	- .967	- .831	- .728	- .689		
		.750				- .715	- .621	- .531	- .463	- .409	- .334		
	Total	.025				- 1.382	- 1.614	- 1.473	- 1.412	- 1.259	- .988		
		.250				- 1.959	- 1.698	- 1.459	- 1.247	- 1.089	- .942		
		.500				- 1.394	- 1.214	- 1.055	- .909	- .802	- .697		
		.750				- .749	- .655	- .572	- .499	- .443	- .363		

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE
BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
(a) $A = \frac{4}{3}$ triangular wing, $r/s = 0.2$ - Concluded

α_B	y/s	δ_w										
		-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°	
15°	Upper	.025	- .129	- .122	.000	- .026	.228	.395	.609	.846	1.082	
		.250	- .098	- .087	.000	.007	.203	.339	.496	.668	.846	
		.500	- .053	- .043	.000	.027	.191	.296	.412	.517	.637	
		.750	- .022	- .017	.000	.018	.101	.168	.236	.295	.352	
	Lower	.025	.295	.205	.000	.031	- .061	- .090	- .060	- .122	- .107	
		.250	.330	.246	.000	.055	- .063	- .078	- .100	- .103	- .089	
		.500	.255	.189	.000	.038	- .034	- .050	- .062	- .065	- .059	
		.750	.129	.090	.000	.015	- .017	- .023	- .029	- .033	- .027	
	Total	.025	.424	.327	.000	.057	- .289	- .485	- .669	- .968	- 1.189	
		.250	.428	.333	.000	.048	- .266	- .417	- .596	- .771	- .935	
		.500	.308	.232	.000	.011	- .225	- .346	- .474	- .582	- .696	
		.750	.151	.107	.000	- .003	- .118	- .191	- .265	- .328	- .379	
20°	Upper	.025	- .150	- .142	- .098	.097	.284	.455	.662	.911	1.152	
		.250	- .112	- .101	- .063	.088	.215	.356	.520	.712	.914	
		.500	- .066	- .054	- .027	.080	.181	.284	.393	.509	.633	
		.750	- .030	- .022	- .009	.041	.092	.159	.227	.290	.352	
	Lower	.025	.437	.350	.230	.050	- .007	- .061	- .088	.157	.195	
		.250	.474	.383	.265	.052	- .011	- .064	- .086	.138	.145	
		.500	.371	.298	.203	.040	- .005	- .042	- .054	.068	.041	
		.750	.301	.157	.101	.019	- .001	- .019	- .025	.043	.034	
	Total	.025	.587	.492	.328	- .047	- .291	- .516	- .750	- .754	- .957	
		.250	.586	.484	.328	- .036	- .226	- .420	- .606	- .574	- .769	
		.500	.437	.352	.230	- .040	- .186	- .326	- .447	- .577	- .592	
		.750	.231	.179	.110	- .022	- .093	- .176	- .252	- .347	- .386	
25°	Upper	.025	- .132	- .113	- .067	- .006	.163	.344	.631	.736	.846	1.112
		.250	- .096	- .084	- .046	- .001	.108	.230	.523	.566	.767	1.001
		.500	- .055	- .046	- .020	- .006	.080	.173	.353	.406	.531	.670
		.750	- .032	- .017	- .004	.008	.043	.088	.201	.226	.291	.357
	Lower	.025	.651	.535	.390	.260	.236	.188	.147	.106	.134	.167
		.250	.678	.563	.426	.275	.157	.055	.041	.072	.102	.123
		.500	.513	.437	.331	.212	.117	.042	.033	.049	.067	.082
		.750	.281	.235	.174	.106	.060	.021	.013	.024	.033	.041
	Total	.025	.783	.548	.457	.266	.073	- .156	- .484	- .630	- .712	- .945
		.250	.774	.547	.472	.276	.049	- .175	- .482	- .494	- .665	- .878
		.500	.568	.483	.351	.206	.037	- .131	- .320	- .357	- .464	- .588
		.750	.303	.252	.178	.098	.017	- .067	- .188	- .202	- .258	- .316

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (b) $A = 2$ triangular wing, $r/s = 0.2$

a_b	y/s	δ_w											
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	
0°	Upper	.025	-1.30	-1.23	-1.31	-1.15	-1.17	-1.04	-0.88	-0.63	-0.28	-0.09	.017
		.250	-0.97	-0.94	-1.05	-0.99	-1.02	-0.97	-0.83	-0.63	-0.35	-0.16	.011
		.500	-0.64	-0.65	-0.72	-0.67	-0.69	-0.66	-0.61	-0.50	-0.28	-0.10	.017
		.750	-0.29	-0.30	-0.35	-0.34	-0.35	-0.34	-0.31	-0.25	-0.14	-0.06	.010
		.875	-0.13	-0.14	-0.17	-0.17	-0.18	-0.17	-0.15	-0.13	-0.07	-0.03	.005
	Lower	.025	1.657	1.410	1.086	0.834	0.585	0.395	0.250	0.109	0.060	0.35	.017
		.250	1.255	1.078	0.870	0.670	0.504	0.367	0.239	0.125	0.076	0.40	.011
		.500	.799	.714	.587	0.476	0.375	0.276	0.198	0.106	0.069	0.41	.017
		.750	.413	.366	.313	0.268	0.218	0.167	0.123	0.073	0.050	0.29	.010
		.875	.211	.185	.162	0.139	0.118	0.093	0.070	0.046	0.031	0.17	.005
4°	Total	.025	1.787	1.533	1.217	0.949	0.702	0.499	0.332	0.178	0.088	0.44	.000
		.250	1.352	1.178	0.975	0.769	0.606	0.454	0.322	0.188	0.111	0.56	.000
		.500	.863	.779	.659	0.543	0.444	0.342	0.253	0.156	0.097	0.51	.000
		.750	.442	.396	.348	0.302	0.253	0.201	0.154	0.098	0.064	0.35	.000
		.875	.224	.200	.179	0.156	0.136	0.110	0.085	0.059	0.038	0.20	.000
	Upper	.025	-1.15	-1.09	-0.95	-1.18	-1.07	-1.18	-0.81	-0.49	-0.44	-0.30	-0.19
		.250	-0.92	-0.90	-0.83	-1.02	-0.98	-0.99	-0.69	-0.52	-0.40	-0.37	-0.22
		.500	-0.60	-0.59	-0.53	-0.68	-0.64	-0.64	-0.53	-0.40	-0.36	-0.23	-0.09
		.750	-0.28	-0.28	-0.26	-0.34	-0.32	-0.31	-0.27	-0.20	-0.17	-0.11	-0.03
		.875	-0.13	-0.13	-0.12	-0.17	-0.15	-0.14	-0.10	-0.09	-0.05	-0.05	-0.02
6°	Lower	.025	1.611	1.597	1.396	1.107	0.809	0.561	0.362	0.226	0.142	0.94	.054
		.250	1.762	1.632	0.973	0.811	0.640	0.461	0.320	0.218	0.139	0.91	.052
		.500	.833	.755	.637	0.551	0.440	0.352	0.247	0.167	0.109	0.75	.045
		.750	.442	.403	.352	0.397	0.246	0.197	0.147	0.105	0.074	0.54	.034
		.875	.227	.209	.185	0.161	0.134	0.108	0.084	0.062	0.045	0.33	.019
	Total	.025	1.726	1.706	1.491	1.225	0.916	0.679	0.443	0.275	0.186	1.24	.073
		.250	1.854	1.323	1.056	0.913	0.738	0.580	0.410	0.277	0.191	1.28	.074
		.500	.893	.814	.690	0.619	0.504	0.415	0.300	0.207	0.145	0.98	.054
		.750	.470	.431	.378	0.319	0.278	0.228	0.174	0.126	0.091	0.65	.037
		.875	.240	.223	.197	0.178	0.151	0.123	0.098	0.072	0.054	0.30	.021
10°	Upper	.025	-1.29	-1.19	-1.09	-1.19	-1.13	-1.00	-0.82	-0.81	-0.81	-0.72	
		.250	-0.92	-0.98	-0.94	-1.06	-1.05	-0.98	-0.86	-0.86	-0.86	-0.73	
		.500	-0.64	-0.64	-0.60	-0.71	-0.69	-0.65	-0.57	-0.57	-0.58	-0.49	
		.750	-0.29	-0.30	-0.29	-0.34	-0.34	-0.32	-0.29	-0.29	-0.29	-0.21	
		.875	-0.14	-0.15	-0.15	-0.17	-0.17	-0.16	-0.15	-0.15	-0.15	-0.10	
	Lower	.025	1.366	1.202	1.065	0.902	0.668	0.497	0.335	0.229	0.199	1.09	
		.250	1.854	1.352	0.895	0.721	0.559	0.421	0.291	0.215	0.151	0.96	
		.500	.872	.700	0.595	0.493	0.393	0.305	0.215	0.151	0.78		
		.750	.443	.390	0.334	0.279	0.225	0.180	0.132	0.097	0.055		
		.875	.257	.203	0.177	0.151	0.124	0.101	0.076	0.057	0.033		
12°	Total	.025	1.495	1.321	1.174	1.021	0.781	0.597	0.417	0.310	0.181		
		.250	1.704	1.450	0.989	0.827	0.604	0.519	0.377	0.285	0.169		
		.500	.936	.764	0.655	0.565	0.462	0.370	0.272	0.209	0.127		
		.750	.478	.420	0.363	0.313	0.289	0.218	0.161	0.126	0.076		
		.875	.271	.218	0.192	0.160	0.141	0.117	0.091	0.072	0.043		
	Upper	.025	-1.09	-1.29	-1.26	-1.23	-1.05	-1.13	-1.03	-1.06	-1.14		
		.250	-0.87	-1.06	-1.02	-1.01	-0.94	-1.00	-0.92	-0.92	-0.95		
		.500	-0.54	-0.69	-0.67	-0.65	-0.59	-0.65	-0.59	-0.59	-0.63		
		.750	-0.24	-0.31	-0.32	-0.31	-0.29	-0.32	-0.29	-0.29	-0.29		
		.875	-0.11	-0.15	-0.16	-0.15	-0.16	-0.16	-0.15	-0.14	-0.14		
14°	Lower	.025	1.174	1.075	0.940	0.833	0.613	0.436	0.339	0.264	0.194		
		.250	1.579	1.343	0.809	0.687	0.539	0.398	0.300	0.217	0.164		
		.500	.832	.719	0.575	0.469	0.387	0.294	0.217	0.167	0.132		
		.750	.451	.393	0.333	0.245	0.201	0.169	0.133	0.107	0.085		
		.875	.258	.207	0.180	0.150	0.123	0.096	0.077	0.064	0.051		
	Total	.025	1.283	1.204	1.068	0.956	0.718	0.549	0.442	0.370	0.308		
		.250	1.666	1.349	0.912	0.788	0.627	0.449	0.382	0.303	0.259		
		.500	.886	.788	0.542	0.554	0.440	0.349	0.276	0.209	0.164		
		.750	.475	.424	0.365	0.302	0.250	0.201	0.162	0.136	0.114		
		.875	.243	.222	0.196	0.165	0.139	0.113	0.092	0.078	0.065		

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (b) $A = 2$ triangular wing, $r/s = 0.2$ - Continued

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (b) A = 2 triangular wing, r/s = 0.2 - Continued

a_B	y/s	δ_w										
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°
15°	Upper	- .165	- .150	- .171	- .165	- .153	- .139	- .129	- .068			
		- .128	- .120	- .135	- .132	- .126	- .115	- .107	- .059			
		- .080	- .075	- .089	- .085	- .080	- .072	- .065	- .035			
		- .038	- .032	- .044	- .042	- .039	- .035	- .030	- .019			
		.019	.018	.022	.021	.020	.017	.014	.009			
	Lower	1.127	.842	.938	.731	.569	.456	.409	.317			
		1.508	1.228	.690	.718	.551	.423	.341	.262			
		.901	.752	.535	.509	.396	.309	.251	.195			
		.474	.404	.449	.286	.227	.183	.152	.123			
		.245	.214	.185	.155	.126	.103	.087	.072			
20°	Upper	1.292	.992	1.109	.896	.722	.595	.538	.385			
		1.636	1.348	1.025	.850	.677	.538	.448	.321			
		.981	.827	.784	.594	.476	.381	.316	.230			
		.512	.441	.393	.328	.266	.218	.182	.142			
		.264	.232	.207	.176	.146	.120	.101	.081			
	Lower	- .133	- .131	- .126	- .120	- .110	- .100	- .109				
		- .103	- .103	- .101	- .098	- .092	- .080	- .069				
		- .068	- .068	- .066	- .063	- .059	- .055	- .050				
		- .033	- .033	- .033	- .031	- .029	- .029	- .023				
		- .016	- .016	- .016	- .015	- .015	- .015	- .015				
25°	Upper	.828	.864	.822	.704	.647	.619	.530				
		1.683	1.301	.951	.750	.600	.500	.419				
		.965	.811	.667	.533	.429	.360	.304				
		.503	.430	.360	.294	.243	.208	.178				
		.258	.226	.190	.160	.136	.116	.101				
	Lower	.961	.995	.948	.824	.757	.739	.639				
		1.786	1.404	1.052	.848	.692	.600	.512				
		1.033	.879	.733	.596	.488	.425	.364				
		.536	.463	.392	.325	.272	.241	.208				
		.274	.242	.206	.175	.151	.132	.116				
Total	Upper	- .122	- .134	- .130	- .118	- .104	- .108					
		- .094	- .104	- .101	- .095	- .086	- .093					
		- .061	- .068	- .066	- .061	- .055	- .053					
		- .029	- .033	- .032	- .029	- .027	- .029					
		- .014	- .016	- .016	- .014	- .013	- .015					
	Lower	1.255	1.191	.983	.878	.893	.765					
		1.556	1.278	1.023	.848	.724	.599					
		1.019	.879	.720	.603	.516	.432					
		.510	.457	.386	.327	.284	.241					
		.232	.212	.184	.165	.152	.131					
	Total	1.377	1.325	1.113	.996	.997	.873					
		1.650	1.382	1.124	.943	.810	.692					
		1.080	.947	.786	.664	.571	.491					
		.539	.490	.418	.356	.311	.270					
		.246	.228	.200	.179	.165	.146					

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (b) $A = 2$ triangular wing, $r/s = 0.2$ - Concluded

a_B	y/s	δ_w										
		-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°	
15°	Upper	.025	-.093	-.077	-.058	.007	1.04	1.74	3.48	4.84	.672	.924
		.250	-.081	-.073	-.058	-.015	.060	1.50	2.57	3.91	.510	.581
		.500	-.050	-.044	-.033	.004	.054	1.05	1.69	2.51	.333	.432
		.750	-.026	-.021	-.014	.014	.044	.074	1.07	1.48	.187	.238
	Lower	.875	-.013	-.011	-.007	.010	.029	.046	.064	.085	.105	.129
		.025	.226	.155	.087	.022	-.015	-.040	-.038	-.079	-.096	-.115
		.250	.203	.149	.091	.027	-.015	-.046	-.057	-.084	-.094	-.097
		.500	.162	.120	.075	.021	-.018	-.040	-.042	-.059	-.064	-.066
	Total	.750	.100	.079	.052	.017	-.006	-.019	-.021	-.029	-.032	-.032
		.875	.060	.047	.031	.011	-.002	-.009	-.010	-.015	-.016	-.016
		.025	.319	.232	.145	.015	-.119	-.214	-.386	-.563	-.768	-.1039
		.250	.284	.222	.149	.042	-.075	-.196	-.314	-.475	-.604	-.778
20°	Upper	.500	.212	.164	.108	.017	-.072	-.145	-.211	-.310	-.397	-.498
		.750	.126	.100	.066	.003	-.050	-.093	-.128	-.177	-.219	-.270
		.875	.073	.058	.038	.001	-.031	-.055	-.074	-.100	-.121	-.145
	Lower	.025	.092	-.068	-.029	.046	1.42	2.24		.447		
		.250	.083	-.066	-.039	.010	.078	1.47		.381		
		.500	-.053	-.041	-.023	.016	.059	.096		.236		
		.750	-.026	-.020	-.011	.012	.070	.092		.130		
	Total	.875	-.013	-.011	-.005	.006	.022	.036		.072		
		.025	.363	.280	.196	.105	.044	-.006		-.055		
		.250	.318	.251	.178	.098	.041	-.004		-.062		
		.500	.239	.191	.134	.071	.018	-.019		-.053		
25°	Upper	.750	.142	.114	.082	.045	.009	-.012		-.027		
		.875	.082	.057	.049	.028	.006	-.005		-.014		
	Lower	.025	.455	.348	.225	.059	-.098	-.230		-.502		
		.250	.401	.317	.217	.088	-.037	-.151		-.443		
		.500	.292	.232	.157	.055	-.041	-.115		-.289		
		.750	.168	.134	.093	.033	-.061	-.104		-.157		
	Total	.875	.095	.078	.054	.022	-.016	-.041		-.086		
		.025	-.090	-.055	-.016	.059	.099	1.72	2.59	.401	.494	.739
		.250	-.083	-.062	-.040	.017	.090	1.64	2.68	.345	.495	.648
		.500	-.052	-.036	-.032	.008	.060	1.00	1.60	.241	.334	.446
	Lower	.750	-.026	-.019	-.018	.001	.035	.058	.088	1.24	.161	.205
		.875	-.013	-.010	-.010	-.001	.018	.032	.047	.064	.084	.104
		.025	.589	.479	.362	.236	.114	.025	-.013	-.029	-.041	-.068
		.250	.495	.406	.312	.207	.130	.049	.009	-.027	-.041	-.069
	Total	.500	.363	.300	.228	.146	.081	.010	-.018	-.037	-.043	-.058
		.750	.203	.169	.130	.085	.044	-.006	-.017	-.022	-.023	-.030
		.875	.112	.095	.074	.049	.026	-.004	-.009	-.011	-.011	-.015
		.025	.679	.534	.378	.177	.015	-.147	-.272	-.430	-.535	-.807
Total	Upper	.250	.578	.468	.352	.190	.040	-.115	-.259	-.372	-.536	-.717
		.500	.415	.336	.260	.136	.021	-.090	-.178	-.278	-.377	-.504
		.750	.239	.188	.148	.084	.009	-.064	-.105	-.146	-.184	-.235
		.875	.125	.105	.084	.048	.008	-.036	-.056	-.075	-.095	-.119

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
 (c) $A = 2$ rectangular wing, $r/s = 0.2$

α_B	y/s	δ_w											
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	
0°	Upper	.025		- .081	- .074	- .076	- .066	- .056	- .034	- .018	.001	.015	
		.250		- .089	- .084	- .084	- .079	- .073	- .051	- .033	- .056	.017	
		.563		- .092	- .087	- .086	- .083	- .077	- .060	- .030	- .020	.006	
		.875		- .090	- .085	- .082	- .076	- .071	- .046	- .030	- .010	.010	
	Lower	.025		.825	.602	.427	.317	.280	.141	.081	.049	.015	
		.250		1.004	.842	.648	.476	.329	.204	.122	.068	.017	
		.563		.991	.849	.648	.468	.313	.190	.108	.047	.006	
		.875		.948	.765	.574	.419	.280	.176	.098	.046	.010	
	Total	.025		.906	.576	.503	.383	.276	.175	.099	.048	.000	
		.250		1.093	.926	.732	.655	.402	.255	.155	.124	.000	
		.563		1.083	.936	.734	.551	.390	.250	.150	.067	.000	
		.875		1.038	.850	.656	.495	.351	.228	.128	.056	.000	
3°	Upper	.025		- .087	- .079	- .068	- .062	- .061	- .053	- .044	- .033	- .019	
		.250		- .092	- .086	- .080	- .073	- .074	- .067	- .061	- .050	- .084	
		.563		- .093	- .087	- .079	- .075	- .076	- .068	- .062	- .051	- .025	
		.875		- .090	- .086	- .077	- .073	- .067	- .059	- .050	- .039	- .013	
	Lower	.025		.883	.795	.570	.416	.299	.188	.135	.093	.057	
		.250		1.114	.936	.770	.571	.411	.269	.177	.112	.066	
		.563		1.082	.935	.761	.559	.389	.244	.154	.090	.046	
		.875		1.080	.854	.669	.483	.340	.217	.137	.081	.042	
	Total	.025		.970	.874	.638	.478	.360	.241	.179	.126	.076	
		.250		1.206	1.022	.850	.644	.485	.336	.238	.162	.090	
		.563		1.175	1.022	.840	.534	.465	.318	.216	.141	.071	
		.875		1.110	.940	.746	.555	.407	.276	.187	.120	.055	
6°	Upper	.025		- .087	- .092	- .084	- .073	- .072	- .069	- .049	- .037		
		.250		- .094	- .096	- .092	- .088	- .085	- .071	- .065	- .044		
		.563		- .096	- .101	- .090	- .088	- .086	- .066	- .062	- .041		
		.875		- .093	- .096	- .095	- .084	- .073	- .061	- .045	- .032		
	Lower	.025		.754	.730	.562	.412	.299	.224	.172	.125		
		.250		.979	.836	.670	.498	.345	.249	.181	.125		
		.563		.980	.843	.665	.482	.320	.222	.155	.104		
		.875		.930	.764	.578	.416	.280	.193	.137	.093		
	Total	.025		.841	.822	.646	.485	.371	.293	.221	.168		
		.250		1.073	.932	.762	.580	.430	.320	.246	.169		
		.563		1.086	.944	.756	.570	.406	.288	.217	.145		
		.875		1.022	.860	.673	.500	.353	.254	.182	.125		
10°	Upper	.025		- .088	- .086	- .080	- .076	- .076	- .078	- .064			
		.250		- .091	- .090	- .084	- .081	- .080	- .068	- .066			
		.563		- .090	- .087	- .087	- .082	- .077	- .074	- .062			
		.875		- .087	- .083	- .077	- .074	- .074	- .069	- .048			
	Lower	.025		.539	.546	.414	.312	.256	.195				
		.250		.784	.629	.466	.358	.281	.211				
		.563		.831	.659	.476	.357	.271	.199				
		.875		.753	.579	.416	.315	.242	.177				
	Total	.025		.627	.638	.494	.388	.334	.259				
		.250		.875	.719	.550	.439	.361	.261				
		.563		.921	.746	.558	.434	.345	.261				
		.875		.840	.662	.493	.389	.311	.225				

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE
BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Continued
(c) $A = 2$ rectangular wing, $r/s = 0.2$ - Continued

a_B	y/s	δ_w									
		-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°
0°	Upper	.025 .250 .563 .875									
	Lower	.025 .250 .563 .875									
	Total	.025 .250 .563 .875									
3°	Upper	.025 .250 .563 .875	.001 .003 .005 .012	.016 .036 .095 .042	.044 .037 .096 .096	.108 .195 .199 .190	.200 .318 .322 .304	.307 .470 .487 .447	.474 .639 .658 .598	.588 .833 .840 .781	.741 1.001 1.014 .953
	Lower	.025 .250 .563 .875	.027 .026 .008 .011	.007 .004 .018 .012	-.018 -.034 -.046 -.036	-.048 -.063 -.070 -.062	-.062 -.073 -.078 -.073	-.076 -.084 -.088 -.083	-.081 -.086 -.088 -.084	-.085 -.090 -.093 -.091	-.089 -.095 -.098 -.095
	Total	.025 .250 .563 .875	.028 .023 .003 .001	-.009 -.040 -.055 -.054	-.062 -.129 -.142 -.132	-.156 -.258 -.269 -.252	-.262 -.391 -.400 -.377	-.383 -.554 -.575 -.530	-.555 -.725 -.746 -.682	-.713 -.923 -.933 -.872	-.830 -1.096 -1.112 -1.050
6°	Upper	.025 .250 .563 .875	.033 .043 .046 .020	-.086 -.022 -.003 -.020	-.004 .028 .050 -.061	.031 .102 .129 .140	.098 .208 .231 .227	.209 .334 .385 .375	.348 .505 .556 .533	.548 .683 .736 .696	.69 ; .88 ; .93 ; .89 ;
	Lower	.025 .250 .563 .875	.079 .075 .056 .051	.043 .038 .024 .030	.009 .000 -.014 -.010	-.027 -.033 -.041 -.036	-.043 -.049 -.052 -.048	-.059 -.063 -.065 -.061	-.069 -.072 -.070 -.071	-.075 -.077 -.076 -.076	-.07 -.08 -.080 -.083
	Total	.025 .250 .563 .875	.112 .118 .102 .071	.069 .060 .027 .010	-.013 -.028 -.064 -.071	-.058 -.135 -.170 -.176	-.141 -.257 -.283 -.275	-.268 -.397 -.450 -.436	-.417 -.577 -.626 -.604	-.623 -.760 -.812 -.772	-.770 -.969 -1.016 -.973
10°	Upper	.025 .250 .563 .875	.062 .071 .059 .042	-.053 -.059 -.040 -.017	-.051 -.040 -.008 -.015	-.018 .013 .063 .082	.037 .097 .156 .179	.102 .203 .276 .291	.188 .325 .413 .422	.329 .507 .615 .591	.523 .683 .762
	Lower	.025 .250 .563 .875	.140 .156 .148 .129	.087 .047 .089 .081	.039 -.009 -.016 -.010	-.013 -.043 -.049 -.038	-.039 -.063 -.065 -.059	-.061 -.063 -.070 -.066	-.067 -.067 -.070 -.066	-.065 -.069 -.070 -.069	-.078 -.080 -.080 -.080
	Total	.025 .250 .563 .875	.202 .227 .201 .171	.140 .160 .129 .098	.090 .087 .044 .022	-.005 -.022 -.079 -.098	-.076 -.140 -.205 -.217	-.163 -.266 -.341 -.350	-.255 -.392 -.483 -.488	-.394 -.576 -.685 -.660	-.601 -.763 -.842 -.835

TABLE III.- SPAN LOADING COEFFICIENTS OF THE WINGS IN THE PRESENCE OF THE
BODY - UPPER SURFACE, LOWER SURFACE, AND TOTAL - Concluded
(c) A = 2 rectangular wing, r/s = 0.2 - Concluded

α_B	y/s	δ_w										
		-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°	
15°	Upper	.025	-.064	-.078	-.060	-.028	.037	.098	.193	.294	.456	
		.250	-.066	-.073	-.048	-.003	.071	.172	.302	.455	.636	
		.563	-.056	-.060	-.022	.049	.119	.239	.383	.561	.752	
		.875	-.046	-.033	-.004							
	Lower	.025	.206	.148	.087	.018	-.022	-.051	-.067	-.074	-.083	
		.250	.248	.183	.115	.034	-.015	-.047	-.062	-.072	-.080	
		.563	.251	.182	.105	.028	-.019	-.053	-.067	-.075	-.082	
		.875	.221	.164	.099	.032	-.009	-.025	-.057	-.066	-.077	
	Total	.025	.270	.226	.147	.046	-.059	-.149	-.260	-.368	.539	
		.250	.314	.256	.163	.037	-.086	-.219	-.364	-.587	.716	
		.563	.307	.242	.127	-.021	-.138	-.292	-.450	-.636	.834	
		.875	.267	.197	.103	-.012	-.154	-.290	-.447	-.622	.808	
20°	Upper	.025	-.075	-.078	-.055	-.023	.042	.131	.208	.325	.485	
		.250	-.074	-.075	-.043	-.009	.065	.167	.295	.445	.618	
		.563	-.065	-.060	-.021	.026	.105	.214	.354	.522	.720	
		.875	-.051	-.046	-.003	.050	.115	.209	.329	.464	.629	
	Lower	.025	.333	.254	.162	.066	.024	-.017	-.040	-.059	-.068	
		.250	.403	.312	.213	.100	.038	-.009	-.038	-.057	-.066	
		.563	.431	.331	.221	.104	.038	-.010	-.040	-.057	-.068	
		.875	.389	.301	.204	.101	.048	.001	-.029	-.048	-.064	
	Total	.025	.408	.332	.217	.089	-.018	-.148	-.248	-.384	.553	
		.250	.477	.387	.256	.109	-.027	-.176	-.333	.502	.684	
		.563	.496	.391	.242	.078	-.067	-.224	-.394	.579	.788	
		.875	.440	.347	.207	.051	-.067	-.208	-.358	.512	.693	
25°	Upper	.025	-.066	-.069	-.046	.006	.085	.165	.227		.556	
		.250	-.068	-.063	-.043	.015	.089	.181	.302		.634	
		.563	-.065	-.062	-.023	.043	.123	.214	.331		.709	
		.875	-.060	-.045	-.023	.029	.079	.130	.228		.514	
	Lower	.025	.476	.387	.267	.170	.078	.018	-.019		.054	
		.250	.578	.469	.343	.218	.115	.043	-.016		.058	
		.563	.631	.507	.366	.226	.118	.042	-.018		.059	
		.875	.517	.421	.308	.188	.089	.023	-.027		.064	
	Total	.025	.542	.456	.313	.164	-.007	-.147	-.246		.610	
		.250	.646	.532	.386	.203	-.026	-.138	-.318		.692	
		.563	.696	.569	.389	.185	-.005	-.172	-.349		.768	
		.875	.577	.466	.331	.159	.010	-.107	-.255		.578	

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(a) $A = \frac{1}{4}$ triangular wing, $r/s = 0.2$ - Concluded

a_B	x/r	δ_w									
		-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°
0°	1.134	- .001	- .001	- .007	- .001	- .007	- .002	- .000	- .002	- .001	.000
	1.259	- .003	- .002	- .006	- .002	- .001	- .001	- .003	- .003	- .000	.000
	1.384	- .001	- .003	- .009	- .001	- .001	- .000	- .008	- .003	- .009	.001
	1.509	- .002	- .005	- .006	- .009	- .017	- .000	- .008	- .003	- .009	.001
	1.634	- .010	- .001	- .014	- .019	- .011	- .007	- .005	- .009	- .023	.032
0°	1.756	- .010	- .004	- .024	- .048	- .054	- .034	- .047	- .045	- .072	.082
	1.884	- .013	- .004	- .024	- .043	- .062	- .013	- .049	- .097	- .072	.043
	2.009	- .011	- .007	- .027	- .037	- .054	- .015	- .048	- .073	- .046	.031
	2.134	- .005	- .007	- .024	- .037	- .038	- .032	- .033	- .024	- .035	.023
	2.259	- .001	- .010	- .026	- .037	- .037	- .021	- .016	- .014	- .033	.030
	2.384	- .005	- .012	- .024	- .024	- .024	- .006	- .009	- .006	- .030	.029
	2.509	- .002	- .007	- .009	- .014	- .011	- .007	- .002	- .003	- .016	.016
3°	1.134	- .002	- .004	- .003	- .001	- .002	- .002	- .002	- .002	- .001	.000
	1.259	- .001	- .000	- .001	- .002	- .001	- .003	- .001	- .001	- .000	.001
	1.384	- .003	- .001	- .003	- .003	- .001	- .002	- .002	- .002	- .002	.002
	1.509	- .007	- .007	- .018	- .019	- .007	- .003	- .003	- .003	- .003	.018
	1.634	- .023	- .023	- .027	- .008	- .005	- .013	- .052	- .045	- .034	.067
3°	1.756	- .021	- .022	- .003	- .007	- .021	- .044	- .054	- .047	- .038	.059
	1.884	- .022	- .022	- .004	- .021	- .027	- .035	- .049	- .068	- .079	.063
	2.009	- .030	- .019	- .001	- .011	- .019	- .021	- .023	- .029	- .031	.031
	2.134	- .026	- .014	- .000	- .008	- .010	- .014	- .016	- .025	- .039	.028
	2.259	- .014	- .005	- .010	- .012	- .013	- .012	- .016	- .033	- .034	.034
	2.384	- .002	- .007	- .012	- .015	- .020	- .016	- .018	- .023	- .025	.034
	2.509	- .004	- .007	- .012	- .015	- .020	- .016	- .018	- .023	- .025	.034
6°	1.134	- .010	- .017	- .007	- .008	- .008	- .007	- .009	- .010	- .009	.010
	1.259	- .002	- .021	- .001	- .001	- .002	- .001	- .000	- .000	- .001	.001
	1.384	- .003	- .008	- .000	- .001	- .001	- .001	- .001	- .000	- .001	.000
	1.509	- .002	- .004	- .003	- .004	- .004	- .002	- .002	- .003	- .003	.001
	1.634	- .035	- .027	- .034	- .017	- .015	- .028	- .072	- .056	- .032	.044
6°	1.756	- .041	- .028	- .021	- .004	- .008	- .036	- .045	- .046	- .065	.080
	1.884	- .039	- .028	- .009	- .006	- .020	- .030	- .037	- .046	- .065	.080
	2.009	- .042	- .033	- .011	- .001	- .010	- .014	- .020	- .026	- .046	.080
	2.134	- .027	- .000	- .005	- .003	- .003	- .014	- .020	- .026	- .046	.080
	2.259	- .017	- .011	- .005	- .002	- .003	- .006	- .002	- .003	- .004	.040
	2.384	- .006	- .011	- .010	- .012	- .005	- .002	- .003	- .004	- .019	.040
	2.509	.015	.009	.002	.000	.010	.013	.007	.007	.004	.021
10°	1.134	- .015	- .025	- .014	- .016	- .015	- .015	- .014	- .015	- .015	.015
	1.259	- .004	- .004	- .003	- .003	- .004	- .004	- .003	- .003	- .003	.002
	1.384	- .001	- .001	- .008	- .008	- .002	- .004	- .003	- .003	- .003	.000
	1.509	- .002	- .002	- .030	- .030	- .004	- .002	- .003	- .003	- .001	.001
	1.634	- .049	- .039	- .036	- .036	- .035	- .033	- .082	- .049	- .124	.144
10°	1.756	- .047	- .039	- .015	- .003	- .028	- .039	- .045	- .047	- .068	.084
	1.884	- .048	- .035	- .003	- .003	- .027	- .038	- .045	- .047	- .068	.084
	2.009	- .061	- .040	- .003	- .005	- .007	- .005	- .008	- .008	- .014	.028
	2.134	- .060	- .045	- .015	- .008	- .005	- .008	- .006	- .006	- .014	.041
	2.259	- .056	- .041	- .008	- .002	- .008	- .020	- .007	- .003	- .003	.010
	2.384	- .017	- .004	- .002	- .001	- .002	- .019	- .021	- .025	- .030	.119
	2.509	.049	.038	.004	.004	.002	.002	.000	.007	.007	.019
15°	1.134	- .017	- .035	- .021	- .020	- .021	- .030	- .021	- .014	- .020	.020
	1.259	- .010	- .009	- .010	- .011	- .009	- .004	- .004	- .011	- .005	.005
	1.384	- .011	- .009	- .011	- .010	- .009	- .004	- .004	- .010	- .004	.004
	1.509	- .004	- .004	- .023	- .041	- .003	- .004	- .003	- .003	- .004	.000
	1.634	- .031	- .031	- .037	- .027	- .017	- .016	- .017	- .027	- .044	.066
15°	1.756	- .056	- .050	- .035	- .024	- .016	- .016	- .017	- .027	- .048	.066
	1.884	- .052	- .036	- .018	- .005	- .004	- .030	- .034	- .037	- .053	.073
	2.009	.075	.047	.029	.007	- .004	- .030	- .010	- .009	- .018	.034
	2.134	.082	.063	.033	.015	- .005	- .008	- .008	- .003	- .003	.014
	2.259	.084	.062	.029	.011	- .002	- .003	- .013	- .002	- .004	.001
	2.384	.065	.044	.017	.003	- .012	- .016	- .027	- .017	- .010	.021
	2.509	.081	.061	.038	.012	- .004	- .005	- .034	- .006	- .002	.011
20°	1.134	- .017	- .035	- .021	- .020	- .017	- .031	- .021	- .014	- .020	.020
	1.259	- .011	- .009	- .011	- .010	- .009	- .004	- .004	- .011	- .004	.004
	1.384	- .011	- .009	- .011	- .010	- .009	- .004	- .004	- .010	- .004	.004
	1.509	- .004	- .004	- .023	- .041	- .003	- .004	- .003	- .003	- .004	.000
	1.634	- .031	- .031	- .037	- .027	- .017	- .016	- .017	- .027	- .044	.066
20°	1.756	- .056	- .050	- .035	- .024	- .016	- .016	- .017	- .027	- .048	.066
	1.884	- .052	- .036	- .018	- .005	- .004	- .030	- .034	- .037	- .053	.073
	2.009	.075	.047	.029	.007	- .004	- .003	- .010	- .009	- .018	.034
	2.134	.082	.063	.033	.015	- .005	- .008	- .008	- .003	- .003	.014
	2.259	.084	.062	.029	.011	- .002	- .003	- .013	- .002	- .004	.001
	2.384	.065	.044	.017	.003	- .012	- .016	- .027	- .017	- .010	.021
	2.509	.081	.061	.038	.012	- .004	- .005	- .034	- .006	- .002	.011
25°	1.134	- .030	- .034	- .032	- .032	- .031	- .026	- .030	- .030	- .032	.032
	1.259	- .005	- .001	- .004	- .004	- .003	- .007	- .005	- .005	- .005	.003
	1.384	- .005	- .003	- .005	- .005	- .004	- .010	- .008	- .008	- .008	.003
	1.509	- .001	- .001	- .028	- .048	- .002	- .003	- .002	- .001	- .001	.000
	1.634	- .017	- .028	- .016	- .002	- .013	- .001	- .007	- .021	- .036	.069
25°	1.756	- .067	- .038	- .028	- .004	- .019	- .001	- .025	- .090	- .093	.093
	1.884	- .065	- .040	- .017	- .005	- .008	- .010	- .024	- .027	- .020	.031
	2.009	- .086	- .038	- .018	- .004	- .008	- .008	- .007	- .014	- .020	.020
	2.134	- .092	- .038	- .014	- .003	- .004	- .006	- .008	- .007	- .012	.012
	2.259	- .071	- .021	- .003	- .006	- .012	- .002	- .008	- .007	- .002	.002
	2.384	- .097	- .039	- .016	- .013	- .005	- .014	- .019	- .019	- .019	.012
	2.509	.099	.050	.031	.026	.019	.026	.026	.029	.030	.020

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(b) A = 2 triangular wing, r/s = 0.2

a_B	x/r	δ_w										
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°
0°	1.134	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
	1.259	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.006	-0.002	-0.001	-0.000	-0.000
	1.384	-0.003	-0.000	-0.000	-0.000	-0.000	-0.018	-0.089	-0.116	-0.055	-0.022	-0.000
	1.509	-0.119	-0.198	-0.17	-0.17	-0.174	-0.182	-0.21	-0.040	-0.32	-0.19	-0.09
	1.634	-0.100	-0.139	-0.094	-0.071	-0.083	-0.088	-0.079	-0.056	-0.027	-0.123	-0.001
	1.756	-0.126	-0.101	-0.067	-0.074	-0.089	-0.088	-0.083	-0.057	-0.042	-0.026	-0.004
	1.884	-0.077	-0.099	-0.111	-0.124	-0.126	-0.103	-0.079	-0.061	-0.052	-0.026	-0.004
	2.009	-0.057	-0.088	-0.099	-0.117	-0.124	-0.111	-0.077	-0.047	-0.036	-0.016	-0.001
	2.134	-0.061	-0.048	-0.066	-0.057	-0.099	-0.098	-0.067	-0.059	-0.040	-0.018	-0.000
	2.259	-0.047	-0.047	-0.044	-0.051	-0.071	-0.061	-0.054	-0.049	-0.030	-0.013	-0.003
3°	1.134	-0.014	-0.01	-0.000	-0.001	-0.000	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
	1.259	-0.004	-0.001	-0.000	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001	-0.001
	1.384	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
	1.509	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
	1.634	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
	1.756	-0.013	-0.019	-0.019	-0.017	-0.019	-0.018	-0.015	-0.011	-0.007	-0.004	-0.001
	1.884	-0.006	-0.006	-0.003	-0.007	-0.014	-0.014	-0.014	-0.009	-0.007	-0.004	-0.001
	2.009	-0.009	-0.013	-0.013	-0.012	-0.015	-0.017	-0.014	-0.005	-0.003	-0.001	-0.000
	2.134	-0.007	-0.007	-0.009	-0.013	-0.015	-0.014	-0.010	-0.009	-0.007	-0.004	-0.001
	2.259	-0.000	-0.009	-0.017	-0.027	-0.061	-0.065	-0.085	-0.067	-0.044	-0.029	-0.010
6°	1.134	-0.010	-0.026	-0.017	-0.017	-0.017	-0.017	-0.017	-0.017	-0.017	-0.017	-0.017
	1.259	-0.010	-0.021	-0.014	-0.014	-0.014	-0.014	-0.014	-0.014	-0.014	-0.014	-0.014
	1.384	-0.015	-0.042	-0.072	-0.071	-0.088	-0.088	-0.088	-0.088	-0.045	-0.030	-0.022
	1.609	-0.131	-0.388	-0.325	-0.125	-0.051	-0.086	-0.074	-0.064	-0.046	-0.037	-0.027
	1.634	-0.239	-0.193	-0.182	-0.151	-0.144	-0.101	-0.079	-0.061	-0.051	-0.042	-0.032
	1.756	-0.272	-0.214	-0.178	-0.150	-0.140	-0.133	-0.130	-0.099	-0.080	-0.064	-0.054
	1.884	-0.172	-0.165	-0.173	-0.169	-0.164	-0.139	-0.108	-0.129	-0.098	-0.078	-0.064
	2.009	-0.066	-0.090	-0.118	-0.118	-0.126	-0.135	-0.110	-0.107	-0.100	-0.073	-0.064
	2.134	-0.114	-0.095	-0.066	-0.135	-0.179	-0.138	-0.114	-0.092	-0.066	-0.055	-0.034
	2.259	-0.101	-0.078	-0.079	-0.110	-0.119	-0.119	-0.181	-0.092	-0.065	-0.041	-0.024
10°	1.134	-0.056	-0.003	-0.01	-0.001	-0.002	-0.007	-0.002	-0.004	-0.001	-0.001	-0.001
	1.259	-0.071	-0.064	-0.014	-0.004	-0.004	-0.004	-0.005	-0.005	-0.005	-0.005	-0.005
	1.384	-0.015	-0.042	-0.072	-0.071	-0.088	-0.088	-0.088	-0.088	-0.045	-0.030	-0.022
	1.609	-0.313	-0.388	-0.325	-0.125	-0.051	-0.086	-0.074	-0.064	-0.046	-0.037	-0.027
	1.634	-0.239	-0.193	-0.182	-0.151	-0.144	-0.101	-0.079	-0.061	-0.051	-0.042	-0.032
	1.756	-0.272	-0.214	-0.178	-0.150	-0.140	-0.133	-0.130	-0.099	-0.080	-0.064	-0.054
	1.884	-0.159	-0.189	-0.189	-0.189	-0.165	-0.133	-0.113	-0.165	-0.119	-0.092	-0.072
	2.009	-0.036	-0.068	-0.107	-0.119	-0.167	-0.158	-0.127	-0.137	-0.129	-0.093	-0.078
	2.134	-0.057	-0.073	-0.079	-0.086	-0.124	-0.158	-0.134	-0.100	-0.092	-0.065	-0.055
	2.259	-0.043	-0.053	-0.057	-0.073	-0.090	-0.124	-0.087	-0.043	-0.039	-0.021	-0.019
15°	1.134	-0.026	-0.024	-0.013	-0.013	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019	-0.019
	1.259	-0.090	-0.041	-0.022	-0.022	-0.008	-0.008	-0.008	-0.008	-0.008	-0.008	-0.008
	1.384	-0.025	-0.064	-0.085	-0.111	-0.157	-0.196	-0.136	-0.147	-0.138	-0.134	-0.124
	1.509	-0.160	-0.320	-0.266	-0.057	-0.082	-0.090	-0.070	-0.058	-0.056	-0.046	-0.036
	1.634	-0.442	-0.288	-0.239	-0.184	-0.165	-0.125	-0.098	-0.085	-0.075	-0.065	-0.056
	1.756	-0.360	-0.299	-0.245	-0.184	-0.144	-0.129	-0.141	-0.135	-0.115	-0.091	-0.081
	1.884	-0.159	-0.189	-0.189	-0.189	-0.165	-0.133	-0.113	-0.165	-0.119	-0.092	-0.072
	2.009	-0.036	-0.068	-0.107	-0.119	-0.167	-0.158	-0.127	-0.137	-0.129	-0.093	-0.078
	2.134	-0.037	-0.073	-0.079	-0.086	-0.124	-0.158	-0.134	-0.100	-0.092	-0.065	-0.055
	2.259	-0.043	-0.053	-0.057	-0.073	-0.090	-0.124	-0.087	-0.043	-0.039	-0.021	-0.019
20°	1.134	-0.010	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009
	1.259	-0.101	-0.134	-0.145	-0.145	-0.241	-0.241	-0.050	-0.045	-0.047	-0.044	-0.044
	1.384	-0.110	-0.110	-0.125	-0.125	-0.251	-0.251	-0.096	-0.091	-0.078	-0.073	-0.058
	1.609	-0.344	-0.266	-0.225	-0.201	-0.269	-0.269	-0.166	-0.148	-0.128	-0.104	-0.061
	1.634	-0.239	-0.193	-0.182	-0.151	-0.144	-0.146	-0.162	-0.151	-0.137	-0.104	-0.081
	1.756	-0.272	-0.214	-0.178	-0.150	-0.140	-0.133	-0.120	-0.117	-0.101	-0.071	-0.051
	1.884	-0.141	-0.189	-0.189	-0.189	-0.165	-0.133	-0.113	-0.165	-0.119	-0.092	-0.072
	2.009	-0.045	-0.080	-0.122	-0.178	-0.200	-0.200	-0.156	-0.186	-0.167	-0.121	-0.101
	2.134	-0.037	-0.080	-0.122	-0.177	-0.200	-0.200	-0.147	-0.184	-0.161	-0.121	-0.101
	2.259	-0.038	-0.048	-0.072	-0.117	-0.179	-0.179	-0.107	-0.161	-0.141	-0.094	-0.086
25°	1.134	-0.040	-0.040	-0.003	-0.001	-0.002	-0.002	-0.005	-0.005	-0.005	-0.005	-0.005
	1.259	-0.090	-0.041	-0.022	-0.004	-0.004	-0.004	-0.005	-0.005	-0.005	-0.005	-0.005
	1.384	-0.025	-0.064	-0.085	-0.111	-0.157	-0.196	-0.136	-0.147	-0.138	-0.134	-0.124
	1.509	-0.160	-0.320	-0.266	-0.057	-0.082	-0.090	-0.070	-0.058	-0.056	-0.046	-0.036
	1.634	-0.339	-0.266	-0.225	-0.201	-0.269	-0.269	-0.188	-0.166	-0.136	-0.103	-0.077
	1.756	-0.272	-0.214	-0.178	-0.150	-0.140	-0.133	-0.120	-0.117	-0.101	-0.071	-0.051
	1.884	-0.159	-0.189	-0.189	-0.189	-0.165	-0.133	-0.113	-0.165	-0.119	-0.092	-0.072
	2.009	-0.036	-0.068	-0.107	-0.119	-0.167	-0.158	-0.127	-0.137	-0.129	-0.093	-0.078
	2.134	-0.037	-0.073	-0.079	-0.086	-0.124	-0.158	-0.134	-0.107	-0.092	-0.065	-0.055
	2.259	-0.040	-0.071	-0.094	-0.104	-0.129	-0.129	-0.079	-0.147	-0.131	-0.101	-0.077
20°	1.134	-0.026	-0.026	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009
	1.259	-0.090	-0.041	-0.022	-0.004	-0.004	-0.004	-0.005	-0.005	-0.005	-0.005	-0.005
	1.384	-0.025	-0.064	-0.085	-0.111	-0.157	-0.196	-0.136	-0.147	-0.138	-0.134	-0.124
	1.609	-0.160	-0.320	-0.266	-0.057	-0.082	-0.090	-0.070	-0.058	-0.056	-0.046	-0.036
	1.634	-0.339	-0.266	-0.225	-0.201	-0.269	-0.269	-0.188	-0.166	-0.136	-0.103	-0.077
	1.756	-0.272	-0.214	-0.178	-0.150	-0.140	-0.133	-0.120	-0.117	-0.101	-0.071	-0.051
	1.884	-0.159	-0.189	-0.189	-0.189	-0.165	-0.133	-0.113	-0.165	-0.119	-0.092	-0.072
	2.009	-0.036	-0.068	-0.107	-0.119	-0.167	-0.158	-0.127	-0.137	-0.129	-0.093	-0.078
	2.134	-0.037	-0.073	-0.079	-0.086	-0.124	-0.158	-0.134	-0.107	-0.092	-0.065	-0.055
	2.259	-0.040	-0.071	-0.094	-0.104	-0.129	-0.129	-0.079	-0.147	-0.131	-0.101	-0.077
25°	1.134	-0.026	-0.026	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009
	1.259	-0.090	-0.041	-0.022	-0.004							

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(b) A = 2 triangular wing, r/s = 0.2 - Concluded

a_s	x/r	δ_w									
		-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°
0°	1.134										
	1.259	.003	.010	.002	.000	.002	.000	.001	.000	.000	.000
	1.384	.004	.007	.011	.004	.002	.003	.003	.003	.003	.001
	1.509	.009	.004	.001	.008	.009	.003	.003	.003	.003	.007
	1.634	.009	.004	.025	.038	.039	.044	.045	.021	.026	.045
	1.756	.010	.005	.027	.055	.063	.058	.043	.026	.044	.066
	1.884	.012	.006	.033	.050	.074	.090	.101	.090	.077	.055
	2.009	.013	.003	.016	.048	.068	.080	.096	.076	.068	.043
	2.134	.009	.009	.027	.038	.047	.049	.043	.028	.039	.030
	2.259	.008	.013	.034	.041	.034	.049	.029	.010	.033	.030
3°	1.134	.003	.001	.001	.000	.001	.000	.001	.000	.000	.000
	1.259	.006	.007	.008	.002	.003	.003	.002	.003	.003	.001
	1.384	.023	.012	.014	.038	.001	.005	.002	.003	.002	.004
	1.509	.036	.032	.030	.016	.006	.148	.149	.174	.116	.089
	1.634	.033	.018	.003	.002	.000	.001	.005	.046	.144	.184
	1.756	.036	.021	.004	.020	.038	.055	.039	.022	.011	.026
	1.884	.047	.023	.003	.021	.035	.063	.078	.075	.070	.072
	2.009	.048	.028	.009	.010	.023	.035	.046	.065	.072	.077
	2.134	.038	.014	.002	.004	.007	.015	.008	.010	.031	.052
	2.259	.023	.005	.007	.015	.012	.007	.008	.008	.008	.006
6°	1.134	.003	.004	.001	.001	.000	.001	.001	.002	.001	.001
	1.259	.006	.007	.008	.002	.003	.003	.002	.003	.003	.004
	1.384	.023	.012	.014	.038	.001	.005	.002	.003	.002	.004
	1.509	.036	.032	.030	.016	.006	.148	.149	.174	.116	.089
	1.634	.033	.018	.003	.002	.000	.001	.005	.046	.144	.184
	1.756	.036	.021	.004	.020	.038	.055	.039	.022	.011	.026
	1.884	.047	.023	.003	.021	.035	.063	.078	.075	.070	.072
	2.009	.048	.028	.009	.010	.023	.035	.046	.065	.072	.077
	2.134	.038	.014	.002	.004	.007	.015	.008	.010	.031	.052
	2.259	.023	.005	.007	.015	.012	.007	.008	.008	.008	.006
10°	1.134	.001	.003	.004	.002	.004	.002	.002	.003	.001	.001
	1.259	.000	.009	.007	.006	.006	.006	.005	.007	.006	.006
	1.384	.033	.029	.023	.036	.004	.030	.035	.009	.006	.006
	1.509	.046	.050	.042	.026	.004	.130	.135	.152	.188	.195
	1.634	.056	.042	.030	.025	.011	.011	.054	.044	.028	.017
	1.756	.054	.036	.008	.020	.043	.059	.054	.082	.079	.084
	1.884	.071	.016	.019	.008	.005	.053	.062	.080	.093	.095
	2.009	.067	.041	.015	.007	.012	.016	.040	.080	.083	.085
	2.134	.052	.027	.011	.002	.001	.005	.004	.003	.004	.011
	2.259	.035	.014	.005	.006	.001	.002	.005	.008	.012	.025
15°	1.134	.001	.011	.017	.002	.004	.002	.002	.003	.001	.001
	1.259	.003	.020	.008	.005	.005	.006	.005	.007	.006	.006
	1.384	.043	.050	.038	.033	.007	.007	.007	.007	.006	.006
	1.509	.052	.062	.068	.048	.047	.094	.038	.113	.013	.013
	1.637	.061	.040	.043	.040	.028	.093	.084	.144	.160	.177
	1.756	.068	.043	.027	.007	.027	.051	.088	.161	.139	.087
	1.884	.099	.069	.036	.005	.016	.016	.088	.111	.107	.107
	2.009	.091	.066	.042	.012	.012	.004	.068	.108	.108	.107
	2.134	.079	.048	.025	.006	.004	.004	.003	.006	.028	.054
	2.259	.069	.042	.015	.006	.008	.008	.009	.015	.010	.022
20°	1.134	.001	.013	.020	.008	.020	.013	.013	.013	.004	.037
	1.259	.002	.032	.008	.002	.002	.004	.003	.003	.004	.005
	1.384	.067	.079	.060	.026	.026	.004	.005	.005	.004	.011
	1.509	.076	.067	.101	.079	.066	.088	.297	.137	.004	.018
	1.634	.085	.068	.069	.077	.067	.139	.016	.043	.105	.195
	1.756	.081	.059	.024	.004	.032	.068	.093	.105	.086	.047
	1.884	.151	.059	.057	.022	.008	.021	.067	.111	.135	.135
	2.009	.132	.069	.069	.030	.010	.024	.017	.042	.073	.016
	2.134	.119	.081	.046	.028	.007	.016	.009	.018	.031	.055
	2.259	.101	.070	.036	.011	.006	.018	.016	.034	.033	.017
25°	1.134	.005	.002	.008	.002	.004	.002	.003	.003	.002	.008
	1.259	.004	.007	.007	.007	.007	.007	.007	.007	.008	.005
	1.384	.088	.112	.057	.019	.004	.004	.002	.004	.004	.009
	1.509	.103	.110	.146	.114	.098	.093	.132	.162	.005	.009
	1.634	.120	.100	.093	.121	.088	.104	.080	.093	.134	
	1.756	.109	.086	.061	.015	.031	.065	.088	.105	.098	.039
	1.884	.174	.138	.089	.048	.017	.008	.039	.037	.100	.157
	2.009	.181	.127	.086	.034	.020	.001	.019	.026	.140	.060
	2.134	.165	.115	.063	.021	.006	.011	.023	.024	.119	.057
	2.259	.132	.093	.045	.020	.008	.007	.016	.014	.104	.028
	2.384	.167	.114	.065	.026	.016	.004	.004	.004	.003	.014
	2.509	.157	.104	.060	.036	.022	.008	.005	.006	.005	.004

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(c) A = 1 triangular wing, r/s = 0.2

a_B	x/r	δ_w											
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	
0°	6.94	0.00	0.01	0.01	0.01	0.00	0.00	0.01	0.01	0.01	0.01	0.01	
	8.37	0.001	0.003	0.003	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	
	9.81	0.000	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	
	11.25	-	0.009	-	0.012	-	0.013	-	0.014	-	0.014	-	
	12.69	-	0.002	-	0.016	-	0.019	-	0.022	-	0.022	-	
	14.12	-	0.038	-	0.061	-	0.083	-	0.103	-	0.123	-	
	15.56	-	0.056	-	0.072	-	0.088	-	0.105	-	0.124	-	
	16.44	-	0.078	-	0.118	-	0.156	-	0.195	-	0.236	-	
	17.87	-	0.050	-	0.073	-	0.095	-	0.101	-	0.125	-	
	21.31	-	0.028	-	0.047	-	0.065	-	0.076	-	0.098	-	
	22.75	-	0.005	-	0.014	-	0.028	-	0.031	-	0.044	-	
	24.19	-	0.014	-	0.014	-	0.026	-	0.031	-	0.044	-	
	25.62	-	0.020	-	0.020	-	0.031	-	0.031	-	0.048	-	
3°	6.94	0.01	0.01	0.01	0.01	0.02	0.02	0.02	0.03	0.03	0.03	0.03	
	8.37	0.002	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	
	9.81	0.004	0.003	0.003	0.003	0.004	0.003	0.003	0.003	0.003	0.003	0.003	
	11.25	-	0.000	-	0.001	-	0.000	-	0.000	-	0.000	-	
	12.69	-	0.030	-	0.050	-	0.075	-	0.099	-	0.117	-	
	14.12	-	0.036	-	0.076	-	0.105	-	0.137	-	0.166	-	
	15.56	-	0.052	-	0.086	-	0.118	-	0.147	-	0.178	-	
	16.44	-	0.076	-	0.118	-	0.150	-	0.180	-	0.210	-	
	17.00	-	0.058	-	0.086	-	0.118	-	0.144	-	0.172	-	
	18.44	-	0.036	-	0.056	-	0.084	-	0.105	-	0.126	-	
	19.87	-	0.005	-	0.007	-	0.013	-	0.017	-	0.021	-	
	22.75	-	0.015	-	0.015	-	0.026	-	0.031	-	0.038	-	
	24.19	-	0.024	-	0.034	-	0.036	-	0.033	-	0.040	-	
	25.62	-	0.049	-	0.049	-	0.053	-	0.051	-	0.058	-	
6°	6.94	0.00	0.01	0.01	0.01	0.00	0.00	0.01	0.00	0.00	0.00	0.01	
	8.37	0.003	0.003	0.003	0.003	0.001	0.001	0.001	0.001	0.001	0.001	0.001	
	9.81	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	
	11.25	-	0.078	-	0.090	-	0.098	-	0.104	-	0.115	-	
	12.69	-	0.081	-	0.093	-	0.108	-	0.124	-	0.136	-	
	14.12	-	0.093	-	0.169	-	0.208	-	0.256	-	0.294	-	
	15.56	-	0.086	-	0.196	-	0.237	-	0.287	-	0.325	-	
	16.44	-	0.066	-	0.147	-	0.190	-	0.230	-	0.261	-	
	17.00	-	0.056	-	0.138	-	0.180	-	0.217	-	0.248	-	
	18.44	-	0.036	-	0.119	-	0.157	-	0.190	-	0.221	-	
	19.87	-	0.008	-	0.098	-	0.120	-	0.145	-	0.176	-	
	22.75	-	0.017	-	0.040	-	0.056	-	0.071	-	0.092	-	
	24.19	-	0.045	-	0.114	-	0.164	-	0.201	-	0.241	-	
	25.62	-	0.049	-	0.114	-	0.164	-	0.201	-	0.241	-	
10°	6.94	0.049	0.02	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
	8.37	0.063	0.052	0.052	0.052	0.051	0.051	0.051	0.051	0.051	0.051	0.051	
	9.81	0.080	0.065	0.065	0.065	0.066	0.066	0.066	0.066	0.066	0.066	0.066	
	11.25	-	0.040	-	0.040	-	0.041	-	0.041	-	0.041	-	
	12.69	-	0.046	-	0.053	-	0.061	-	0.068	-	0.075	-	
	14.12	-	0.055	-	0.050	-	0.057	-	0.065	-	0.075	-	
	15.56	-	0.055	-	0.105	-	0.147	-	0.183	-	0.211	-	
	16.44	-	0.055	-	0.147	-	0.189	-	0.217	-	0.245	-	
	17.00	-	0.055	-	0.147	-	0.189	-	0.217	-	0.245	-	
	18.44	-	0.055	-	0.147	-	0.189	-	0.217	-	0.245	-	
	19.87	-	0.055	-	0.147	-	0.189	-	0.217	-	0.245	-	
	22.75	-	0.055	-	0.147	-	0.189	-	0.217	-	0.245	-	
	24.19	-	0.055	-	0.147	-	0.189	-	0.217	-	0.245	-	
	25.62	-	0.055	-	0.147	-	0.189	-	0.217	-	0.245	-	
15°	6.94	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
	8.37	0.002	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	
	9.81	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	0.003	
	11.25	-	0.030	-	0.030	-	0.030	-	0.030	-	0.030	-	
	12.69	-	0.033	-	0.033	-	0.033	-	0.033	-	0.033	-	
	14.12	-	0.037	-	0.037	-	0.037	-	0.037	-	0.037	-	
	15.56	-	0.047	-	0.050	-	0.050	-	0.050	-	0.050	-	
	16.44	-	0.050	-	0.053	-	0.053	-	0.053	-	0.053	-	
	17.00	-	0.050	-	0.053	-	0.053	-	0.053	-	0.053	-	
	18.44	-	0.050	-	0.053	-	0.053	-	0.053	-	0.053	-	
	19.87	-	0.050	-	0.053	-	0.053	-	0.053	-	0.053	-	
	22.75	-	0.050	-	0.053	-	0.053	-	0.053	-	0.053	-	
	24.19	-	0.050	-	0.053	-	0.053	-	0.053	-	0.053	-	
	25.62	-	0.050	-	0.053	-	0.053	-	0.053	-	0.053	-	
20°	6.94	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
	8.37	0.004	0.047	0.047	0.047	0.047	0.047	0.047	0.047	0.047	0.047	0.047	
	9.81	0.009	0.093	0.093	0.093	0.093	0.093	0.093	0.093	0.093	0.093	0.093	
	11.25	-	0.034	-	0.034	-	0.034	-	0.034	-	0.034	-	
	12.69	-	0.034	-	0.034	-	0.034	-	0.034	-	0.034	-	
	14.12	-	0.037	-	0.037	-	0.037	-	0.037	-	0.037	-	
	15.56	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	16.44	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	17.00	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	18.44	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	19.87	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	22.75	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	24.19	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	25.62	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
25°	6.94	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
	8.37	0.004	0.047	0.047	0.047	0.047	0.047	0.047	0.047	0.047	0.047	0.047	
	9.81	0.009	0.093	0.093	0.093	0.093	0.093	0.093	0.093	0.093	0.093	0.093	
	11.25	-	0.034	-	0.034	-	0.034	-	0.034	-	0.034	-	
	12.69	-	0.034	-	0.034	-	0.034	-	0.034	-	0.034	-	
	14.12	-	0.037	-	0.037	-	0.037	-	0.037	-	0.037	-	
	15.56	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	16.44	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	17.00	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	18.44	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	19.87	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	22.75	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	24.19	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	
	25.62	-	0.040	-	0.040	-	0.040	-	0.040	-	0.040	-	

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(d) $A = 1$ triangular wing, $r/s = 0.4$

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(d) $A = 1$ triangular wing, $r/s = 0.4$ - Concluded

a_B	x/r		δ_w									
			-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°
0°	654	.002	.009	.000	.001	.000	b01	b01	.002	.001	.001	.001
	837	-.003	-.001	-.001	-.000	-.000	b00	b00	-.001	-.001	-.000	-.000
	981	-.000	-.001	-.000	-.000	-.000	b00	b00	-.001	-.000	-.000	-.000
	1125	-.002	-.001	-.001	-.000	-.000	b00	b00	-.001	-.000	-.000	-.000
	1269	-.000	-.001	-.001	-.000	-.000	b00	b00	-.000	-.000	-.000	-.001
	1412	-.001	-.001	-.001	-.000	-.000	b00	b00	-.000	-.000	-.000	-.000
	1556	-.002	-.019	-.027	-.044	-.074	b01	b00	-.017	-.027	-.052	-.060
	1700	-.016	-.027	-.044	-.074	-.066	b01	b00	-.027	-.052	-.063	-.060
	1844	-.015	-.032	-.050	-.074	-.054	b01	b00	-.027	-.052	-.063	-.060
	1987	-.018	-.026	-.041	-.045	-.048	b01	b00	-.027	-.051	-.049	-.046
3°	8131	-.016	-.028	-.041	-.045	-.048	b01	b00	-.027	-.051	-.049	-.046
	2175	-.008	-.016	-.028	-.035	-.030	b01	b00	-.027	-.051	-.049	-.046
	2439	.001	-.005	-.004	-.004	-.002	b01	b00	-.027	-.051	-.049	-.046
	2552	.003	-.003	-.006	-.014	-.017	b01	b00	-.027	-.051	-.049	-.046
	654	.000	.001	.001	.000	b00	b00	.001	.000	.000	.000	.001
	837	.000	-.001	-.002	-.001	-.001	b00	b00	-.001	-.001	-.000	-.000
	981	-.001	-.001	-.002	-.001	-.001	b00	b00	-.001	-.001	-.000	-.000
	1125	-.001	-.001	-.002	-.001	-.001	b00	b00	-.001	-.001	-.000	-.000
	1269	-.005	-.005	-.006	-.005	-.005	b00	b00	-.005	-.004	-.004	-.001
	1412	-.001	-.001	-.001	-.001	-.001	b00	b00	-.001	-.001	-.000	-.000
6°	1556	.000	-.009	-.024	-.042	-.054	b01	b00	-.017	-.066	-.043	-.050
	1700	-.003	-.013	-.028	-.042	-.048	b01	b00	-.017	-.066	-.043	-.050
	1844	-.003	-.017	-.027	-.030	-.030	b01	b00	-.017	-.066	-.043	-.050
	1987	-.005	-.017	-.020	-.025	-.028	b01	b00	-.017	-.065	-.042	-.049
	2175	-.007	-.017	-.020	-.025	-.028	b01	b00	-.017	-.065	-.042	-.049
	2439	-.007	-.017	-.020	-.025	-.028	b01	b00	-.017	-.065	-.042	-.049
	2552	.005	-.017	-.020	-.025	-.028	b01	b00	-.017	-.065	-.042	-.049
	654	.000	.000	.001	.000	.001	b00	b00	.000	.000	.000	.000
	837	-.001	-.008	-.008	-.002	-.001	b00	b00	-.001	-.001	-.000	-.000
	981	-.001	-.002	-.002	-.001	-.001	b00	b00	-.001	-.001	-.000	-.000
10°	1125	-.002	-.002	-.001	-.001	-.001	b00	b00	-.006	-.006	-.006	-.006
	1269	-.006	-.005	-.006	-.004	-.004	b00	b00	-.006	-.006	-.006	-.006
	1412	-.001	-.004	-.006	-.007	-.007	b00	b00	-.006	-.006	-.006	-.006
	1556	-.017	-.015	-.015	-.017	-.017	b01	b00	-.040	-.034	-.034	-.034
	1700	-.024	-.016	-.017	-.021	-.021	b01	b00	-.040	-.034	-.034	-.034
	1844	-.030	-.017	-.017	-.020	-.021	b01	b00	-.040	-.034	-.034	-.034
	1987	-.037	-.012	-.008	-.008	-.008	b01	b00	-.040	-.034	-.034	-.034
	2175	-.045	-.012	-.008	-.008	-.008	b01	b00	-.040	-.034	-.034	-.034
	2439	-.053	-.012	-.008	-.008	-.008	b01	b00	-.040	-.034	-.034	-.034
	2552	-.061	-.012	-.008	-.008	-.008	b01	b00	-.040	-.034	-.034	-.034
15°	654	.000	.000	.000	.000	.000	b00	b00	.000	.000	.000	.000
	837	.000	.000	.001	.000	.001	b00	b00	.001	.001	.001	.001
	981	-.001	-.001	-.001	-.001	-.001	b00	b00	-.001	-.001	-.001	-.001
	1125	-.000	-.001	-.001	-.001	-.001	b00	b00	-.001	-.001	-.001	-.001
	1269	-.000	-.001	-.001	-.001	-.001	b00	b00	-.001	-.001	-.001	-.001
	1412	-.003	-.007	-.007	-.007	-.007	b00	b00	-.026	-.026	-.026	-.026
	1556	-.023	-.025	-.015	-.014	-.014	b01	b00	-.146	-.147	-.147	-.147
	1700	-.037	-.029	-.011	-.006	-.006	b01	b00	-.147	-.147	-.147	-.147
	1844	-.046	-.029	-.010	-.006	-.006	b01	b00	-.147	-.147	-.147	-.147
	1987	-.046	-.029	-.009	-.006	-.006	b01	b00	-.147	-.147	-.147	-.147
20°	2175	-.050	-.030	-.008	-.006	-.006	b01	b00	-.147	-.147	-.147	-.147
	2439	-.059	-.030	-.008	-.006	-.006	b01	b00	-.147	-.147	-.147	-.147
	2552	-.069	-.030	-.008	-.006	-.006	b01	b00	-.147	-.147	-.147	-.147
	654	-.001	.002	.005	.006	.002	b00	b00	.002	.004	.004	.004
	837	-.006	.001	.001	.001	.001	b00	b00	-.001	-.004	-.004	-.004
	981	-.004	.001	.001	.001	.001	b00	b00	-.001	-.004	-.004	-.004
	1125	-.007	.001	.001	.001	.001	b00	b00	-.001	-.004	-.004	-.004
	1269	-.003	.023	.014	.015	.015	b00	b00	-.001	-.004	-.004	-.004
	1412	-.041	.048	.033	.034	.034	b00	b00	-.001	-.004	-.004	-.004
	1556	-.041	.048	.033	.034	.034	b00	b00	-.001	-.004	-.004	-.004
25°	1700	-.046	.046	.028	.028	.028	b00	b00	-.001	-.004	-.004	-.004
	1844	-.047	.046	.028	.028	.028	b00	b00	-.001	-.004	-.004	-.004
	1987	-.057	.049	.037	.034	.034	b00	b00	-.001	-.004	-.004	-.004
	2175	-.063	.053	.037	.034	.034	b00	b00	-.001	-.004	-.004	-.004
	2439	-.064	.053	.037	.034	.034	b00	b00	-.001	-.004	-.004	-.004
	2552	-.064	.053	.037	.034	.034	b00	b00	-.001	-.004	-.004	-.004
	654	.001	.003	.003	.005	.005	b00	b00	.006	.001	.002	.002
	837	.004	.006	.005	.005	.005	b00	b00	-.005	.005	.005	.005
	981	-.001	.001	.001	.001	.001	b00	b00	-.005	.005	.005	.005
	1125	-.004	.002	.002	.002	.002	b00	b00	-.005	.005	.005	.005

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE
WINGS - Continued

(e) $A = 2/3$ triangular wing, $r/s = 0.4$

x/r	$\delta_w, \alpha_B = 0^\circ$												$\alpha_B, \delta_w = 0^\circ$						
	45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°		
6.94	.005	.006	.004	.003	.004	.003	.004	.003	.003	.000	.003	.004	.000	.007	.006	.003	.006	.006	
8.37	- .001	- .000	- .001	- .001	- .000	- .001	- .001	- .001	- .002	- .000	- .006	- .005	- .005	- .002	- .003	- .003	- .003	- .003	
9.81	- .007	- .003	- .004	- .005	- .005	- .001	- .005	- .004	- .003	- .001	- .003	- .001	- .001	- .002	- .000	- .000	- .000	- .005	
11.25	- .004	- .002	- .003	- .003	- .002	- .001	- .003	- .002	- .001	- .003	- .000	- .006	- .004	- .000	- .000	- .002	- .004	- .004	
12.69	.001	.002	.002	.001	.001	.001	.000	.016	.000	.004	.000	.011	.007	.006	.004	.005	.009	.006	
14.12	.000	.000	.000	.000	.000	.058	.056	.017	.007	.002	.000	.011	.024	.038	.039	.044	.056	.056	
15.56	.017	- .083	- .251	- .348	- .180	.030	.051	.032	.016	.007	.000	.016	.032	.047	.053	.068	.079	.080	
17.00	.020	.017	.010	.029	.039	.084	.073	.047	.024	.009	.000	.019	.039	.057	.065	.080	.102	.102	
18.44	.076	.067	.074	.086	.090	.060	.060	.045	.004	.006	.005	.019	.042	.063	.073	.093	.123	.123	
19.87	.068	.070	.068	.068	.061	.057	.031	.031	.025	.008	.005	.021	.047	.061	.086	.107	.133	.133	
21.31	.039	.047	.029	.086	.086	.086	.087	.031	.020	.017	.003	.015	.036	.054	.069	.096	.117	.117	
22.75	.028	.053	.017	.011	.013	.018	.020	.017	.014	.001	.003	.008	.017	.036	.054	.087	.109	.109	
24.19	.000	.000	- .008	- .005	- .007	- .006	.016	.008	.007	.002	.000	.001	.003	.019	.080	.060	- .087	- .087	
25.62	- .030	- .083	- .011	.010	.020	.023	.005	.002	.006	.006	.009	.009	.003	.043	.050	.050	.090	.090	

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN THE PRESENCE OF THE
WINGS - Continued

(f) $A = 3/8$ triangular wing, $r/s = 0.4$

x/r	$\delta_w, \alpha_B = 0^\circ$												$\alpha_B, \delta_w = 0^\circ$						
	45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	3°	6°	10°	15°	20°	25°		
6.94	.004	.002	- .015	.001	.001	.000	.001	.001	.000	- .002	- .002	.000	.000	.000	.000	.000	.000	.003	
8.37	.001	- .002	- .016	.001	.001	.012	.000	- .001	- .008	- .002	- .002	.005	.001	.001	.003	.001	.000	.000	
9.81	- .001	- .001	- .020	- .004	- .003	- .005	- .003	- .011	- .018	- .001	- .002	.005	.019	.031	.046	.060	.065	.074	
11.25	.000	- .001	- .018	- .001	- .001	- .001	- .001	- .002	- .000	- .003	- .003	.009	.017	.037	.046	.060	.065	.074	
12.69	.003	.000	- .015	- .044	.000	.037	- .086	.009	.013	.004	- .001	.001	.032	.049	.064	.077	.090	.090	
14.12	- .092	- .095	- .132	- .206	- .289	- .557	.013	.044	.014	.005	- .003	.015	.031	.053	.075	.086	.104	.104	
15.56	- .354	- .364	- .509	- .904	- .001	.045	.074	.056	.020	.008	- .005	.014	.035	.059	.080	.108	.126	.126	
17.00	- .046	- .955	- .149	.063	.063	.079	.083	.057	.020	.007	- .006	.017	.038	.061	.080	.109	.140	.140	
18.44	.060	.060	.028	.024	.024	.078	.084	.059	.048	.021	.006	.015	.038	.064	.088	.124	.157	.157	
19.87	.080	.080	.024	.006	.006	.071	.034	.058	.026	.004	- .006	.016	.039	.068	.096	.127	.159	.159	
21.31	.080	.080	.028	.016	.014	.010	.007	.005	.003	.001	.001	.015	.040	.078	.095	.128	.156	.156	
22.75	.000	- .001	- .038	- .086	- .035	- .030	- .088	- .007	.004	- .003	- .005	.001	.010	.039	.051	.109	.168	.168	
24.19	- .014	- .004	- .038	- .086	- .035	- .030	- .088	- .007	.004	- .003	- .005	.001	.005	.035	.067	.084	.131	.131	
25.62	- .021	- .020	- .048	- .071	- .036	- .023	- .011	.001	.007	.005	- .005	.001	- .005	.035	.067	.084	.131	.131	

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TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(g) A = 3 rectangular wing, r/s = 0.2

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(g) $A = 3$ rectangular wing, $r/s = 0.2$ - Concluded

a_B	x/r		δ_w									
			-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°
0°	6.94	.001	.002	.000	.001	.002	.002	.003	.002	.001	.001	.001
	8.37	.000	.000	.000	.000	.000	.000	.000	.001	.001	.000	.000
	9.81	.000	.001	.001	.000	.000	.000	.000	.001	.001	.000	.000
	1.125	.000	.001	.001	.000	.001	.000	.000	.000	.000	.000	.000
	1.259	.000	.001	.000	.001	.000	.000	.000	.001	.001	.001	.001
	1.412	.000	.002	.002	.000	.001	.000	.000	.002	.001	.001	.001
	1.556	.000	.003	.002	.001	.000	.000	.000	.003	.001	.001	.001
	1.700	.000	.002	.001	.001	.000	.000	.000	.002	.001	.001	.001
	1.844	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
	1.987	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
	2.131	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
3°	2.275	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
	2.419	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
	2.552	.000	.003	.002	.001	.000	.000	.000	.003	.001	.001	.001
	6.94	.002	.003	.002	.001	.000	.000	.000	.002	.001	.001	.001
	8.37	.000	.001	.000	.000	.000	.000	.000	.002	.001	.001	.001
	9.81	.000	.001	.000	.000	.000	.000	.000	.001	.001	.000	.000
	1.125	.000	.001	.000	.000	.000	.000	.000	.001	.001	.000	.001
	1.259	.000	.001	.000	.000	.000	.000	.000	.001	.001	.000	.001
	1.412	.000	.001	.000	.000	.000	.000	.000	.001	.001	.000	.001
	1.556	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
	1.700	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	1.844	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	1.987	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	2.131	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
6°	2.275	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	2.419	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	2.552	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
	6.94	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.001
	8.37	.001	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	9.81	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.125	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.259	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.412	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.556	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.700	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.844	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
10°	1.987	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	2.131	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	2.275	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	2.419	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	2.552	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
	6.94	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.001
	8.37	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	9.81	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.125	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.259	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.412	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
15°	1.556	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
	1.700	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	1.844	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	1.987	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	2.131	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	2.275	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	2.419	.000	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	2.552	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
	6.94	.001	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	8.37	.001	.001	.000	.000	.000	.000	.000	.001	.001	.001	.001
	9.81	.002	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
20°	1.125	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.259	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.412	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.556	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.700	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.844	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	1.987	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	2.131	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	2.275	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	2.419	.000	.001	.000	.000	.000	.000	.000	.000	.000	.000	.000
	2.552	.000	.002	.001	.000	.000	.000	.000	.002	.001	.001	.001
25°	6.94	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003
	8.37	.007	.007	.007	.007	.007	.007	.007	.007	.007	.007	.007
	9.81	.005	.005	.005	.005	.005	.005	.005	.005	.005	.005	.005
	1.125	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
	1.259	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
	1.412	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003
	1.556	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003
	1.700	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003	.003
	1.844	.007	.006	.005	.004	.003	.002	.001	.000	.000	.000	.000
	1.987	.007	.006	.005	.004	.003	.002	.001	.000	.000	.000	.000
	2.131	.007	.006	.005	.004	.003	.002	.001	.000	.000	.000	.000
	2.275	.007	.006	.005	.004	.003	.002	.001	.000	.000	.000	.000
	2.419	.006	.005	.004	.003	.002	.001	.000	.000	.000	.000	.000
	2.552	.008	.008	.004	.003	.002	.001	.000	.000	.000	.000	.000

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(h) A = 2 rectangular wing, r/s = 0.2

α_B	x/r	δ_w											
		45°	40°	35°	30°	25°	20°	15°	10°	6°	3°	0°	
0°	1.134	.010	-.016	-.013	-.003	.001	.005	.001	.006	.002	.001	.001	
	1.259	.053	.036	.009	.009	.006	.005	.004	.004	.007	.003	.003	
	1.384	.000	.004	.000	.001	.000	.000	-	.004	-	.004	.000	
	1.509	.012	.021	-.008	-.006	.009	-.007	-	.004	-	.004	.009	
	1.634	.055	.060	.014	.006	.011	.009	-	.009	-	.008	.018	
	1.756	-.008	.000	.000	.007	.010	.019	-.007	-	.015	-	.006	
	1.884	-.031	.036	.025	.010	.019	.019	-.007	-	.000	.001	.001	
	2.009	.020	.058	.003	.001	.008	.000	.000	.000	.007	.004	.000	
	2.134	.006	-.014	-.037	-.063	.040	.000	.000	.007	.009	.006	.016	
	2.259	.007	.001	-.008	-.031	.023	.028	.000	.009	.005	.006	.014	
3°	2.384	.035	.050	.001	-.002	.008	.001	.005	.005	.006	.006	.014	
	2.509	-.044	.029	-.058	.005	.026	.014	-	.003	-.001	.001	.011	
	1.134	-.001	-.001	-.003	-.003	.001	-.008	-.008	-.001	-.001	-.001	-.001	
	1.259	.000	-.001	-.001	-.002	.000	-.001	-.001	-.001	-.001	-.001	-.001	
	1.384	-.024	.004	.001	.001	.002	.000	-.001	-.001	-.001	-.001	-.002	
	1.509	.105	.055	.006	.015	.005	.005	-.004	-.002	-.001	-.001	-.002	
	1.634	.232	.147	.125	.102	.047	.046	.032	.025	.018	.018	.036	
	1.756	.264	.234	.218	.178	.121	.110	.083	.058	.041	.041	.045	
	1.884	.196	.225	.226	.148	.127	.113	.088	.068	.051	.051	.053	
	2.009	.089	.112	.135	.150	.145	.133	.098	.073	.063	.063	.065	
6°	2.134	.103	.098	.097	.097	.092	.113	.094	.071	.051	.051	.053	
	2.259	.075	.046	.056	.082	.084	.073	.057	.042	.042	.042	.043	
	2.384	.029	.018	.021	.045	.053	.051	.039	.027	.027	.027	.029	
	2.509	.017	.008	.005	.027	.037	.037	.029	.021	.021	.021	.021	
	1.134	-.002	-.004	-.001	-.002	.001	-.001	-.031	-.002	-.002	-.002	-.003	
	1.259	-.001	-.002	-.001	-.001	.000	-.001	-.004	-.004	-.004	-.004	-.004	
	1.384	.086	.004	-.001	-.005	.004	-.004	-.004	-.004	-.004	-.004	-.004	
	1.509	.060	.021	-.001	-.005	.005	-.005	-.004	-.004	-.004	-.004	-.004	
	1.634	.238	.161	.109	.074	.061	.040	.039	.039	.039	.039	.056	
	1.756	.310	.265	.190	.174	.143	.116	.085	.085	.085	.085	.068	
10°	1.884	.991	.270	.195	.177	.151	.122	.087	.087	.087	.087	.067	
	2.009	.151	.195	.199	.163	.117	.091	.087	.087	.087	.087	.062	
	2.134	.106	.138	.161	.141	.118	.091	.073	.073	.073	.073	.046	
	2.259	.055	.088	.113	.114	.097	.076	.061	.061	.061	.061	.046	
	2.384	.018	.046	.059	.067	.061	.049	.040	.040	.040	.040	.029	
	2.509	.008	.004	.013	.088	.037	.031	.023	.023	.023	.023	.014	
	1.134	-.000	-.001	-.005	-.003	.003	-.005	-.005	-.005	-.005	-.005	-.003	
	1.259	-.001	-.001	-.001	-.001	.000	-.001	-.002	-.002	-.002	-.002	-.001	
	1.384	-.007	-.025	-.015	-.003	.003	-.003	-.003	-.003	-.003	-.003	-.004	
	1.509	-.188	.107	.059	.059	.059	.059	.053	.053	.053	.053	.048	
15°	1.634	.301	.213	.161	.161	.161	.154	.126	.126	.126	.126	.123	
	1.756	.109	.217	.200	.196	.148	.118	.115	.115	.115	.115	.100	
	1.884	.228	.196	.163	.163	.109	.096	.083	.083	.083	.083	.069	
	2.009	.085	.144	.114	.114	.065	.057	.054	.054	.054	.054	.047	
	2.134	.037	.056	.065	.050	.050	.051	.047	.047	.047	.047	.045	
	2.259	.034	.042	.042	.034	.034	.034	.031	.031	.031	.031	.031	
	2.384	.003	.009	.010	.013	.014	.010	.008	.008	.008	.008	.008	
	2.509	.005	.006	.006	.005	.005	.005	.004	.004	.004	.004	.003	
	1.134	.004	.032	.015	.007	.001	.001	.001	.001	.001	.001	.001	
	1.259	.001	.006	.002	.001	.001	.001	.001	.001	.001	.001	.001	
20°	1.384	.048	.006	.003	.002	.001	.001	.001	.001	.001	.001	.000	
	1.509	.011	.032	.015	.007	.001	.001	.001	.001	.001	.001	.003	
	1.634	.283	.173	.074	.064	.064	.064	.051	.051	.051	.051	.048	
	1.756	.409	.387	.283	.168	.168	.168	.125	.125	.125	.125	.123	
	1.884	.350	.367	.294	.168	.168	.168	.135	.135	.135	.135	.130	
	2.009	.234	.259	.242	.173	.173	.173	.155	.155	.155	.155	.156	
	2.134	.066	.165	.193	.181	.181	.181	.147	.147	.147	.147	.147	
	2.259	.097	.134	.134	.146	.146	.146	.134	.134	.134	.134	.136	
	2.384	.028	.040	.064	.084	.084	.084	.076	.076	.076	.076	.076	
	2.509	.047	.047	.069	.096	.096	.096	.087	.087	.087	.087	.086	
25°	1.134	-.017	.020	.021	.015	.015	.015	.017	.017	.017	.017	.017	
	1.259	.016	.018	.011	.006	.006	.006	.006	.006	.006	.006	.006	
	1.384	.015	.018	.011	.006	.006	.006	.004	.004	.004	.004	.004	
	1.509	.025	.018	.011	.006	.006	.006	.004	.004	.004	.004	.004	
	1.634	.407	.318	.146	.146	.146	.146	.118	.118	.118	.118	.117	
	1.756	.386	.316	.156	.156	.156	.156	.126	.126	.126	.126	.126	
	1.884	.381	.363	.161	.161	.161	.161	.138	.138	.138	.138	.138	
	2.009	.248	.261	.181	.181	.181	.181	.158	.158	.158	.158	.158	
28°	2.134	.115	.143	.143	.143	.143	.143	.115	.115	.115	.115	.115	
	2.259	.144	.167	.167	.167	.167	.167	.139	.139	.139	.139	.139	
	2.384	-.004	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
	2.509	.272	.303	.286	.286	.286	.286	.228	.228	.228	.228	.228	
	1.134	.264	.272	.286	.286	.286	.286	.229	.229	.229	.229	.229	

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(h) $A = 2$ rectangular wing, $r/s = 0.2$ - Concluded

a_B	x/r	δ_W									
		-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°
0°	1.134										
	1.259										
	1.384										
	1.509										
	1.634										
	1.756										
	1.884										
	2.009										
	2.134										
	2.259										
	2.384										
	2.509										
3°	1.134	-0.023	-0.002	-0.001	-0.001	-0.001	-0.000	-0.001	-0.001	-0.001	-0.001
	1.259	-0.001	-0.001	-0.001	-0.000	-0.001	-0.002	-0.001	-0.001	-0.001	-0.001
	1.384	-0.000	-0.001	-0.001	-0.000	-0.001	-0.002	-0.001	-0.001	-0.001	-0.001
	1.509	-0.001	-0.001	-0.001	-0.000	-0.001	-0.002	-0.001	-0.001	-0.001	-0.001
	1.634	-0.007	-0.001	-0.010	-0.000	-0.001	-0.005	-0.001	-0.001	-0.001	-0.001
	1.756	-0.015	-0.002	-0.008	-0.000	-0.005	-0.005	-0.002	-0.001	-0.001	-0.001
	1.884	-0.015	-0.004	-0.008	-0.000	-0.004	-0.006	-0.002	-0.001	-0.001	-0.001
	2.009	-0.017	-0.008	-0.008	-0.000	-0.004	-0.008	-0.002	-0.001	-0.001	-0.001
	2.134	-0.009	-0.012	-0.008	-0.000	-0.004	-0.008	-0.002	-0.001	-0.001	-0.001
	2.259	-0.009	-0.012	-0.008	-0.000	-0.004	-0.008	-0.002	-0.001	-0.001	-0.001
	2.384	-0.002	-0.016	-0.004	-0.000	-0.004	-0.008	-0.002	-0.001	-0.001	-0.001
	2.509	-0.001	-0.011	-0.018	-0.004	-0.019	-0.023	-0.006	-0.007	-0.024	-0.001
6°	1.134	0.001	-0.001	-0.000	-0.000	-0.001	-0.002	-0.003	-0.003	-0.001	-0.001
	1.259	0.000	-0.001	-0.001	-0.000	-0.001	-0.002	-0.001	-0.001	-0.000	-0.000
	1.384	0.005	-0.004	-0.004	-0.000	-0.004	-0.003	-0.005	-0.005	-0.004	-0.004
	1.509	0.003	-0.003	-0.003	-0.000	-0.004	-0.002	-0.004	-0.004	-0.003	-0.003
	1.634	0.025	-0.021	-0.003	-0.003	-0.004	-0.005	-0.007	-0.008	-0.007	-0.007
	1.756	0.038	-0.021	-0.003	-0.003	-0.004	-0.005	-0.007	-0.008	-0.007	-0.007
	1.884	0.046	-0.026	-0.008	-0.002	-0.004	-0.005	-0.007	-0.008	-0.007	-0.007
	2.009	0.040	-0.021	-0.000	-0.002	-0.004	-0.005	-0.007	-0.008	-0.007	-0.007
	2.134	0.040	-0.020	-0.003	-0.008	-0.005	-0.007	-0.007	-0.008	-0.007	-0.007
	2.259	0.026	-0.012	-0.003	-0.007	-0.011	-0.007	-0.003	-0.002	-0.012	-0.009
	2.384	0.012	-0.001	-0.010	-0.009	-0.013	-0.014	-0.009	-0.011	-0.014	-0.011
	2.509	0.007	-0.003	-0.011	-0.014	-0.014	-0.014	-0.009	-0.011	-0.014	-0.011
10°	1.134	0.004	0.005	0.004	-0.010	-0.001	-0.001	-0.012	-0.000	-0.000	-0.000
	1.259	0.003	0.001	0.003	-0.002	-0.001	-0.000	-0.008	-0.004	-0.004	-0.004
	1.384	0.003	0.002	0.003	-0.003	-0.001	-0.000	-0.005	-0.007	-0.007	-0.007
	1.509	0.006	0.004	0.006	-0.003	-0.004	-0.000	-0.035	-0.035	-0.035	-0.035
	1.634	0.045	0.039	0.031	-0.018	-0.010	-0.010	-0.041	-0.056	-0.056	-0.056
	1.756	0.051	0.031	0.021	-0.004	-0.017	-0.017	-0.034	-0.048	-0.048	-0.048
	1.884	0.060	0.046	0.020	-0.007	-0.010	-0.011	-0.024	-0.038	-0.038	-0.038
	2.009	0.071	0.044	0.017	-0.007	-0.004	-0.004	-0.027	-0.037	-0.037	-0.037
	2.134	0.058	0.037	0.015	-0.005	-0.004	-0.001	-0.005	-0.020	-0.020	-0.020
	2.259	0.051	0.033	0.011	-0.007	-0.005	-0.000	-0.006	-0.020	-0.020	-0.020
	2.384	0.038	0.017	0.004	-0.005	-0.002	-0.002	-0.012	-0.014	-0.014	-0.014
	2.509	0.040	0.031	0.010	-0.008	-0.012	-0.010	-0.019	-0.024	-0.024	-0.024
15°	1.134	0.028	0.10	0.08	0.008	0.007	0.009	0.008	0.10	0.000	0.000
	1.259	0.005	0.006	0.004	-0.005	-0.004	-0.005	-0.005	0.008	-0.005	-0.005
	1.384	0.008	0.003	0.001	-0.003	-0.004	-0.005	-0.008	0.008	-0.005	-0.005
	1.509	0.002	0.004	0.002	-0.007	-0.004	-0.005	-0.007	0.008	-0.005	-0.005
	1.634	0.057	0.047	0.047	-0.007	-0.016	-0.016	-0.031	0.037	-0.037	-0.037
	1.756	0.069	0.047	0.047	-0.007	-0.016	-0.016	-0.031	0.047	-0.047	-0.047
	1.884	0.063	0.047	0.047	-0.007	-0.016	-0.016	-0.031	0.047	-0.047	-0.047
	2.009	0.087	0.064	0.064	-0.007	-0.016	-0.016	-0.031	0.064	-0.064	-0.064
	2.134	0.094	0.069	0.069	-0.007	-0.016	-0.016	-0.031	0.069	-0.069	-0.069
	2.259	0.088	0.066	0.066	-0.007	-0.016	-0.016	-0.031	0.066	-0.066	-0.066
	2.384	0.057	0.036	0.033	-0.007	-0.016	-0.016	-0.031	0.036	-0.036	-0.036
	2.509	0.085	0.067	0.033	-0.006	-0.016	-0.016	-0.030	0.033	-0.033	-0.033
20°	1.134	0.24	0.25	0.23	0.17	0.01	0.00	0.30	0.00	0.15	0.15
	1.259	0.17	0.18	0.16	0.14	0.13	0.14	0.15	0.45	0.45	0.45
	1.384	0.12	0.12	0.12	0.09	0.08	0.09	0.09	0.40	0.40	0.40
	1.509	0.05	0.06	0.05	0.05	0.04	0.05	0.06	0.35	0.35	0.35
	1.634	0.61	0.60	0.60	0.21	0.13	0.14	0.15	0.55	0.55	0.55
	1.756	0.69	0.58	0.47	0.23	0.14	0.15	0.16	0.58	0.58	0.58
	1.884	0.89	0.67	0.48	0.23	0.16	0.17	0.18	0.59	0.59	0.59
	2.009	1.27	0.85	0.48	0.20	0.16	0.17	0.18	0.60	0.60	0.60
	2.134	1.41	1.07	0.53	0.20	0.16	0.17	0.18	0.63	0.63	0.63
	2.259	1.45	1.10	0.56	0.24	0.16	0.17	0.18	0.65	0.65	0.65
	2.384	1.21	0.68	0.32	0.01	0.18	0.02	0.03	0.81	0.81	0.81
	2.509	1.65	1.21	1.63	0.33	0.05	0.04	0.03	0.01	0.11	0.11
25°	1.134	0.29	0.31	0.16	0.06	0.02	0.01	0.40	0.03	0.01	0.01
	1.259	0.11	0.15	0.09	0.01	0.09	0.09	0.10	0.09	0.09	0.09
	1.384	0.10	0.13	0.08	0.09	0.01	0.09	0.09	0.09	0.09	0.09
	1.509	0.02	0.01	0.04	0.02	0.01	0.01	0.02	0.01	0.01	0.01
	1.634	0.98	0.95	0.85	0.64	0.56	0.64	1.05	0.55	0.55	0.55
	1.756	1.16	1.03	0.60	0.31	0.11	0.04	0.35	0.58	0.58	0.58
	1.884	1.60	1.05	0.64	0.27	0.02	0.09	0.15	0.30	0.30	0.30
	2.009	1.88	1.27	0.70	0.29	0.14	0.01	0.04	0.05	0.14	0.14
	2.134	2.07	1.55	0.88	0.30	0.13	0.02	0.04	0.01	0.04	0.04
	2.259	2.08	1.61	0.82	0.19	0.03	0.07	0.06	0.02	0.02	0.02
	2.384	2.28	1.76	0.94	0.54	0.34	0.22	0.24	0.16	0.16	0.16
	2.509								0.23	0.23	0.23

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(i) $A = 1$ rectangular wing, $r/s = 0.2$

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(i) A = 1 rectangular wing, r/s = 0.2 - Concluded

α_B	x/r	δ_W									
		-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°
0°	6.94	.000	.001	.000	.000	.001	.000	.002			
	8.37	.000	.000	.001	.000	.000	.000	.000			
	9.81	.001	.001	.000	.000	.001	.000	.000			
	11.25	.000	.001	.000	.000	.001	.000	.000			
	12.69	.000	.001	.000	.000	.001	.000	.000			
	14.12	.000	.003	.000	.001	.069	.004	.000			
	15.56	-	.015	-	.028	-	.048	-	.082		.365
	17.00	-	.021	-	.049	-	.071	-	.108		.331
	18.44	-	.043	-	.079	-	.105	-	.146		.315
	19.87	-	.047	-	.079	-	.106	-	.141		.317
	21.31	-	.042	-	.056	-	.079	-	.101		.091
	22.75	-	.035	-	.059	-	.074	-	.099		.047
3°	8.37	.001	.001	.000	.001	.000	.001	.000			
	9.81	.002	.002	.001	.003	.003	.001	.003			
	11.25	.000	-	.001	.001	.000	.000	.000			
	12.69	.004	.003	.001	.003	.004	.004	.004			
	14.12	.007	.007	.001	.012	.012	.003	.001			
	15.56	.009	-	.014	.014	.018	.018	.013			
	17.00	-	.014	-	.014	-	.014	-	.014		
	18.44	-	.014	-	.014	-	.014	-	.014		
	19.87	-	.015	-	.028	-	.075	-	.115		
	21.31	-	.014	-	.010	-	.014	-	.014		
	22.75	-	.008	-	.010	-	.014	-	.014		
	24.19	-	.005	-	.020	-	.039	-	.059		
6°	8.37	.006	-	.014	-	.024	-	.026	-	.019	-
	9.81	.000	.000	.000	.000	.000	.000	.000			
	11.25	.000	.001	.001	.001	.001	.001	.001			
	12.69	.003	.005	.004	.002	.004	.003	.003			
	14.12	.017	.015	.011	.025	.011	.001	.001			
	15.56	.036	.028	.010	.006	.006	.001	.008			
	17.00	.037	.014	.010	.029	.066	.071	.041			
	18.44	.053	.023	.005	.026	.047	.041	.074			
	19.87	.053	.029	.007	.031	.037	.045	.056			
	21.31	.055	.032	.000	.026	.018	.024	.030			
	22.75	.056	.027	.004	.024	.027	.024	.034			
	24.19	.059	.016	.013	.027	.020	.007	.010			
10°	8.37	.002	.000	.001	.000	.000	.000	.001			
	9.81	.001	.000	.001	.001	.001	.001	.001			
	11.25	.001	.002	.002	.003	.003	.003	.006			
	12.69	.002	.002	.001	.002	.002	.002	.001			
	14.12	.047	.056	.016	.022	.040	.044	.022			
	15.56	.066	.054	.016	.024	.049	.044	.034			
	17.00	.066	.050	.019	.016	.037	.044	.030			
	18.44	.080	.060	.014	.016	.031	.044	.030			
	19.87	.092	.070	.019	.003	.011	.016	.017			
	21.31	.105	.070	.024	.003	.011	.018	.018			
	22.75	.088	.055	.010	.003	.001	.005	.008			
	24.19	.067	.033	.010	.001	.004	.004	.004			
15°	8.37	.008	.000	.001	.000	.000	.000	.001			
	9.81	.002	.002	.001	.003	.002	.001	.001			
	11.25	.004	.004	.001	.002	.003	.001	.006			
	12.69	.004	.004	.001	.002	.002	.001	.001			
	14.12	.022	.022	.002	.022	.022	.004	.004			
	15.56	.047	.058	.016	.028	.040	.047	.038			
	17.00	.050	.062	.016	.024	.049	.044	.034			
	18.44	.068	.076	.016	.024	.041	.056	.040			
	19.87	.088	.092	.013	.024	.041	.052	.048			
	21.31	.113	.072	.034	.010	.000	.005	.008			
	22.75	.130	.091	.040	.008	.000	.007	.010			
	24.19	.137	.096	.046	.008	.007	.019	.021			
20°	8.37	.008	.000	.001	.000	.000	.000	.001			
	9.81	.001	.003	.002	.003	.001	.001	.003			
	11.25	.000	.002	.002	.003	.001	.001	.002			
	12.69	.003	.005	.006	.005	.006	.008	.005			
	14.12	.055	.053	.010	.045	.042	.003	.002			
	15.56	.076	.074	.014	.064	.070	.075	.061			
	17.00	.078	.078	.015	.064	.076	.074	.064			
	18.44	.087	.090	.017	.067	.077	.086	.076			
	19.87	.108	.097	.027	.066	.076	.086	.076			
	21.31	.108	.097	.027	.066	.076	.086	.076			
	22.75	.108	.095	.027	.064	.074	.084	.074			
	24.19	.104	.070	.026	.062	.070	.089	.071			
25°	8.37	.008	.000	.001	.000	.000	.000	.001			
	9.81	.001	.000	.001	.000	.001	.001	.001			
	11.25	.000	.001	.001	.000	.002	.001	.002			
	12.69	.003	.001	.001	.002	.002	.005	.001			
	14.12	.081	.087	.005	.057	.036	.001	.004			
	15.56	.134	.148	.039	.139	.099	.086	.078			
	17.00	.134	.148	.039	.136	.068	.089	.078			
	18.44	.136	.148	.036	.135	.068	.090	.081			
	19.87	.136	.148	.036	.135	.068	.090	.081			
	21.31	.136	.148	.036	.134	.068	.090	.081			
	22.75	.136	.148	.036	.134	.068	.090	.081			
	24.19	.136	.148	.036	.134	.068	.090	.081			
25°	8.37	.008	.000	.001	.000	.000	.000	.001			
	9.81	.001	.000	.001	.000	.001	.001	.001			
	11.25	.000	.001	.001	.000	.002	.001	.002			
	12.69	.003	.001	.001	.002	.002	.005	.001			
	14.12	.081	.087	.005	.057	.036	.001	.004			
	15.56	.134	.148	.039	.139	.099	.086	.078			
	17.00	.134	.148	.039	.136	.068	.089	.078			
	18.44	.136	.148	.036	.135	.068	.090	.081			
	19.87	.136	.148	.036	.135	.068	.090	.081			
	21.31	.136	.148	.036	.134	.068	.090	.081			
	22.75	.136	.148	.036	.134	.068	.090	.081			
	24.19	.136	.148	.036	.134	.068	.090	.081			
	25.58	.136	.148	.036	.134	.068	.090	.081			

TABLE IV.--LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Continued
(j) $A = 1$ rectangular wing, $r/s = 0.4$

TABLE IV.- LONGITUDINAL INTERFERENCE LOADING COEFFICIENTS OF THE BODY IN
THE PRESENCE OF THE WINGS - Concluded
(j) $A = 1$ rectangular wing, $r/s = 0.4$ - Concluded

α_B	x/r		δ_w									
			-3°	-6°	-10°	-15°	-20°	-25°	-30°	-35°	-40°	-45°
0°	6.94	b001	.001	.000	.001	.003	.000	.000	.001	.000	.000	.000
	8.37	b001	.000	.000	b001	b000	.000	.000	b001	b000	b000	b000
	9.81	b001	.001	.000	b001	b000	.000	.001	b001	b001	b001	b001
	11.25	b000	.000	.000	b000	b000	.000	.001	b001	b001	b001	b001
	12.69	b000	.000	.000	b000	b000	.000	.001	b001	b001	b001	b001
	14.12	b000	.000	.000	b000	b000	.000	.001	b001	b001	b001	b001
	15.56	b000	.000	.000	b000	b000	.000	.001	b001	b001	b001	b001
	17.00	b000	.001	.000	b000	b000	.000	.001	b001	b001	b001	b001
	18.44	b001	.001	.000	b000	b000	.000	.001	b001	b001	b001	b001
	19.87	b001	.001	.000	b000	b000	.000	.001	b001	b001	b001	b001
	21.31	b001	.001	.000	b000	b000	.000	.001	b001	b001	b001	b001
3°	22.75	b005	.031	.030	b032	b027	b028	b024	b014	b017	b012	b020
	24.19	b005	.031	.030	b030	b027	b028	b024	b014	b017	b012	b020
	25.62	b005	.031	.030	b030	b027	b028	b024	b014	b017	b012	b020
	6.94	b002	.001	.000	b002	b002	b002	b002	b001	b002	b001	b002
	8.37	b002	.001	.000	b002	b002	b002	b002	b001	b002	b001	b002
	9.81	b002	.001	.000	b002	b002	b002	b002	b001	b002	b001	b002
	11.25	b002	.001	.000	b002	b002	b002	b002	b001	b002	b001	b002
	12.69	b006	.005	.006	b007	b006	b005	b005	b004	b005	b004	b005
	14.12	b006	.005	.006	b007	b006	b005	b005	b004	b005	b004	b005
	15.56	b006	.005	.006	b007	b006	b005	b005	b004	b005	b004	b005
	17.00	b003	.004	.005	b022	b027	b027	b027	b027	b059	b051	b079
	18.44	b011	.009	.028	b056	b056	b056	b056	b056	b098	b098	b063
	19.87	b011	.010	.028	b056	b056	b056	b056	b056	b094	b094	b012
	21.31	b011	.010	.028	b056	b056	b056	b056	b056	b094	b094	b012
6°	22.75	b004	.009	.018	b025	b025	b025	b025	b025	b034	b034	b021
	24.19	b004	.009	.018	b025	b025	b025	b025	b025	b034	b034	b021
	25.62	b008	.007	.007	b005	b002	b007	b16	b16	b01	b01	.010
	6.94	b000	.000	.001	b000	b000	b000	b000	b001	b000	b001	b000
	8.37	b002	.002	.000	b002	b002	b002	b002	b001	b001	b001	b002
	9.81	b000	.000	.001	b000	b000	b000	b000	b001	b000	b001	b000
	11.25	b000	.000	.001	b000	b000	b000	b000	b001	b000	b001	b000
	12.69	b001	.001	.005	b001	b004						
	14.12	b001	.001	.000	b001							
	15.56	b015	.005	.000	b030	b030	b049	b046	b041	b070	b081	.053
	17.00	b015	.005	.000	b030	b030	b046	b046	b045	b078	b078	.078
10°	18.44	b035	.018	.001	b029	b029	b046	b046	b045	b078	b078	.033
	19.87	b036	.016	.004	b029	b029	b046	b046	b045	b078	b078	.033
	21.31	b011	.016	.006	b029	b029	b046	b046	b045	b078	b078	.010
	22.75	b026	.023	.014	b012	b013	b016	b016	b015	b013	b013	.006
	24.19	b011	.012	.007	b006	b006	b006	b006	b005	b010	b010	.007
	25.62	b010	.012	.006	b003	b003	b006	b006	b005	b010	b010	.005
	6.94	b003	.003	.003	b001	b001	b002	b002	b001	b004	b004	b000
	8.37	b003	.002	.002	b001	b001	b003	b003	b001	b005	b005	.002
	9.81	b001	.001	.001	b001	b001	b003	b003	b001	b004	b004	.001
	11.25	b001	.001	.001	b001	b001	b003	b003	b001	b004	b004	.001
	12.69	b002	.001	.001	b002	b002	b003	b003	b001	b004	b004	.001
15°	14.12	b002	.001	.001	b002	b002	b003	b003	b001	b004	b004	.001
	15.56	b009	.006	.006	b008	b008	b004	b004	b003	b004	b004	.003
	17.00	b20	.017	.006	b006	b006	b004	b004	b003	b006	b006	.058
	18.44	b54	.048	.024	b024	b024	b003	b003	b002	b038	b038	.028
	19.87	b54	.049	.026	b026	b026	b003	b003	b002	b038	b038	.030
	21.31	b53	.037	.033	b018	b018	b011	b011	b007	b030	b030	.009
	22.75	b026	.023	.014	b012	b013	b016	b016	b015	b013	b013	.006
	24.19	b011	.012	.007	b006	b006	b006	b006	b005	b012	b012	.006
	25.62	b010	.012	.006	b003	b003	b006	b006	b005	b010	b010	.011
	6.94	b005	.003	.000	b004	b004	b004	b004	b003	b004	b004	b001
	8.37	b002	.004	.002	b002	b002	b003	b003	b002	b004	b004	.001
20°	9.81	b001	.004	.001	b002	b002	b003	b003	b002	b004	b004	.001
	11.25	b001	.004	.001	b002	b002	b003	b003	b002	b004	b004	.001
	12.69	b008	.004	.001	b008	b008	b006	b006	b005	b006	b006	.001
	14.12	b006	.004	.001	b008	b008	b006	b006	b005	b006	b006	.001
	15.56	b025	.027	.014	b014	b014	b013	b013	b012	b014	b014	.019
	17.00	b025	.027	.014	b014	b014	b013	b013	b012	b014	b014	.019
	18.44	b077	.061	.038	b038	b038	b019	b019	b015	b074	b074	.014
	19.87	b085	.068	.038	b038	b038	b019	b019	b015	b074	b074	.014
	21.31	b078	.065	.039	b039	b039	b019	b019	b015	b074	b074	.014
	22.75	b065	.068	.037	b037	b037	b018	b018	b015	b074	b074	.013
	24.19	b060	.068	.037	b037	b037	b018	b018	b015	b074	b074	.013
25°	25.62	b040	.039	.036	b036	b036	b005	b005	b004	b040	b040	.015
	6.94	.014	-	.005	-	.004	-	.002	-	.000	.000	.000
	8.37	.002	-	.008	-	.004	-	.003	-	.003	.003	.003
	9.81	.010	-	.003	-	.008	-	.006	-	.001	.001	.001
	11.25	.010	-	.005	-	.001	-	.007	-	.001	.001	.001
	12.69	.009	-	.005	-	.001	-	.004	-	.002	.001	.001
	14.12	.006	-	.004	-	.002	-	.003	-	.001	.001	.001
	15.56	.011	-	.004	-	.003	-	.006	-	.001	.001	.001
	17.00	b32	-	.014	-	.006	-	.003	-	.005	.005	.005
	18.44	b32	-	.014	-	.006	-	.003	-	.005	.005	.005
	19.87	b55	-	.024	-	.007	-	.002	-	.002	.002	.002
	21.31	b51	-	.024	-	.007	-	.002	-	.002	.002	.002
	22.75	b076	-	.025	-	.008	-	.002	-	.004	.013	.007
	24.19	b068	-	.025	-	.008	-	.002	-	.004	.013	.007
	25.62	b068	-	.028	-	.014	-	.001	-	.005	.014	.007

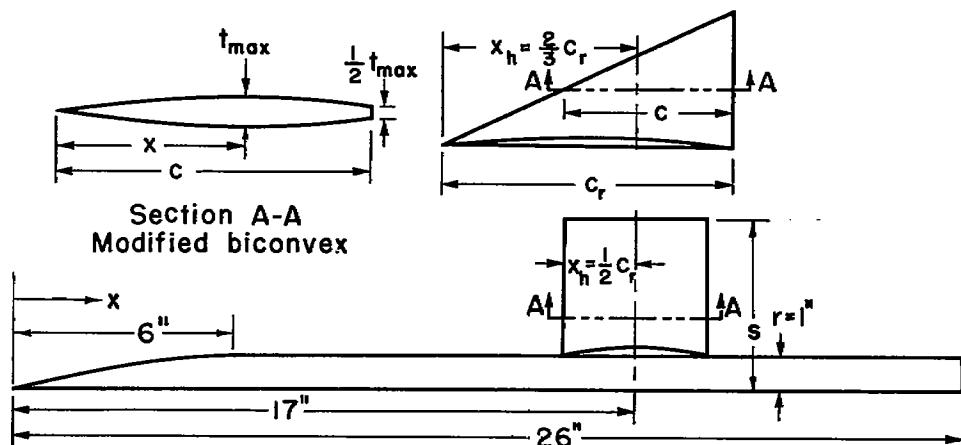
TABLE V.- PRESSURE COEFFICIENTS OF THE BODY ALONE
(a) Model I

θ	x/r	a_B						
		0°	3°	6°	10°	15°	20°	25°
7.02	-0.027	-0.34	-0.40	-0.47	-0.58	-0.79	-0.86	
8.56	-0.022	-0.26	-0.33	-0.38	-0.53	-0.79	-0.84	
9.94	-0.018	-0.22	-0.27	-0.38	-0.59	-0.76	-0.83	
11.34	-0.015	-0.22	-0.27	-0.33	-0.51	-0.76	-0.86	
12.59	-0.015	-0.17	-0.21	-0.21	-0.44	-0.75	-0.81	
13.84	-0.011	-0.10	-0.14	-0.17	-0.34	-0.64	-0.71	
15.09	-0.006	-0.07	-0.09	-0.10	-0.29	-0.58	-0.63	
16.34	-0.007	-0.04	-0.06	-0.07	-0.21	-0.52	-0.59	
17.56	-0.007	-0.04	-0.06	-0.07	-0.21	-0.52	-0.59	
18.84	-0.002	-0.02	-0.03	-0.04	-0.16	-0.48	-0.55	
20.09	-0.005	-0.02	-0.03	-0.04	-0.16	-0.48	-0.55	
21.34	-0.005	-0.02	-0.03	-0.04	-0.16	-0.48	-0.55	
22.59	-0.004	-0.02	-0.03	-0.04	-0.16	-0.48	-0.55	
23.84	-0.019	-0.11	-0.11	-0.11	-0.23	-0.52	-0.64	
25.09	-0.019	-0.11	-0.11	-0.11	-0.23	-0.52	-0.64	
7.02	-0.027	-0.33	-0.38	-0.48	-0.70	-0.81	-0.84	
8.56	-0.022	-0.24	-0.34	-0.49	-0.73	-0.83	-0.84	
9.94	-0.019	-0.21	-0.31	-0.48	-0.74	-0.78	-0.85	
11.34	-0.015	-0.17	-0.28	-0.47	-0.75	-0.78	-0.86	
12.59	-0.015	-0.17	-0.28	-0.41	-0.70	-0.71	-0.81	
13.84	-0.011	-0.10	-0.19	-0.37	-0.67	-0.78	-0.79	
15.09	-0.006	-0.07	-0.19	-0.36	-0.66	-0.77	-0.80	
16.34	-0.007	-0.04	-0.16	-0.42	-0.63	-0.79	-0.80	
17.56	-0.007	-0.04	-0.14	-0.41	-0.64	-0.78	-0.77	
18.84	-0.002	-0.02	-0.13	-0.37	-0.60	-0.77	-0.78	
20.09	-0.005	-0.02	-0.13	-0.37	-0.60	-0.78	-0.79	
21.34	-0.005	-0.02	-0.13	-0.37	-0.60	-0.78	-0.79	
22.59	-0.005	-0.02	-0.13	-0.37	-0.60	-0.78	-0.79	
23.84	-0.005	-0.02	-0.13	-0.37	-0.60	-0.78	-0.79	
25.09	-0.005	-0.02	-0.13	-0.37	-0.60	-0.78	-0.79	
7.02	-0.027	-0.37	-0.44	-0.57	-0.86	-0.97	-0.97	
8.56	-0.024	-0.30	-0.34	-0.57	-0.69	-0.78	-0.86	
9.94	-0.021	-0.28	-0.34	-0.57	-0.70	-0.78	-0.82	
11.34	-0.019	-0.21	-0.29	-0.53	-0.71	-0.68	-0.75	
12.59	-0.015	-0.17	-0.23	-0.53	-0.61	-0.68	-0.79	
13.84	-0.015	-0.17	-0.23	-0.53	-0.61	-0.68	-0.79	
15.09	-0.011	-0.10	-0.19	-0.38	-0.51	-0.65	-0.76	
16.34	-0.006	-0.07	-0.18	-0.38	-0.50	-0.65	-0.76	
17.56	-0.006	-0.07	-0.18	-0.38	-0.50	-0.65	-0.76	
18.84	-0.002	-0.02	-0.18	-0.38	-0.50	-0.65	-0.76	
20.09	-0.005	-0.02	-0.18	-0.38	-0.50	-0.65	-0.76	
21.34	-0.005	-0.02	-0.18	-0.38	-0.50	-0.65	-0.76	
22.59	-0.005	-0.02	-0.18	-0.38	-0.50	-0.65	-0.76	
23.84	-0.005	-0.02	-0.18	-0.38	-0.50	-0.65	-0.76	
25.09	-0.005	-0.02	-0.18	-0.38	-0.50	-0.65	-0.76	
7.02	-0.027	-0.37	-0.44	-0.57	-0.86	-0.97	-0.97	
8.56	-0.024	-0.30	-0.34	-0.57	-0.69	-0.78	-0.86	
9.94	-0.021	-0.28	-0.34	-0.57	-0.70	-0.78	-0.82	
11.34	-0.019	-0.21	-0.29	-0.53	-0.61	-0.68	-0.75	
12.59	-0.015	-0.17	-0.23	-0.53	-0.54	-0.65	-0.79	
13.84	-0.015	-0.17	-0.23	-0.53	-0.54	-0.65	-0.79	
15.09	-0.011	-0.10	-0.15	-0.26	-0.44	-0.60	-0.77	
16.34	-0.006	-0.07	-0.15	-0.26	-0.44	-0.61	-0.77	
17.56	-0.006	-0.07	-0.15	-0.26	-0.44	-0.61	-0.77	
18.84	-0.002	-0.02	-0.15	-0.26	-0.44	-0.61	-0.77	
20.09	-0.005	-0.02	-0.15	-0.26	-0.44	-0.61	-0.77	
21.34	-0.005	-0.02	-0.15	-0.26	-0.44	-0.61	-0.77	
22.59	-0.005	-0.02	-0.15	-0.26	-0.44	-0.61	-0.77	
23.84	-0.005	-0.02	-0.15	-0.26	-0.44	-0.61	-0.77	
25.09	-0.005	-0.02	-0.15	-0.26	-0.44	-0.61	-0.77	
7.02	-0.027	-0.37	-0.40	-0.56	-0.76	-0.79	-0.87	
8.56	-0.024	-0.32	-0.37	-0.56	-0.69	-0.77	-0.85	
9.94	-0.021	-0.32	-0.37	-0.56	-0.69	-0.77	-0.84	
11.34	-0.019	-0.27	-0.32	-0.57	-0.54	-0.68	-0.81	
12.59	-0.015	-0.27	-0.32	-0.57	-0.54	-0.68	-0.81	
13.84	-0.015	-0.27	-0.32	-0.57	-0.54	-0.68	-0.81	
15.09	-0.011	-0.15	-0.21	-0.26	-0.44	-0.69	-0.77	
16.34	-0.006	-0.09	-0.15	-0.21	-0.41	-0.69	-0.75	
17.56	-0.006	-0.09	-0.15	-0.21	-0.41	-0.69	-0.75	
18.84	-0.002	-0.04	-0.15	-0.21	-0.33	-0.63	-0.73	
20.09	-0.005	-0.01	-0.15	-0.21	-0.33	-0.63	-0.73	
21.34	-0.005	-0.01	-0.15	-0.21	-0.33	-0.63	-0.73	
22.59	-0.005	-0.01	-0.15	-0.21	-0.33	-0.63	-0.73	
23.84	-0.005	-0.01	-0.15	-0.21	-0.33	-0.63	-0.73	
25.09	-0.005	-0.01	-0.15	-0.21	-0.33	-0.63	-0.73	

θ	x/r	a_B						
		0°	3°	6°	10°	15°	20°	25°
7.02	-0.027	-0.30	-0.36	-0.41	-0.51	-0.72	-0.87	1.20
8.56	-0.024	-0.26	-0.32	-0.38	-0.48	-0.65	-0.77	1.012
9.94	-0.021	-0.22	-0.27	-0.33	-0.43	-0.60	-0.74	1.128
11.34	-0.019	-0.19	-0.22	-0.27	-0.31	-0.48	-0.63	1.095
12.59	-0.015	-0.15	-0.19	-0.21	-0.24	-0.40	-0.57	1.158
13.84	-0.015	-0.15	-0.19	-0.21	-0.24	-0.40	-0.57	1.158
15.09	-0.011	-0.10	-0.14	-0.17	-0.21	-0.37	-0.53	1.175
16.34	-0.006	-0.07	-0.10	-0.13	-0.16	-0.30	-0.49	1.175
17.56	-0.006	-0.07	-0.10	-0.13	-0.16	-0.30	-0.49	1.175
18.84	-0.002	-0.02	-0.05	-0.08	-0.11	-0.27	-0.48	1.175
20.09	-0.005	-0.01	-0.05	-0.08	-0.11	-0.27	-0.48	1.175
21.34	-0.005	-0.01	-0.05	-0.08	-0.11	-0.27	-0.48	1.175
22.59	-0.005	-0.01	-0.05	-0.08	-0.11	-0.27	-0.48	1.175
23.84	-0.005	-0.01	-0.05	-0.08	-0.11	-0.27	-0.48	1.175
25.09	-0.005	-0.01	-0.05	-0.08	-0.11	-0.27	-0.48	1.175

TABLE V.- PRESSURE COEFFICIENTS OF THE BODY ALONE - Concluded
(b) Model II

θ	x/l	C_B						
		0°	3°	6°	10°	15°	20°	25°
6°	6.94	- .028	- .036	- .042	- .049	- .059	- .069	- .086
	8.37	- .023	- .027	- .034	- .040	- .050	- .066	- .084
	9.81	- .019	- .024	- .027	- .038	- .059	- .066	- .084
	11.25	- .020	- .021	- .021	- .033	- .061	- .066	- .086
	12.69	- .015	- .017	- .016	- .020	- .059	- .065	- .081
	14.13	- .010	- .016	- .016	- .025	- .065	- .071	- .080
	15.56	- .005	- .011	- .016	- .025	- .065	- .071	- .078
	17.00	- .004	- .004	- .005	- .027	- .068	- .070	- .069
	18.44	- .003	- .004	- .004	- .027	- .068	- .064	- .065
	19.87	- .002	- .002	- .004	- .028	- .063	- .054	- .068
	21.31	- .006	- .006	- .004	- .028	- .066	- .051	- .064
	22.75	- .008	- .012	- .004	- .028	- .064	- .052	- .064
	24.19	- .008	- .012	- .004	- .028	- .064	- .052	- .064
	25.63	- .008	- .012	- .004	- .028	- .064	- .052	- .064
15°	6.94	- .029	- .034	- .047	- .069	- .083	- .083	- .083
	8.37	- .029	- .034	- .046	- .074	- .084	- .084	- .084
	9.81	- .019	- .024	- .046	- .075	- .080	- .086	- .086
	11.25	- .016	- .021	- .046	- .069	- .074	- .078	- .078
	12.69	- .016	- .021	- .046	- .067	- .074	- .078	- .079
	14.13	- .010	- .016	- .046	- .063	- .070	- .073	- .073
	15.56	- .007	- .011	- .046	- .063	- .070	- .073	- .073
	17.00	- .004	- .008	- .046	- .063	- .069	- .070	- .070
	18.44	- .003	- .008	- .046	- .063	- .069	- .067	- .067
	19.87	- .002	- .008	- .046	- .063	- .061	- .063	- .063
	21.31	- .006	- .012	- .046	- .063	- .061	- .063	- .063
	22.75	- .006	- .012	- .046	- .063	- .061	- .063	- .063
	24.19	- .006	- .012	- .046	- .063	- .061	- .063	- .063
	25.63	- .006	- .012	- .046	- .063	- .061	- .063	- .063
30°	6.94	- .036	- .046	- .056	- .086	- .097	- .097	- .097
	8.37	- .030	- .036	- .056	- .086	- .096	- .096	- .096
	9.81	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	11.25	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	12.69	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	14.13	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	15.56	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	17.00	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	18.44	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	19.87	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	21.31	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	22.75	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	24.19	- .024	- .029	- .046	- .086	- .096	- .096	- .096
	25.63	- .024	- .029	- .046	- .086	- .096	- .096	- .096
60°	6.94	- .031	- .040	- .054	- .078	- .080	- .087	- .087
	8.37	- .029	- .036	- .048	- .080	- .086	- .088	- .088
	9.81	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	11.25	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	12.69	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	14.13	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	15.56	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	17.00	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	18.44	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	19.87	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	21.31	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	22.75	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	24.19	- .019	- .024	- .048	- .084	- .086	- .088	- .088
	25.63	- .019	- .024	- .048	- .084	- .086	- .088	- .088



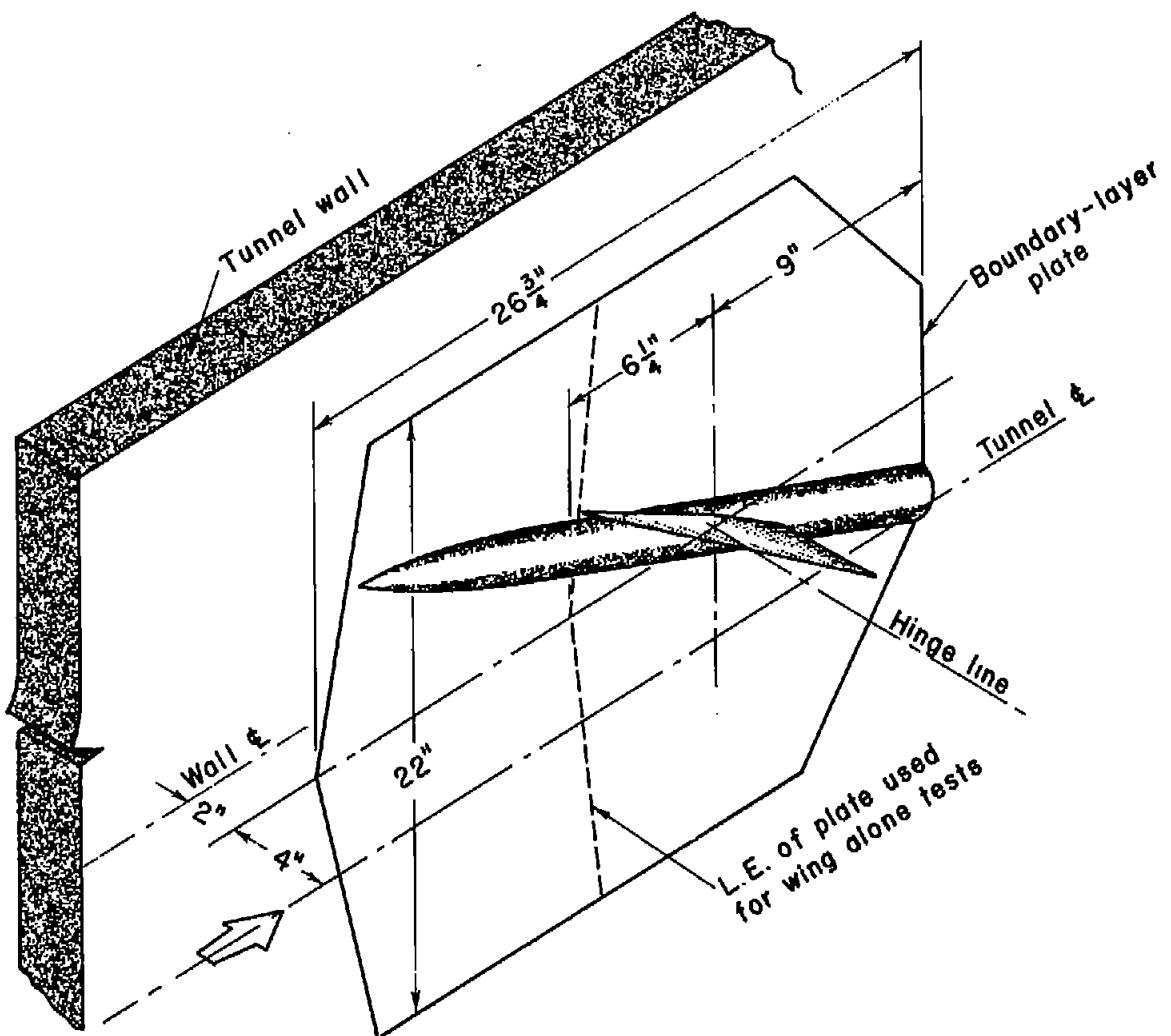
Triangular plan forms								
Model	A	r/s	s in	c_r in	S in 2	t/c_{max}	x/c_{max}	Wing test
	4	.2	5	4	8	.05	.50	press.
	2	.2	5	8	16	.05	.50	press.
	1	.2	5	16	32	.04	.59	force
	1	.4	2.5	6	4.5	.04	.59	force
	$\frac{2}{3}$	4	2.5	9	6.75	.04	.59	force
	$\frac{3}{8}$	4	2.5	16	12	.04	.59	force

Rectangular plan forms								
Model	A	r/s	s in	c_r in	S in 2	t/c_{max}	x/c_{max}	Wing test
	3	.2	5	2.667	10.667	.04	.59	force
	2	.2	5	4	16	.05	.50	press.
	1	.2	5	8	32	.04	.59	force
	1	.4	2.5	3	4.5	.04	.59	force

* Plan form for $7/16$ scale full-span models.

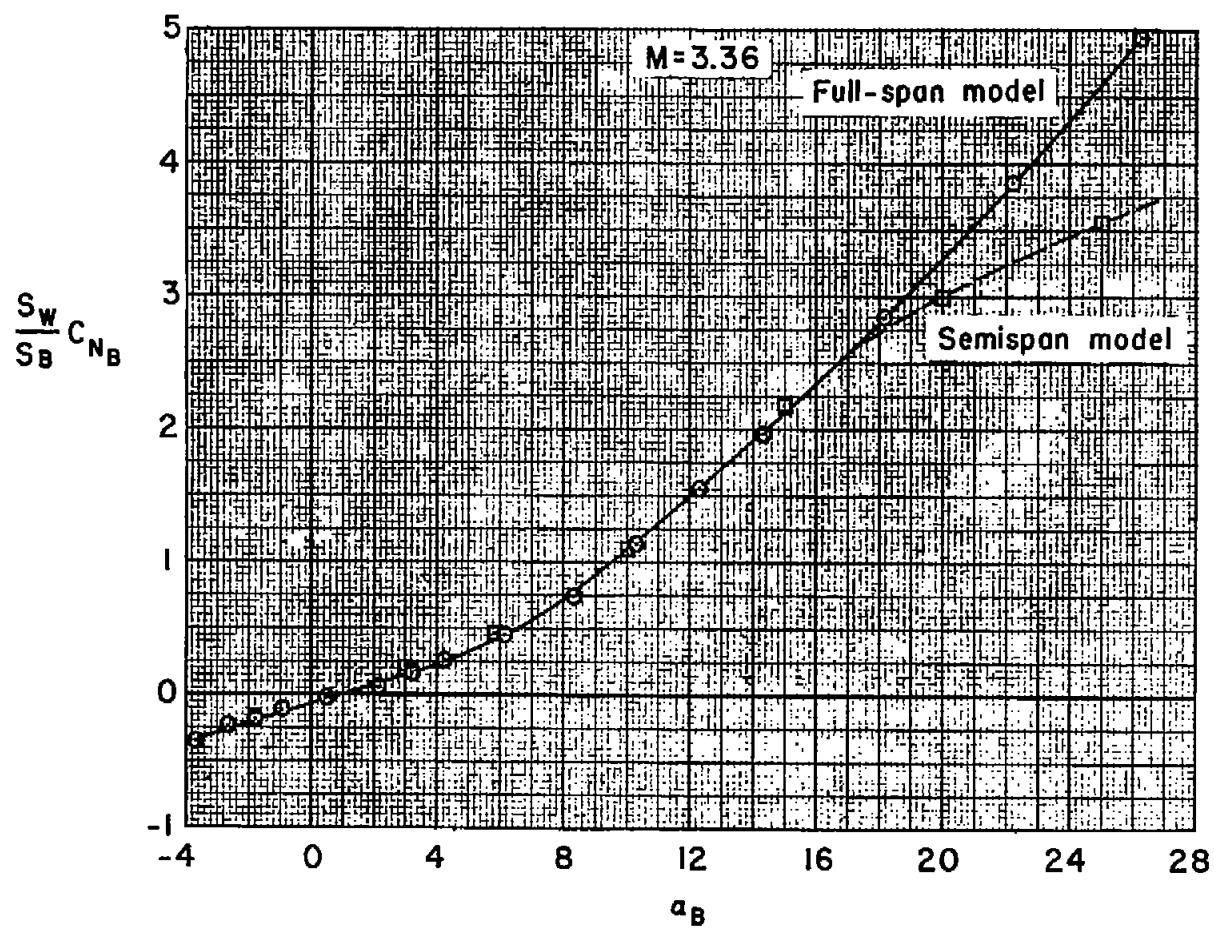
(a) Summary of model geometry and dimensions.

Figure 1.- Models and semispan supports.



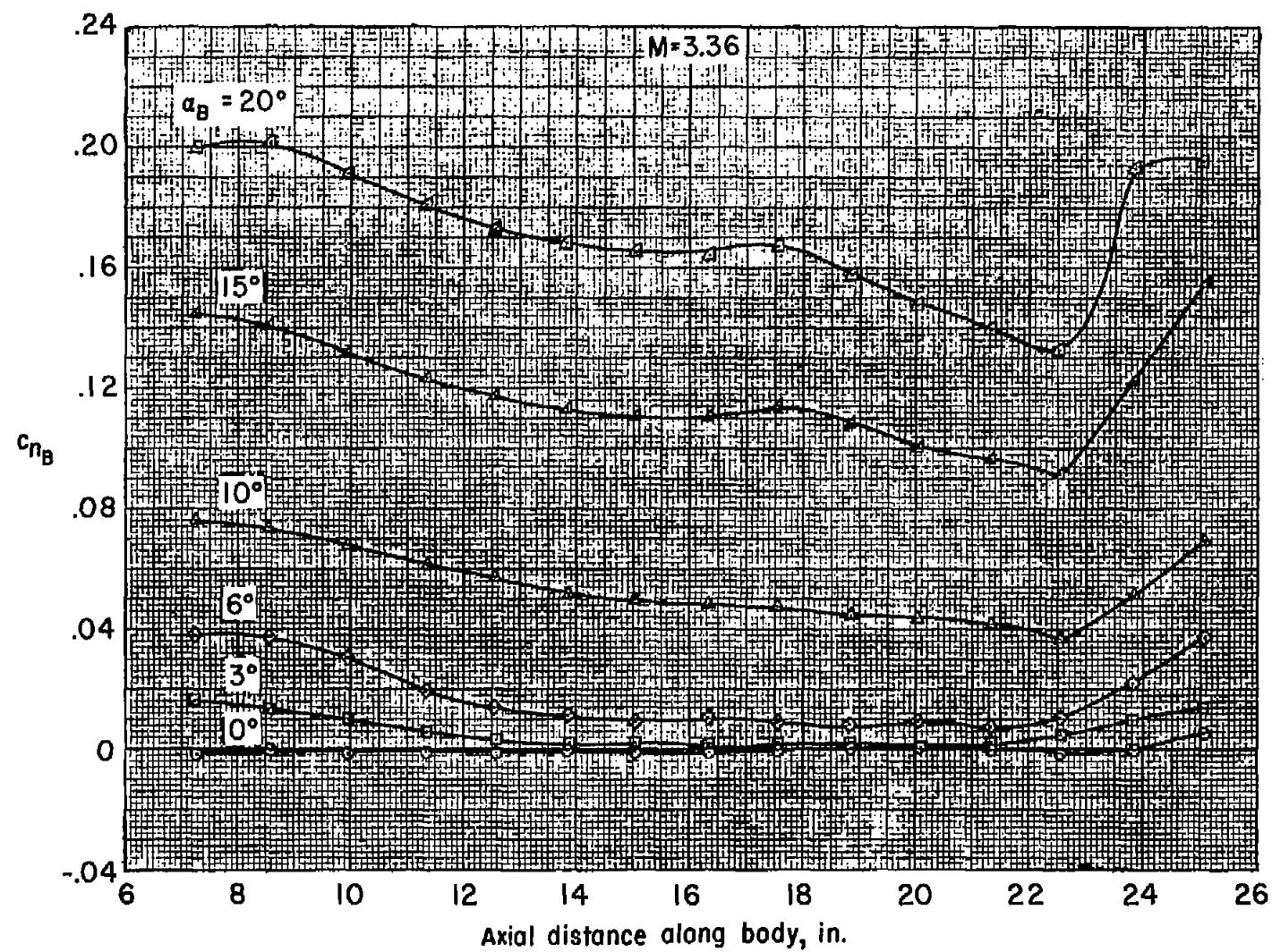
(b) Semispan model installation.

Figure 1.- Concluded.



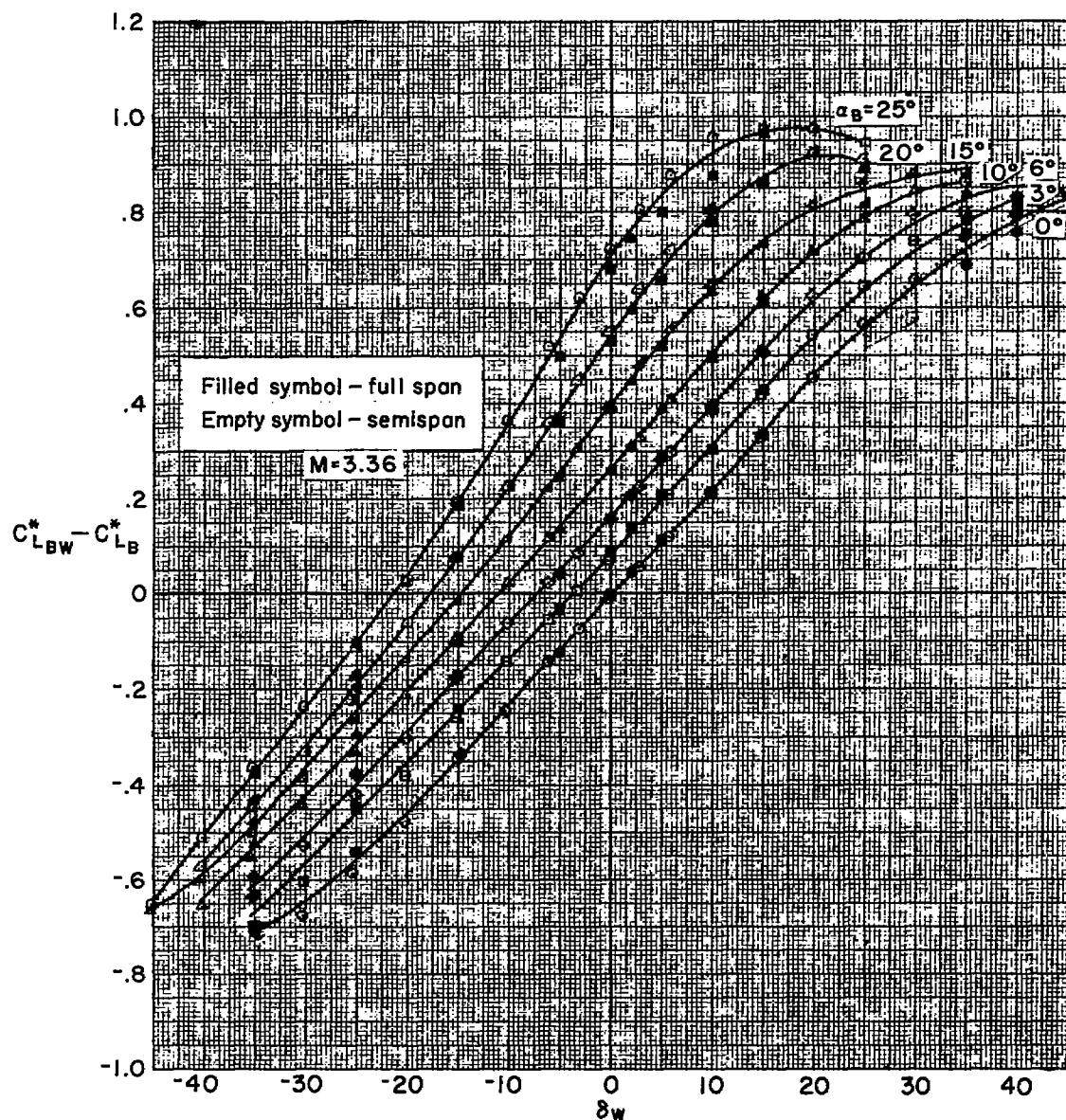
(a) Comparison of the variation of normal-force coefficient with angle of attack for the half body and full body.

Figure 2.- Body alone characteristics.



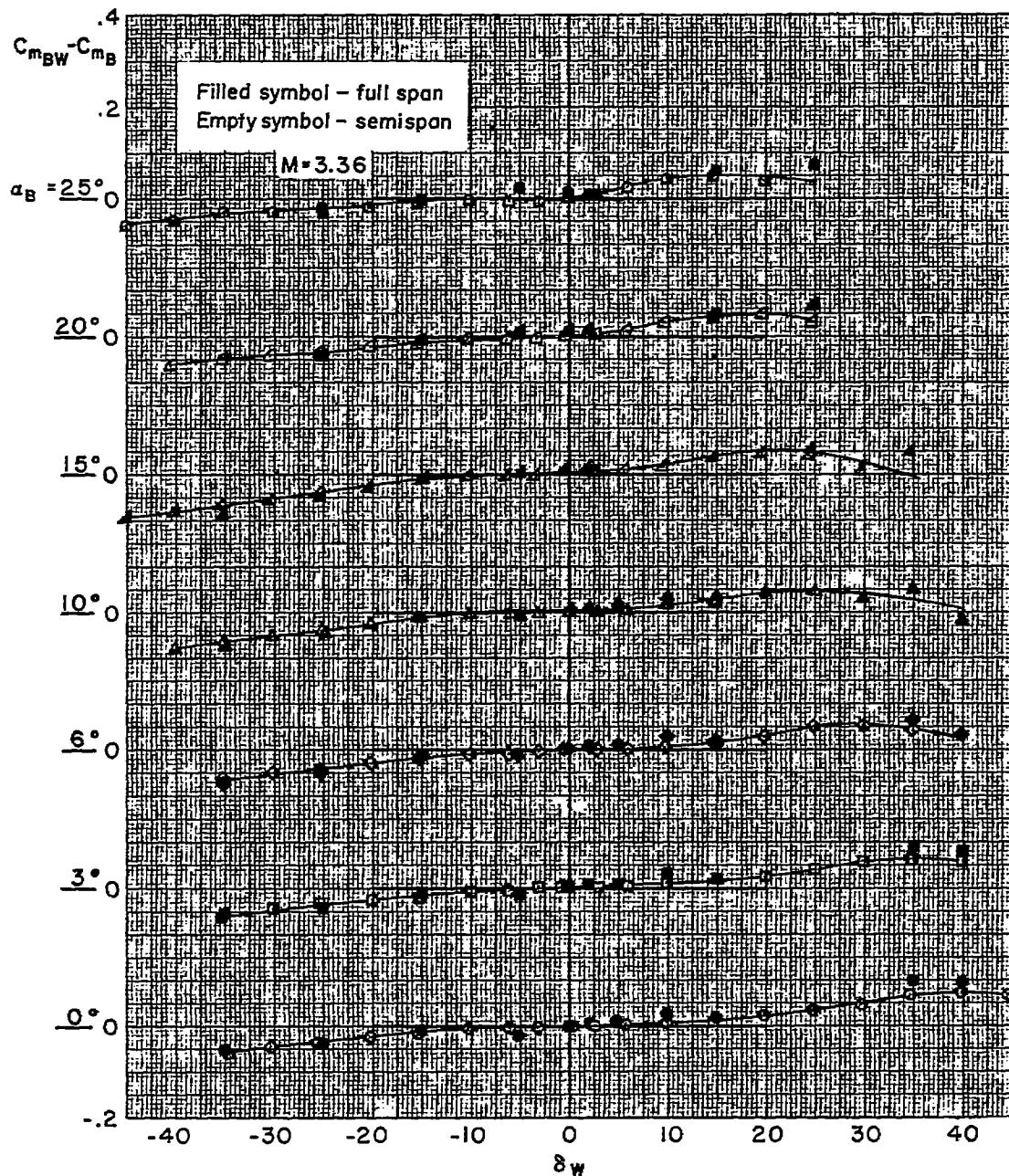
(b) Local normal-force coefficients at several angles of attack for half body.

Figure 2.- Concluded.



- (a) Variation with wing deflection angle of normal-force coefficient for the $A = 1$ rectangular wing and body combination minus that for body alone.

Figure 3.- Comparison of semispan and full-span model data.



- (b) Variation with wing deflection angle of the pitching-moment coefficient for the $A = 1$ rectangular wing and body combination minus that for the body alone.

Figure 3.- Concluded.

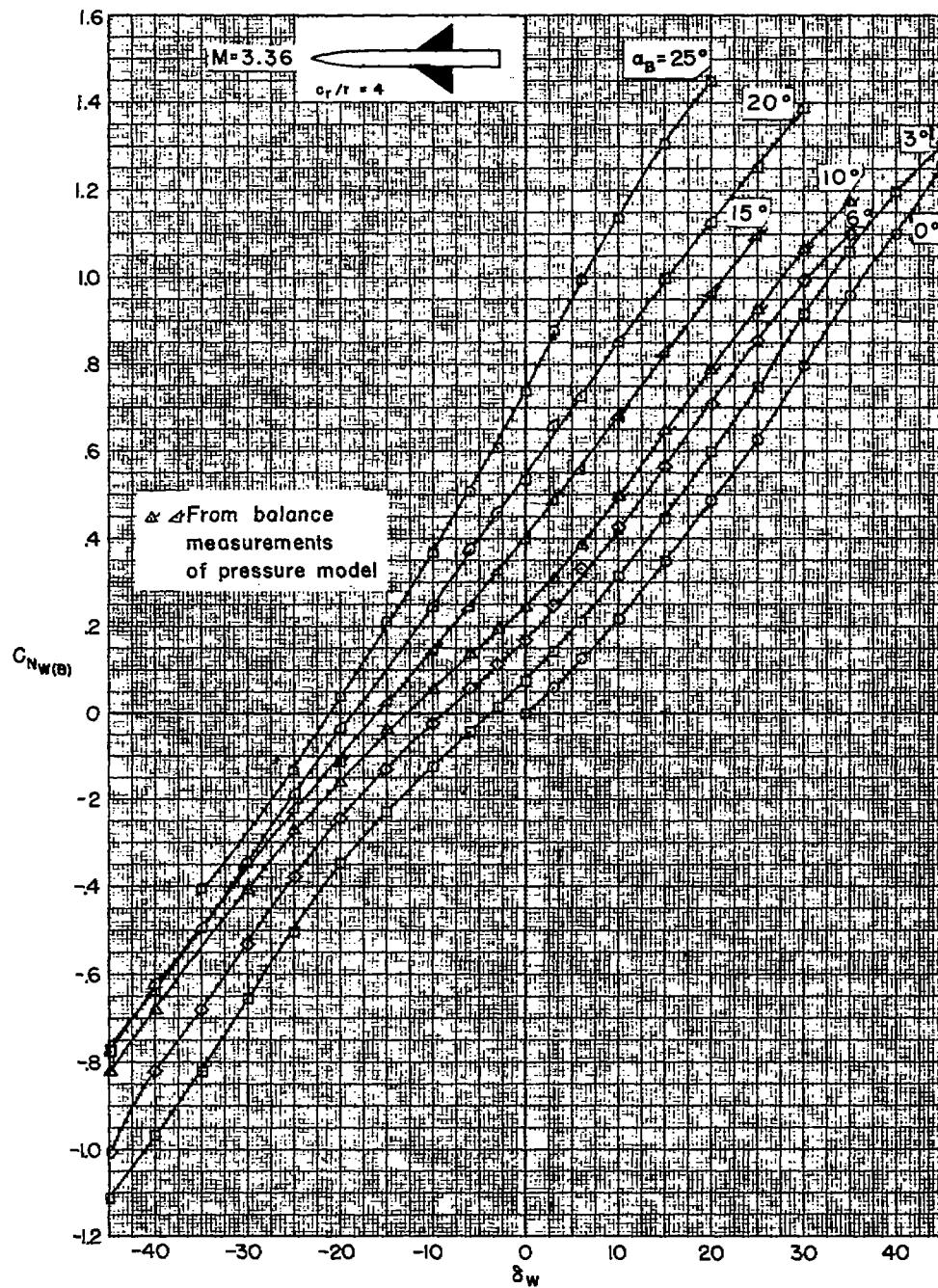
(a) $A = 4$ triangular wing, $r/s = 0.2$.

Figure 4.- Variation with deflection angle of normal-force coefficient for the wings in the presence of the body.

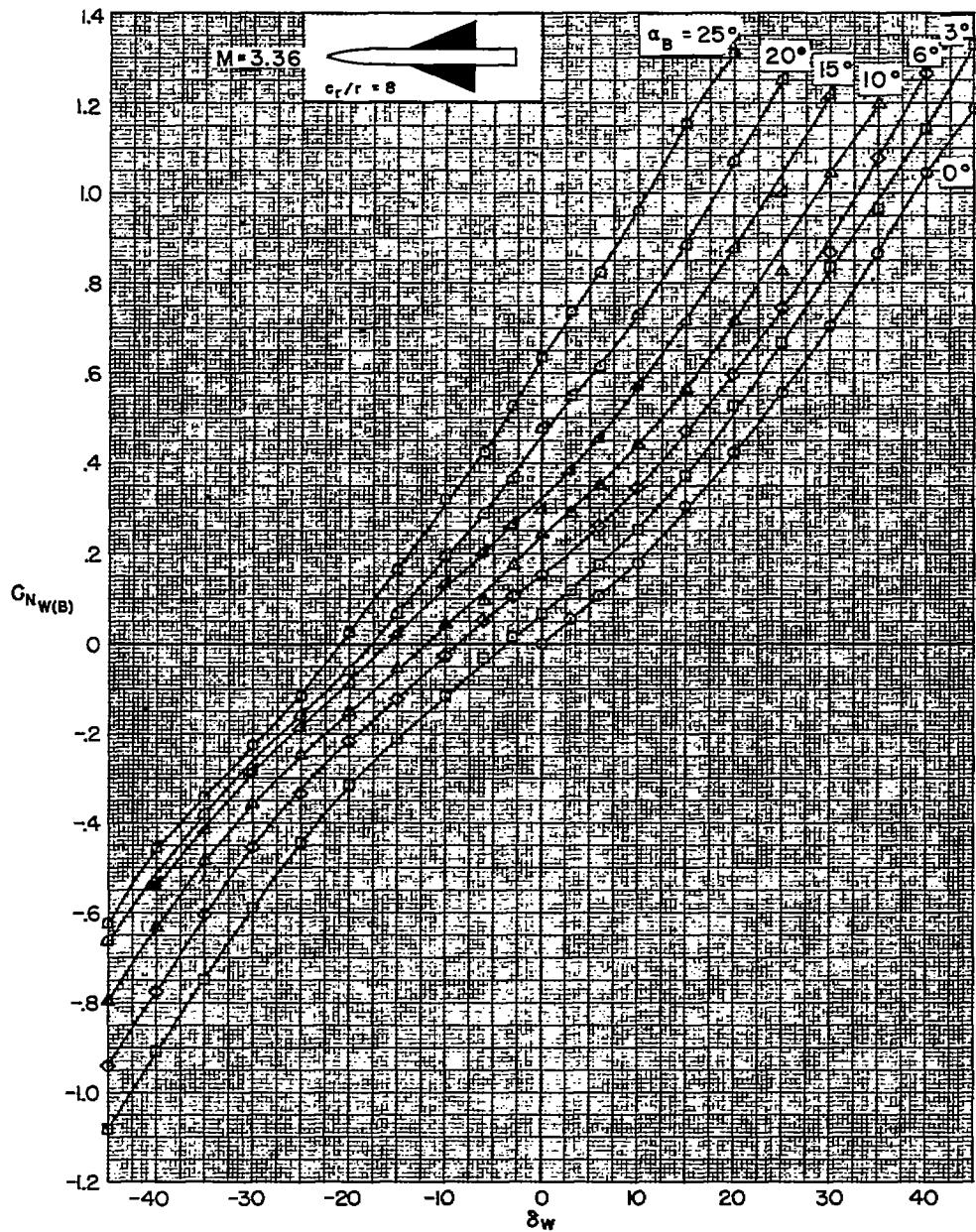
(b) $A = 2$ triangular wing, $r/s = 0.2$.

Figure 4.- Continued.

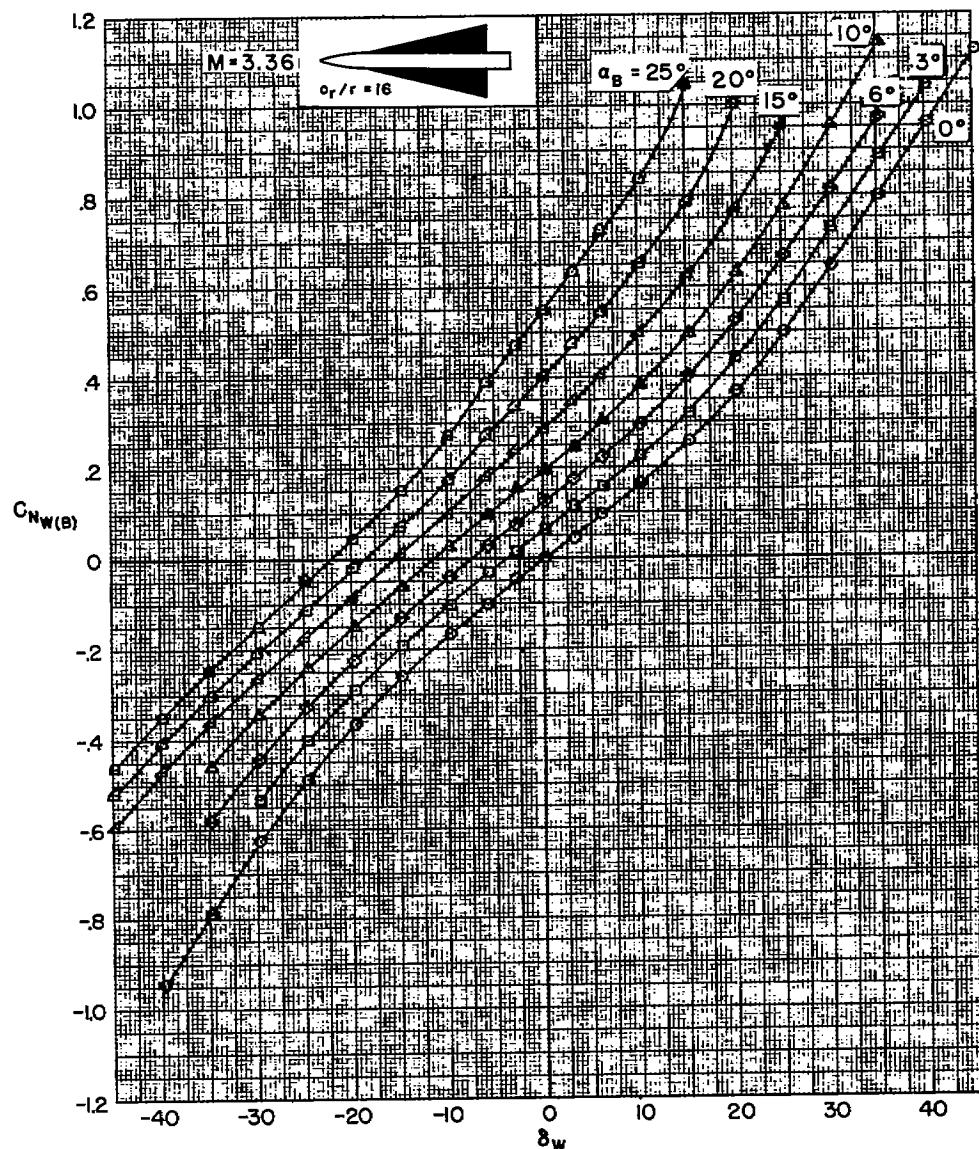
(c) $A = 1$ triangular wing, $r/s = 0.2$.

Figure 4.- Continued.

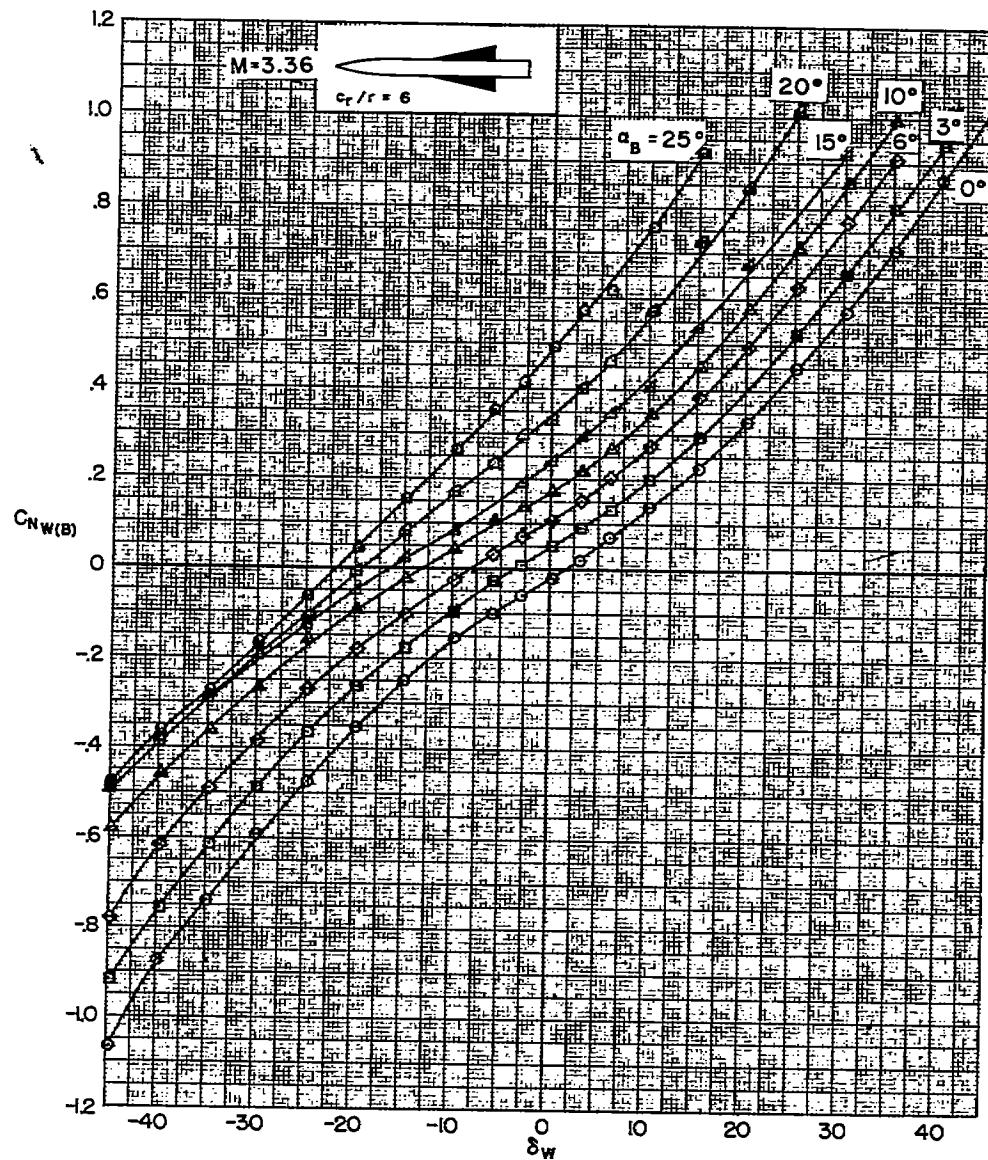
(d) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 4.- Continued.

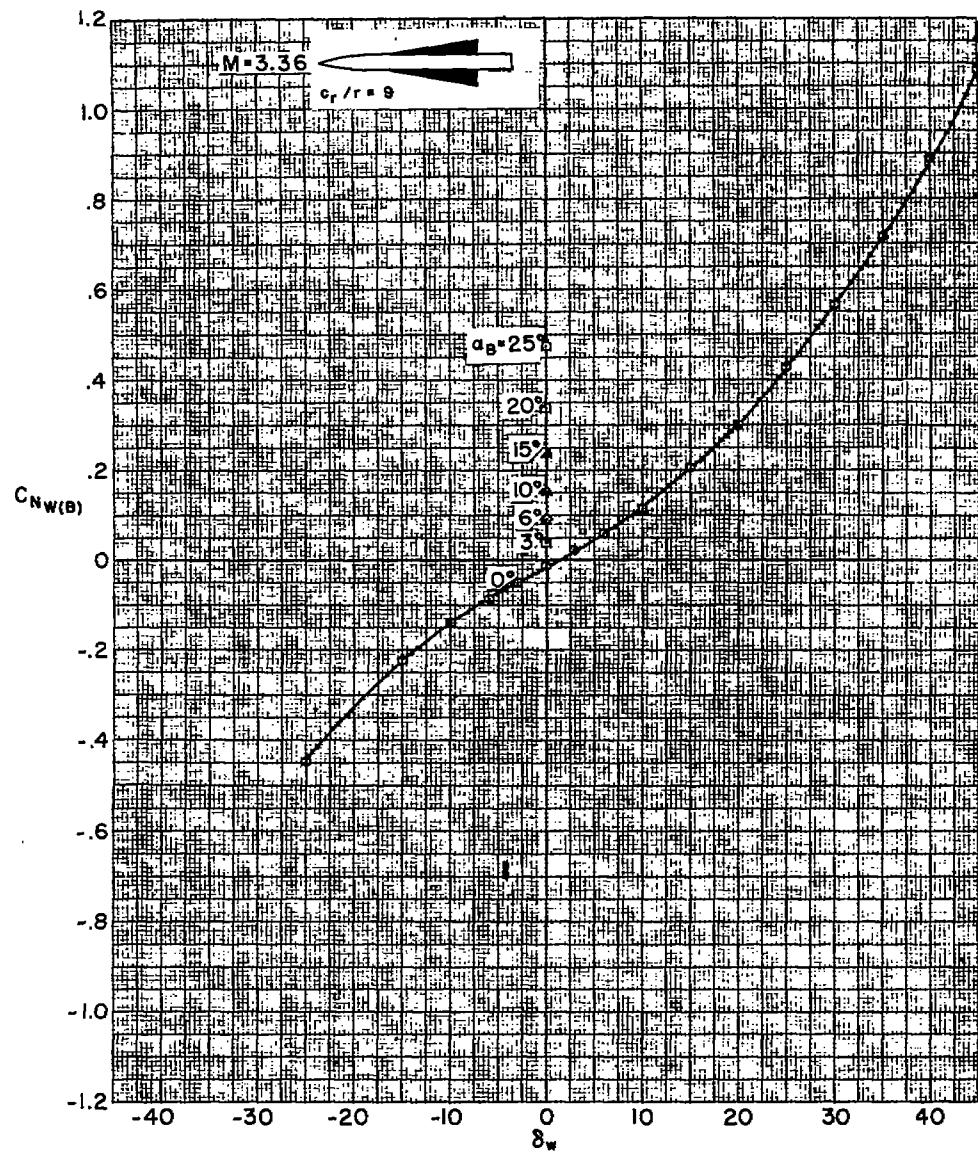
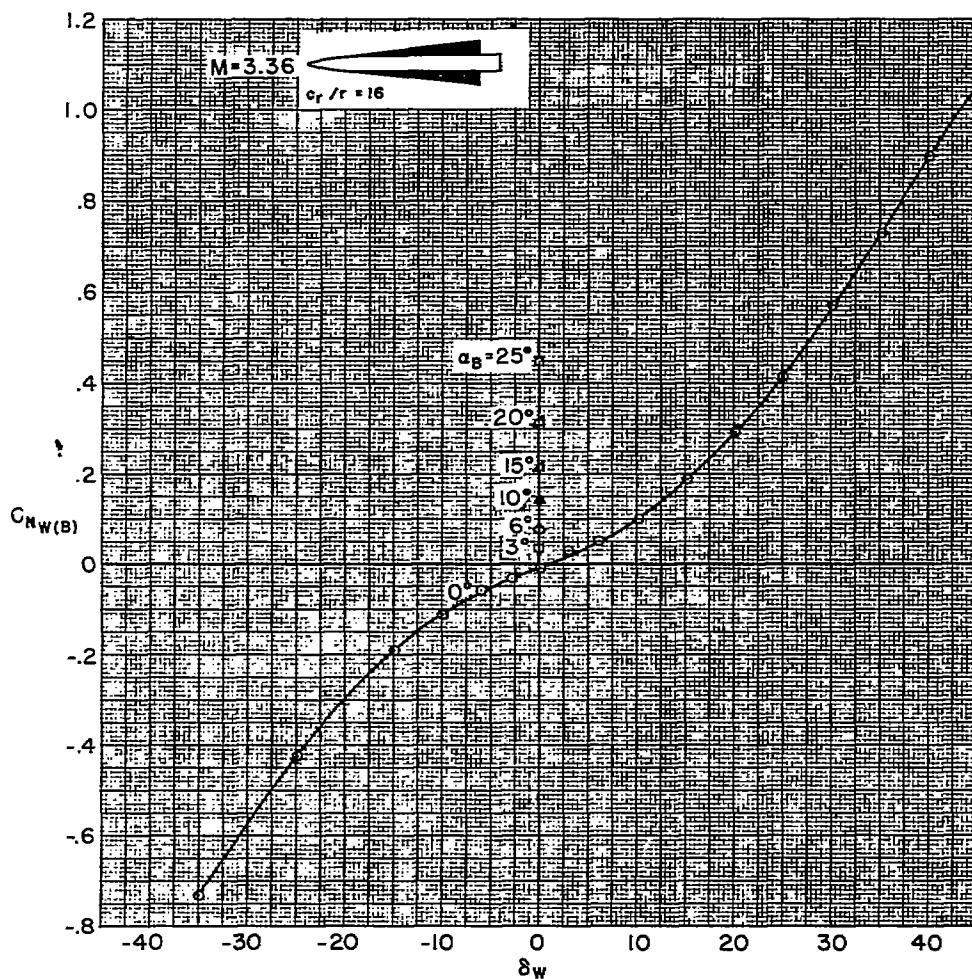
(e) $A = 2/3$ triangular wing, $r/s = 0.4$.

Figure 4.- Continued.



(f) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 4.- Continued.

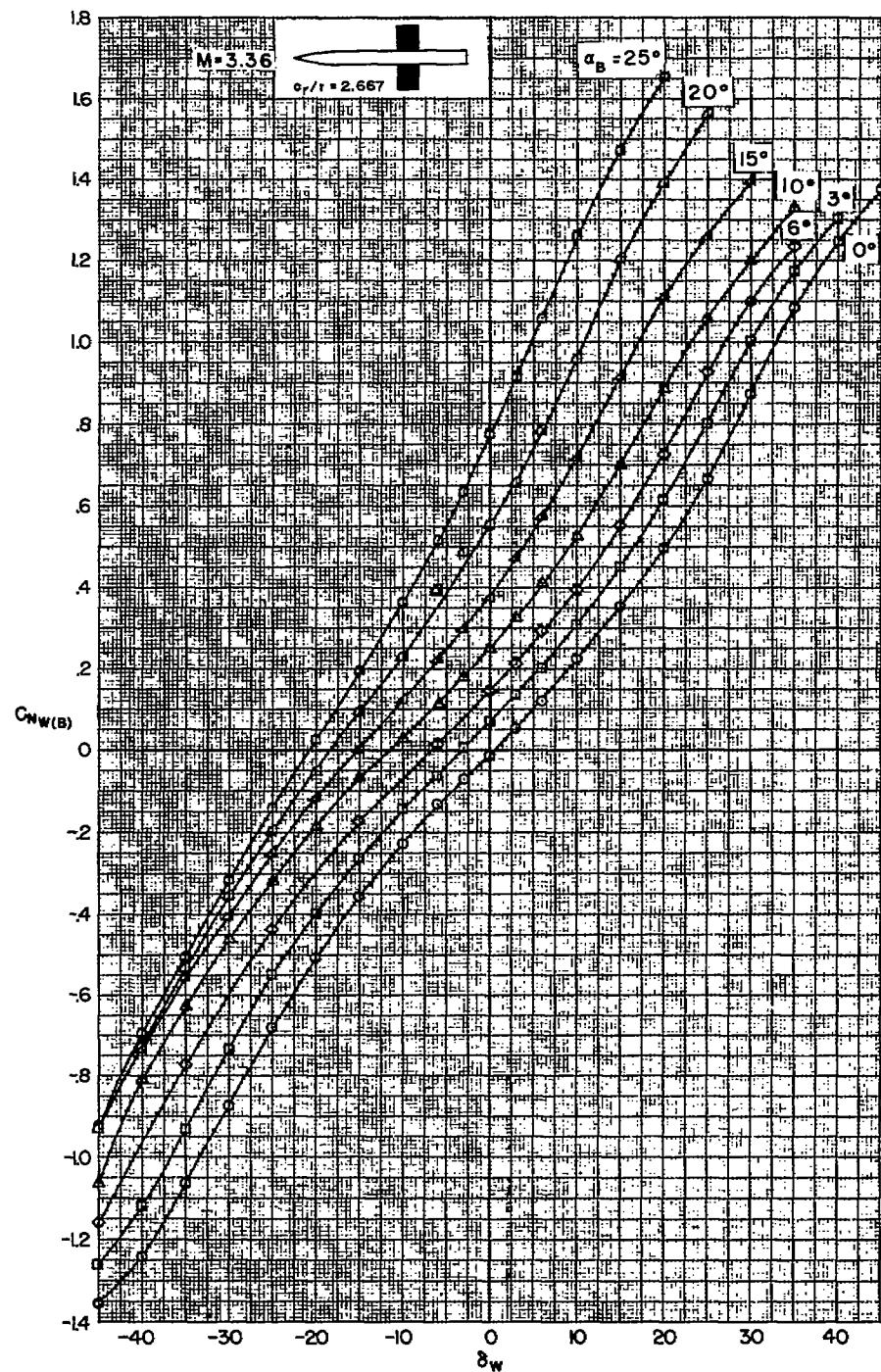
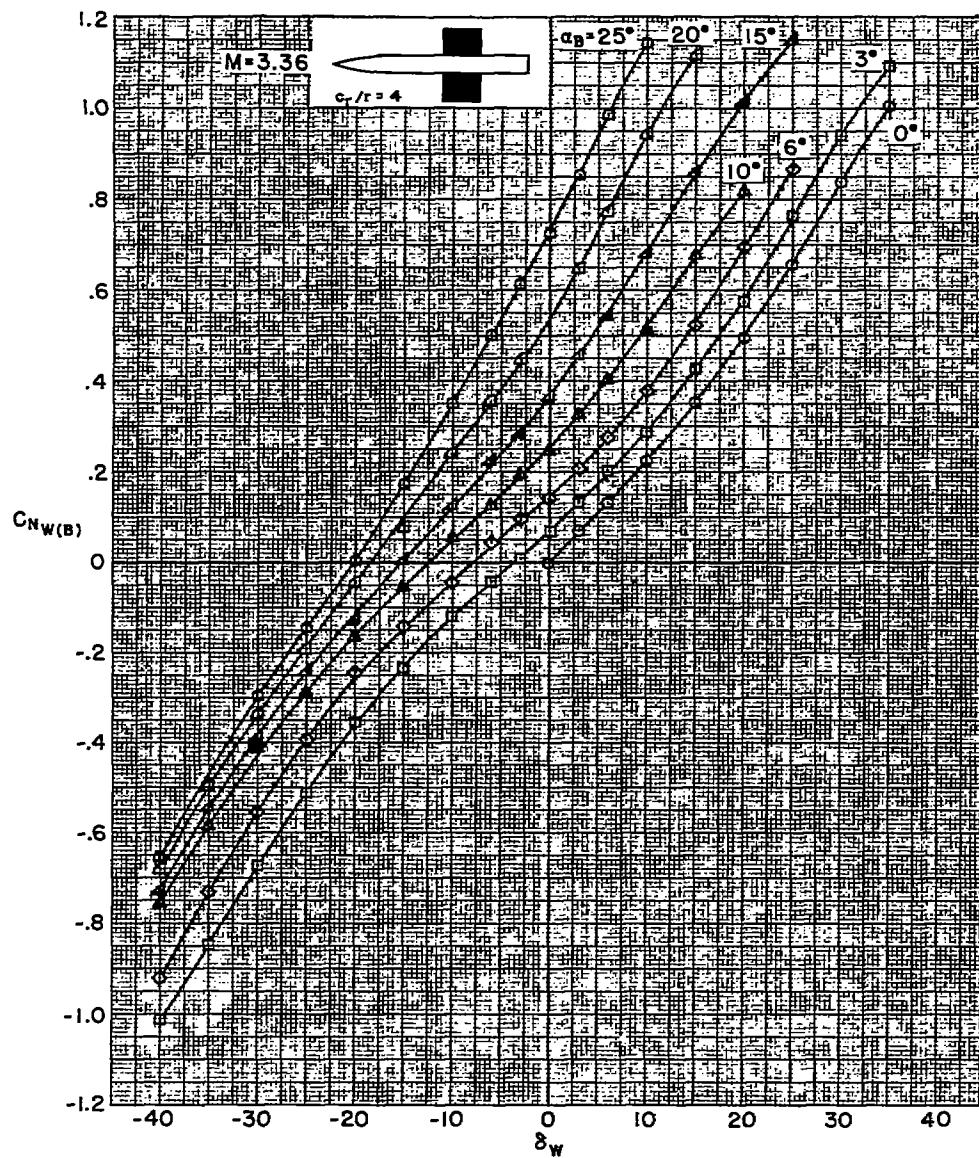
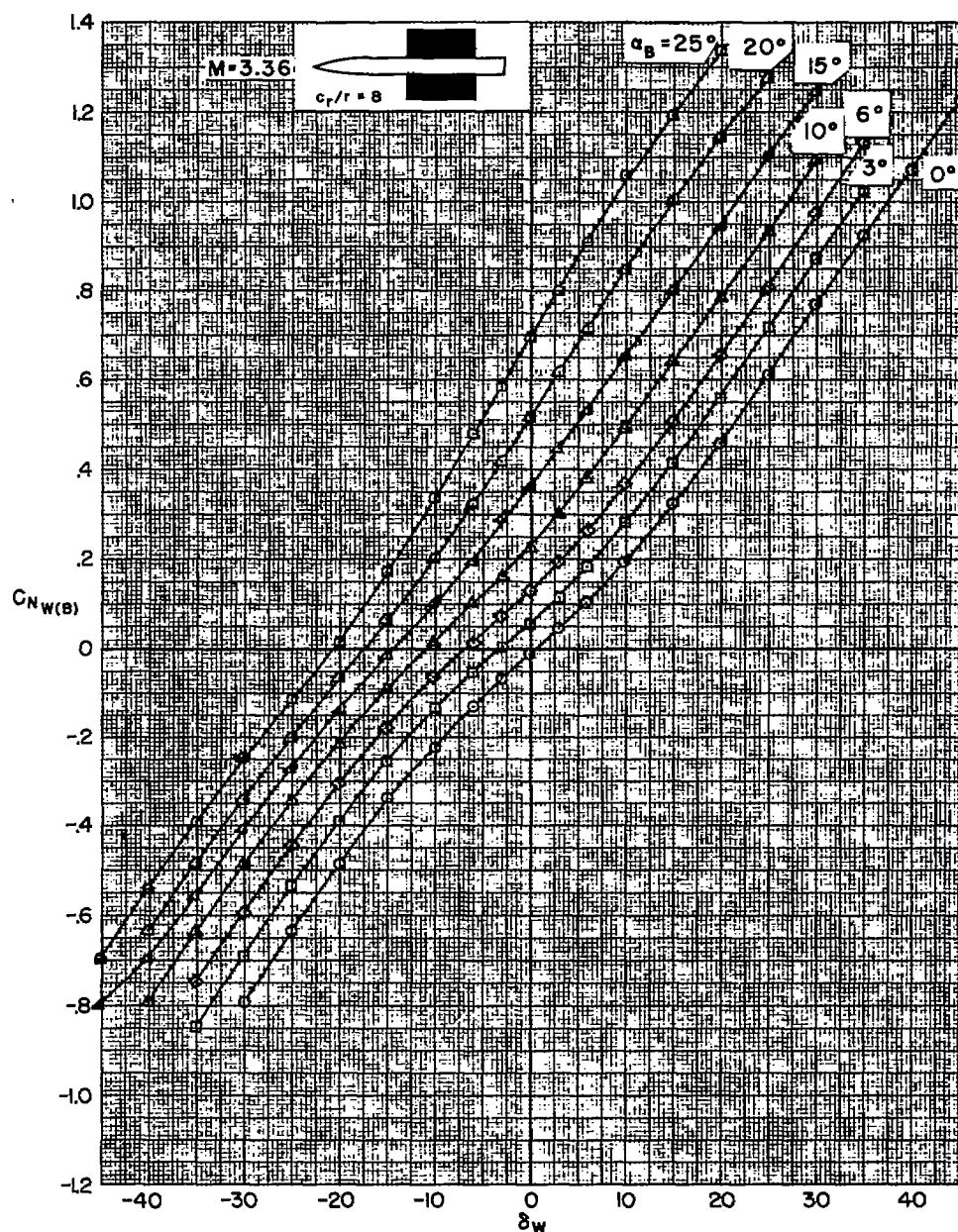
(g) $A = 3$ rectangular wing, $r/s = 0.2$.

Figure 4.- Continued.



(h) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 4.- Continued.



(i) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 4.- Continued.

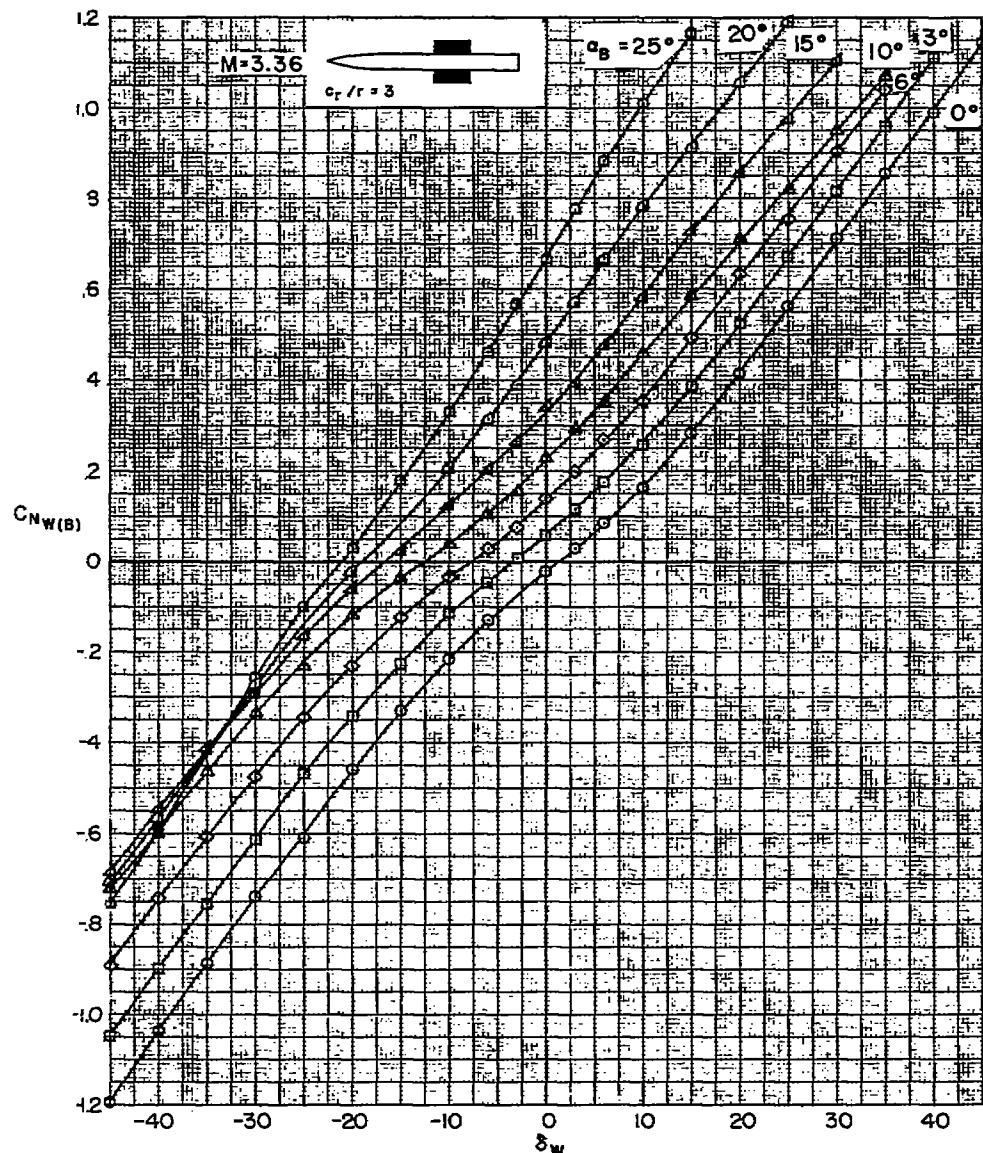
(j) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 4.- Concluded.

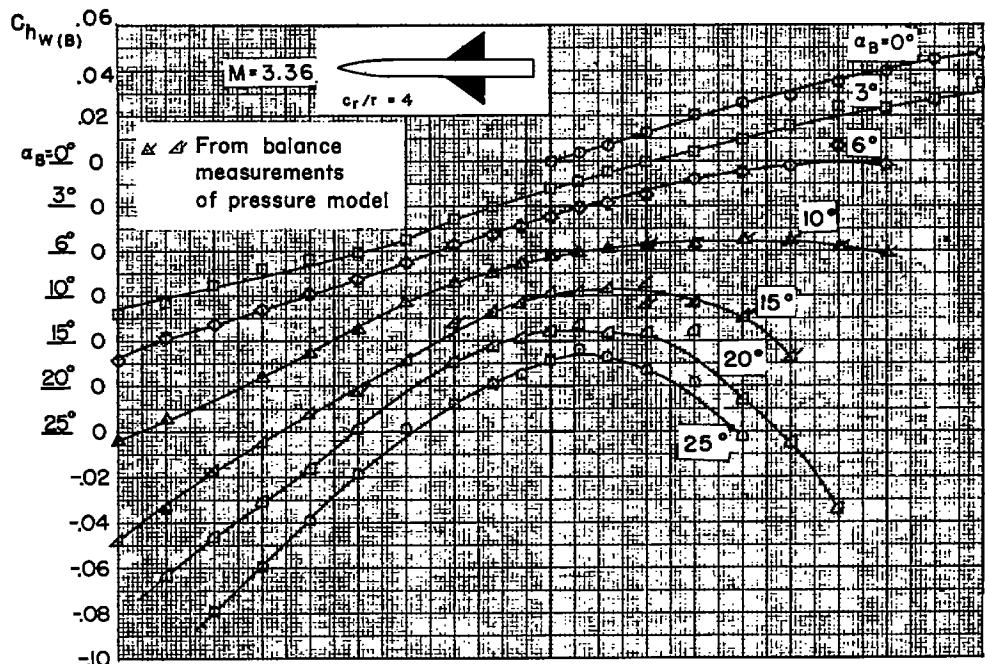
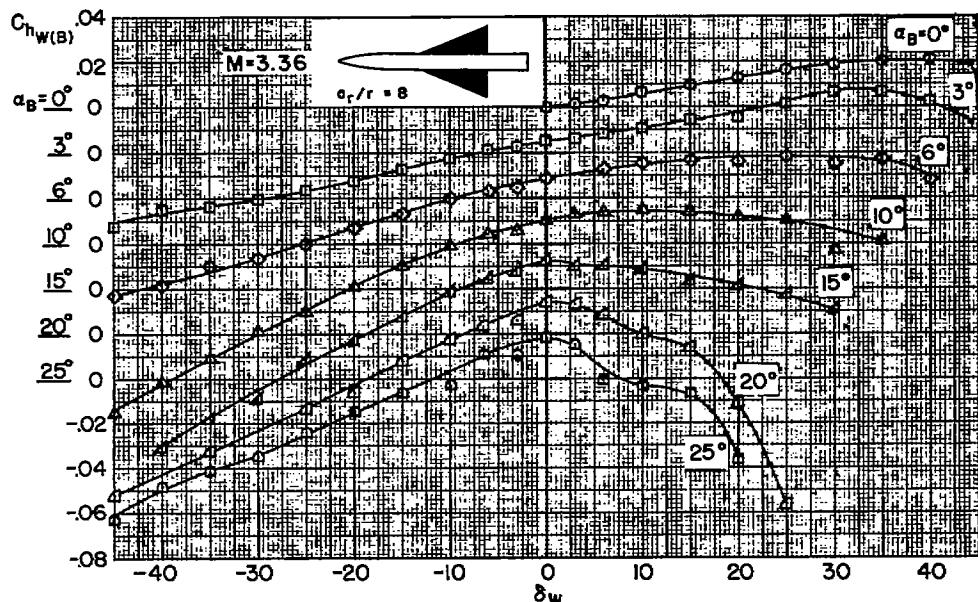
(a) $A = 4$ triangular wing, $r/s = 0.2$.(b) $A = 2$ triangular wing, $r/s = 0.2$.

Figure 5.- Variation with deflection angle of hinge-moment coefficient for the wings in the presence of the body.

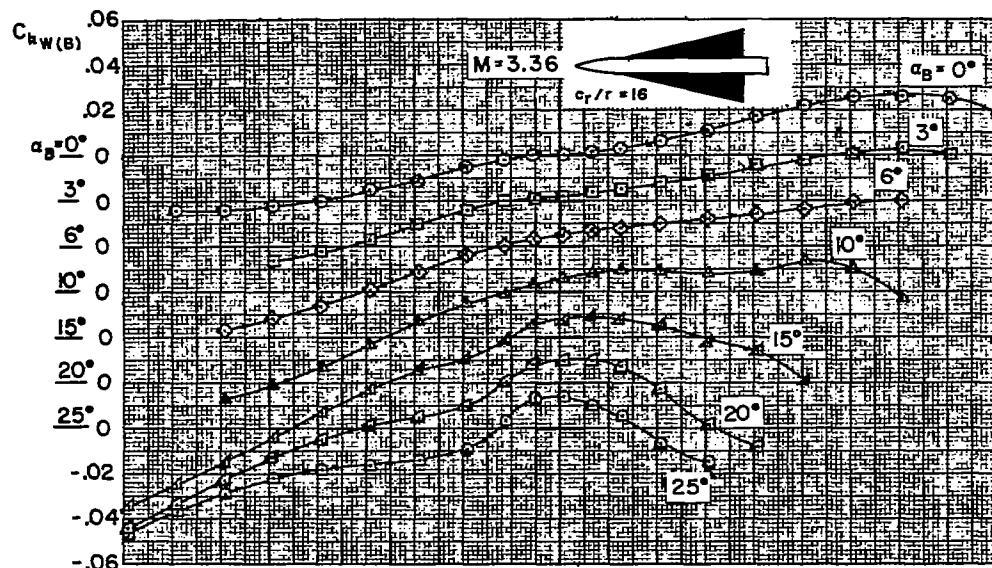
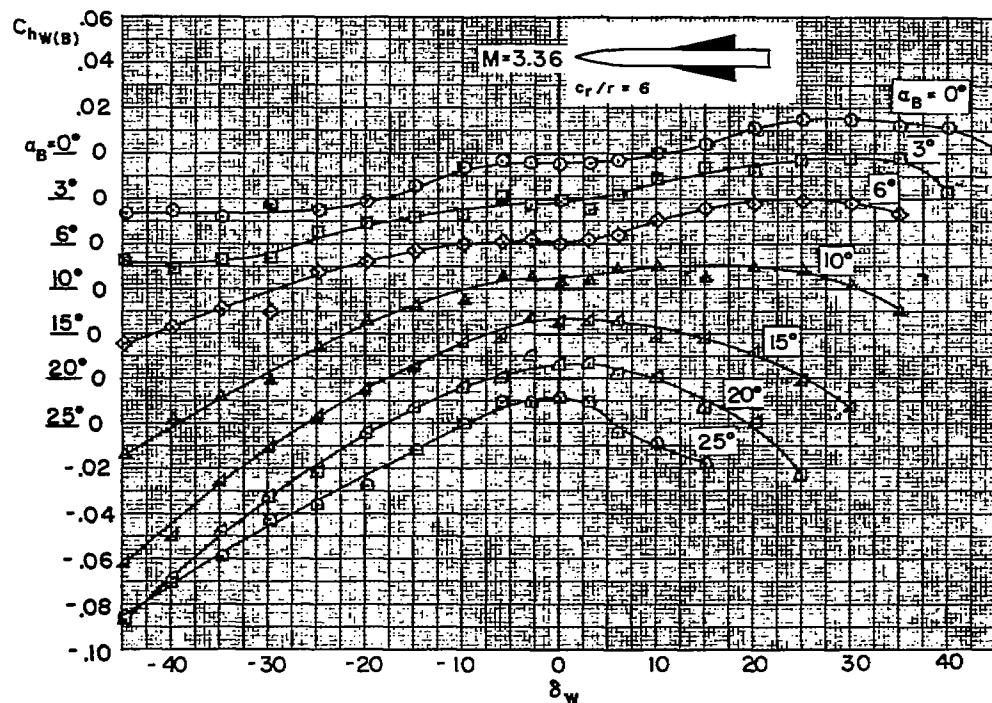
(c) $A = 1$ triangular wing, $r/s = 0.2$.(d) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 5.- Continued.

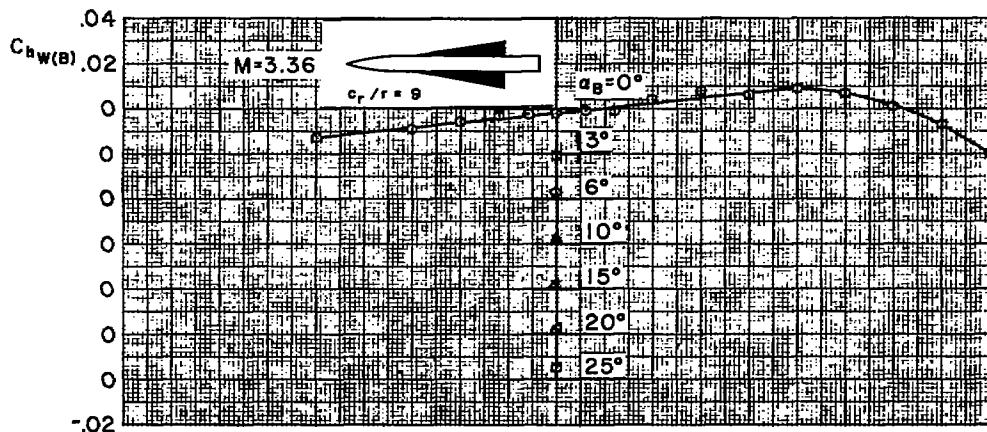
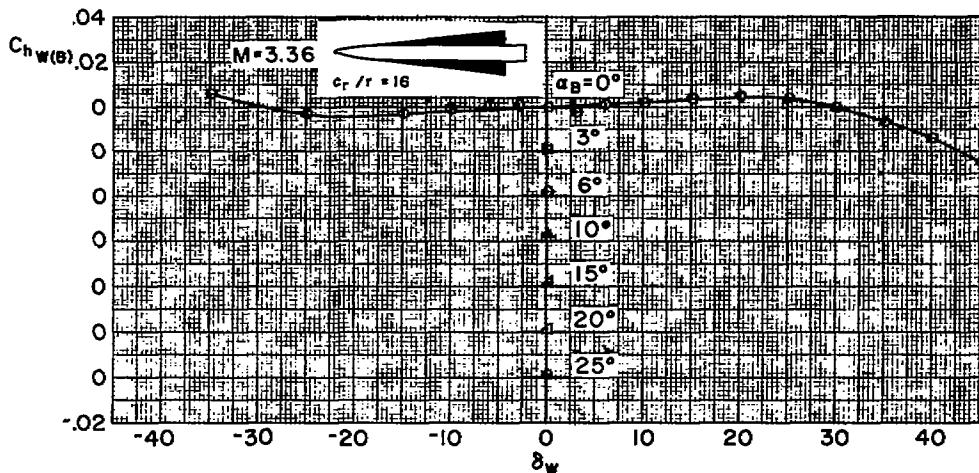
(e) $A = 2/3$ triangular wing, $r/s = 0.4$.(f) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 5.- Continued.

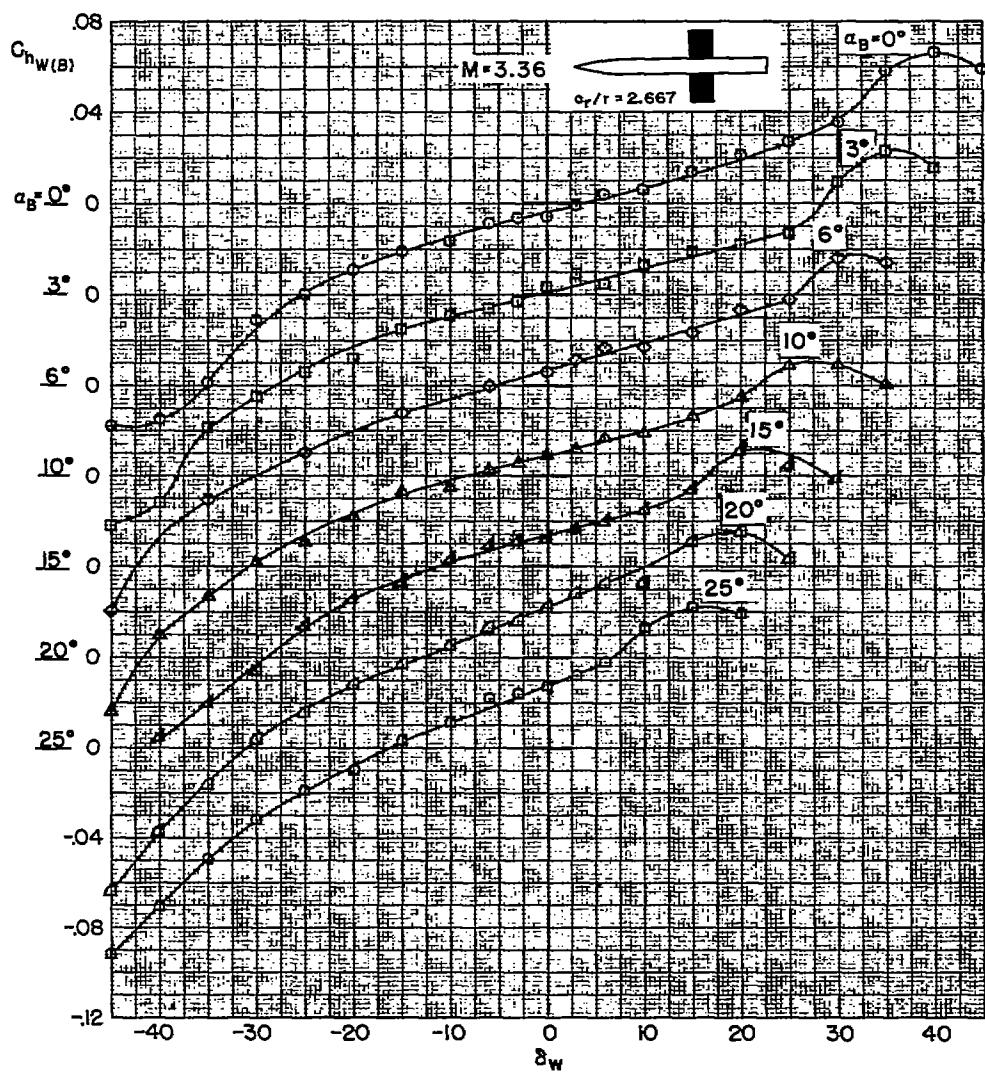
(g) $A = 3$ rectangular wing, $r/s = 0.2$.

Figure 5.- Continued.

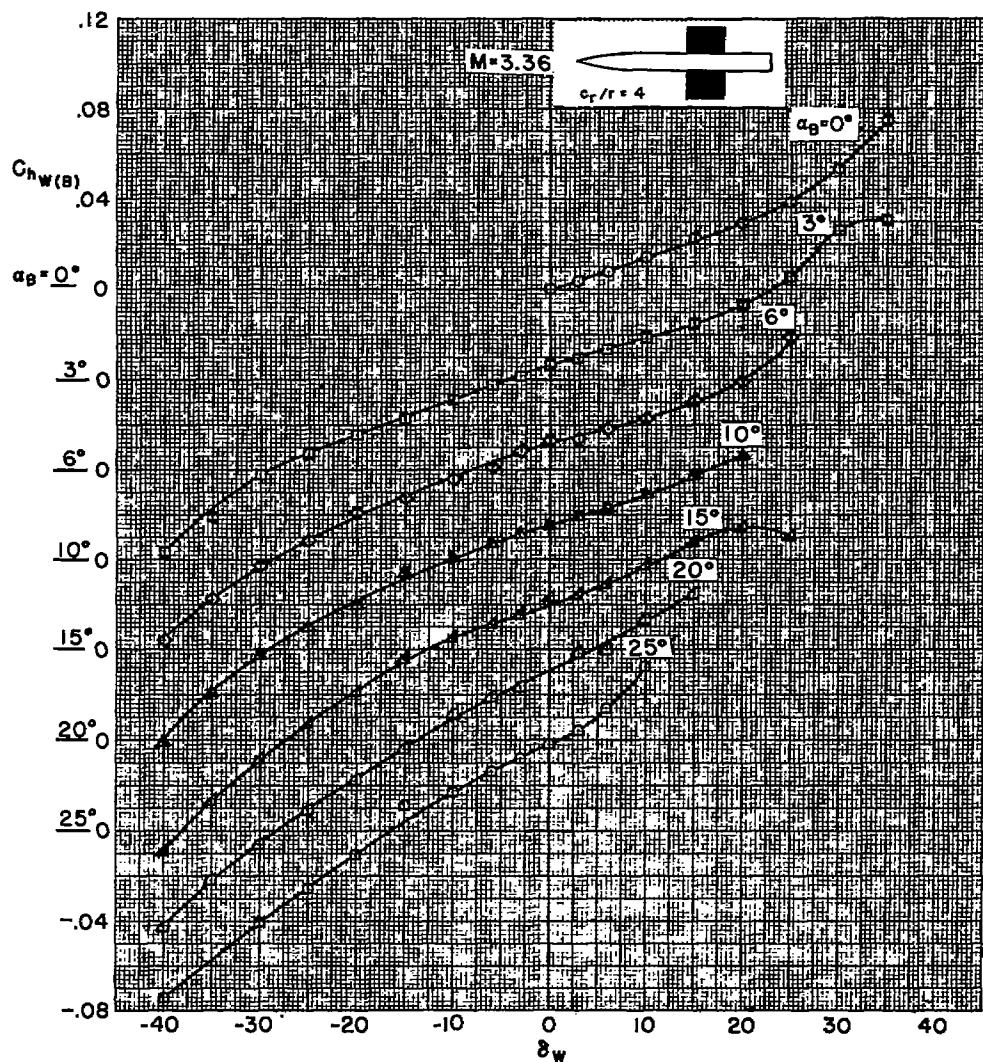
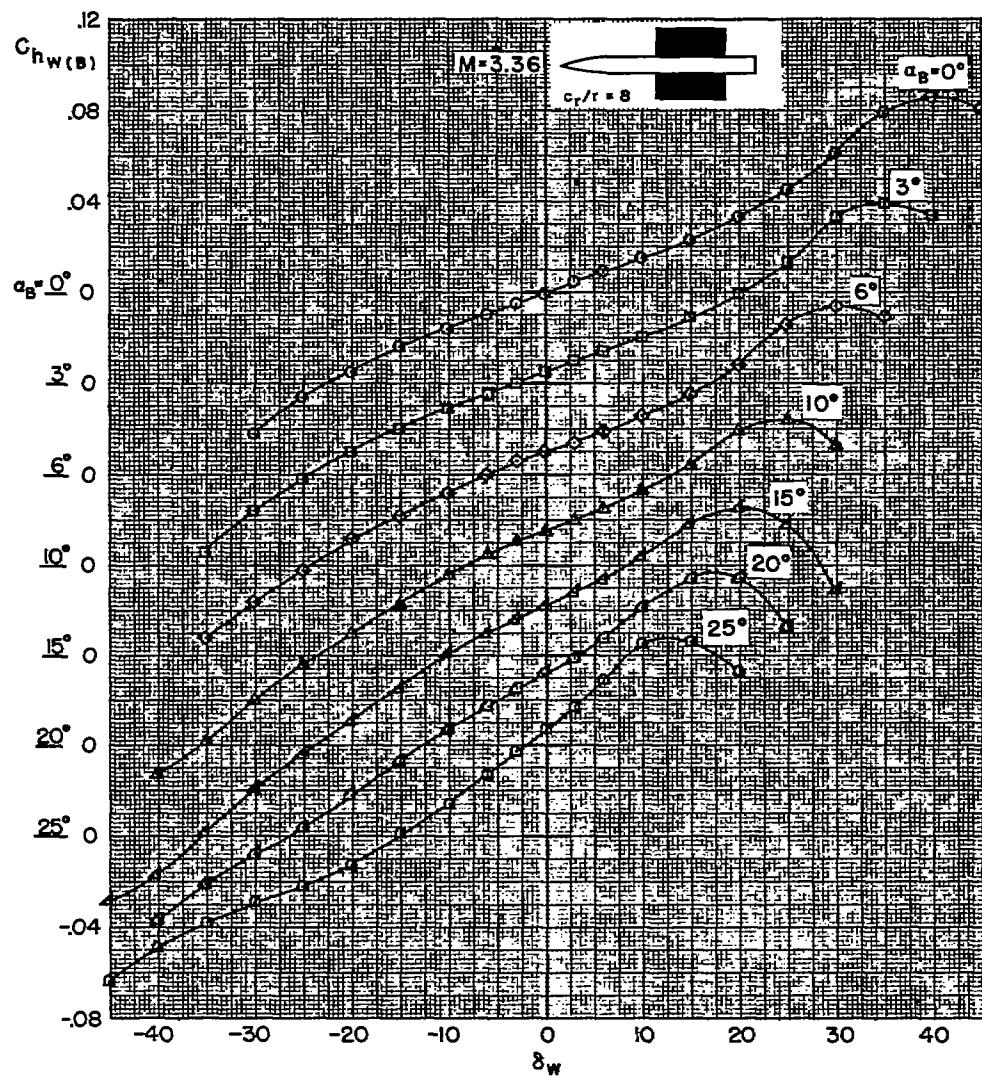
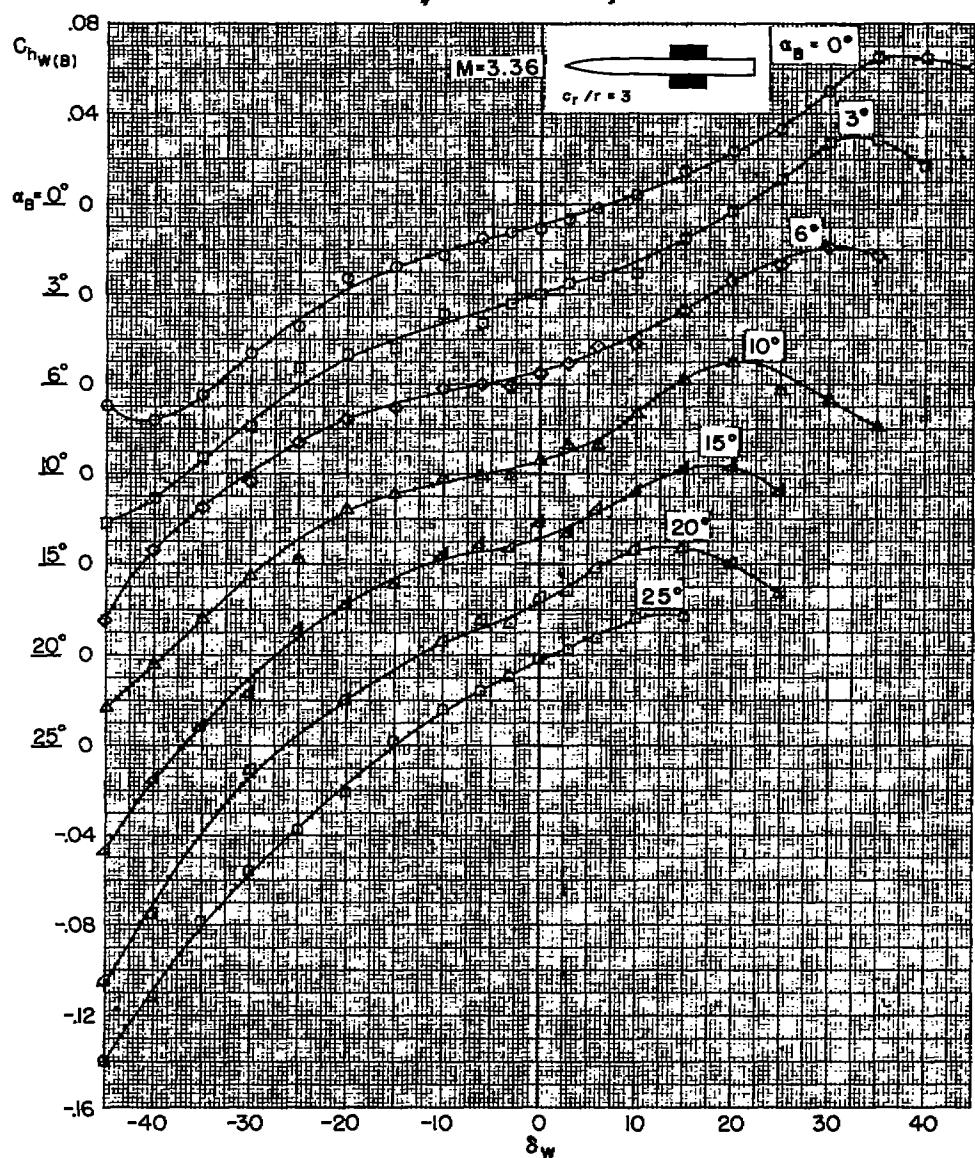
(h) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 5.- Continued.



(i) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 5.- Continued.



(j) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 5.- Concluded.

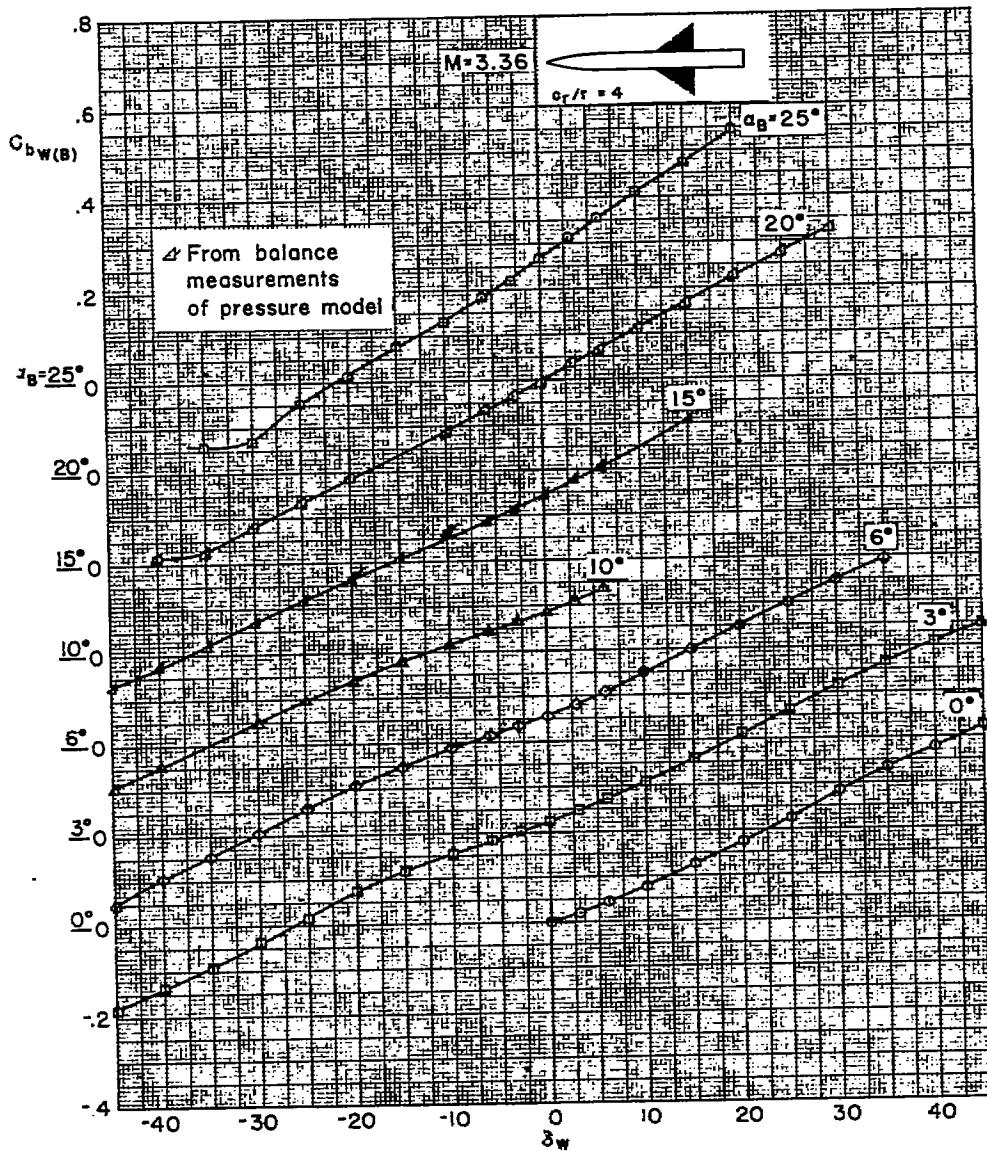
(a) $A = 4$ triangular wing, $r/s = 0.2$.

Figure 6.- Variation with deflection angle of bending-moment coefficient for the wings in the presence of the body.

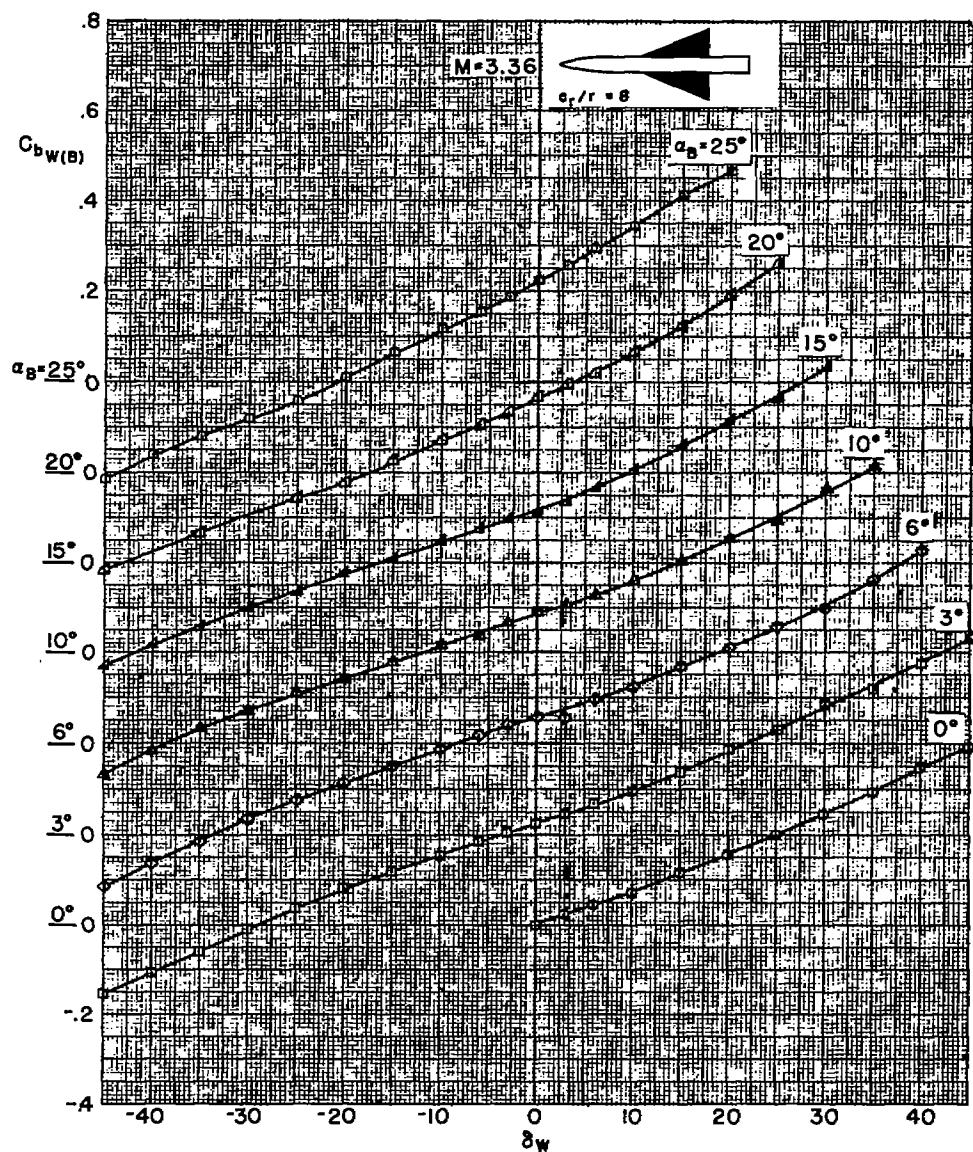
(b) $A = 2$ triangular wing, $r/s = 0.2$.

Figure 6.- Continued.

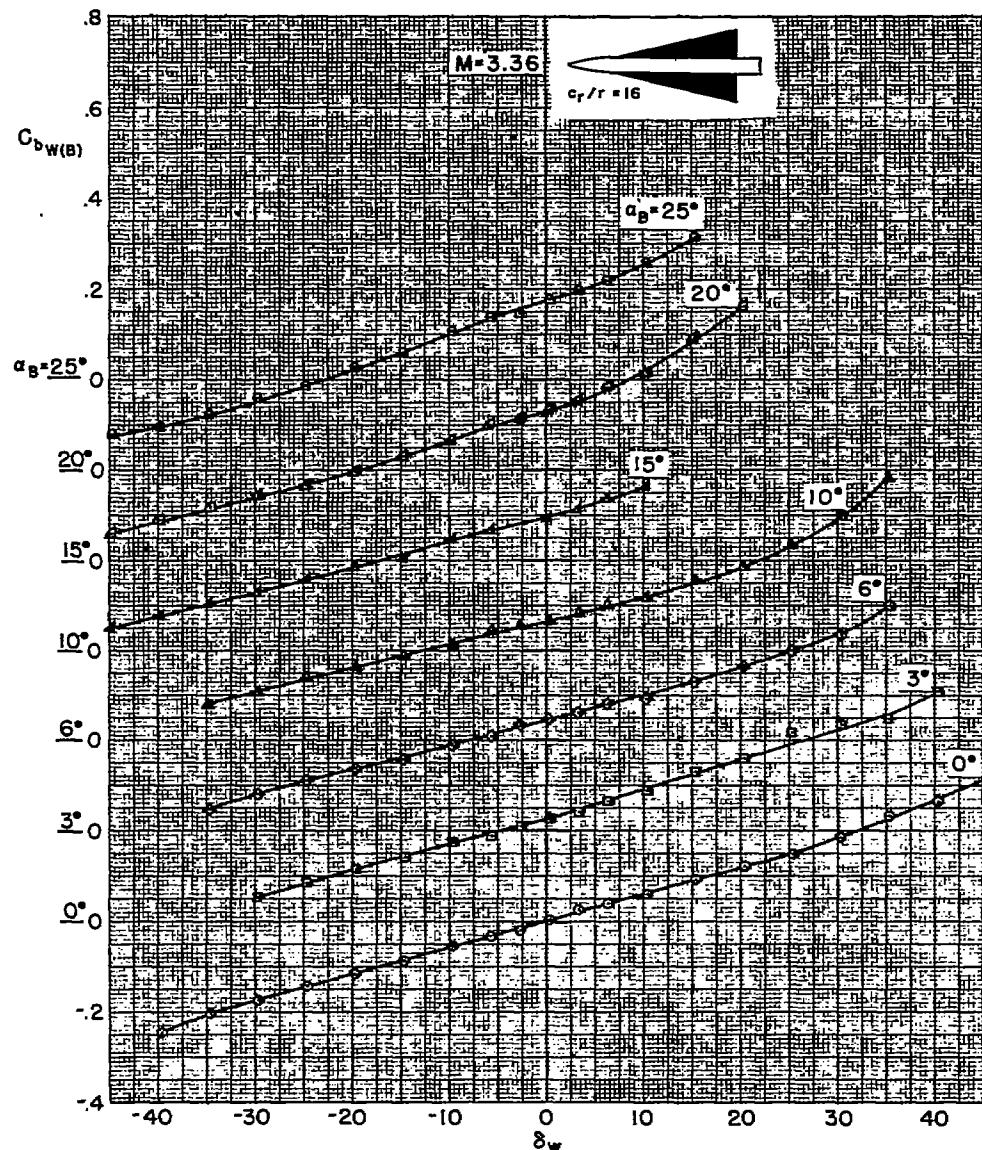
(c) $A = 1$ triangular wing, $r/s = 0.2$.

Figure 6.- Continued.

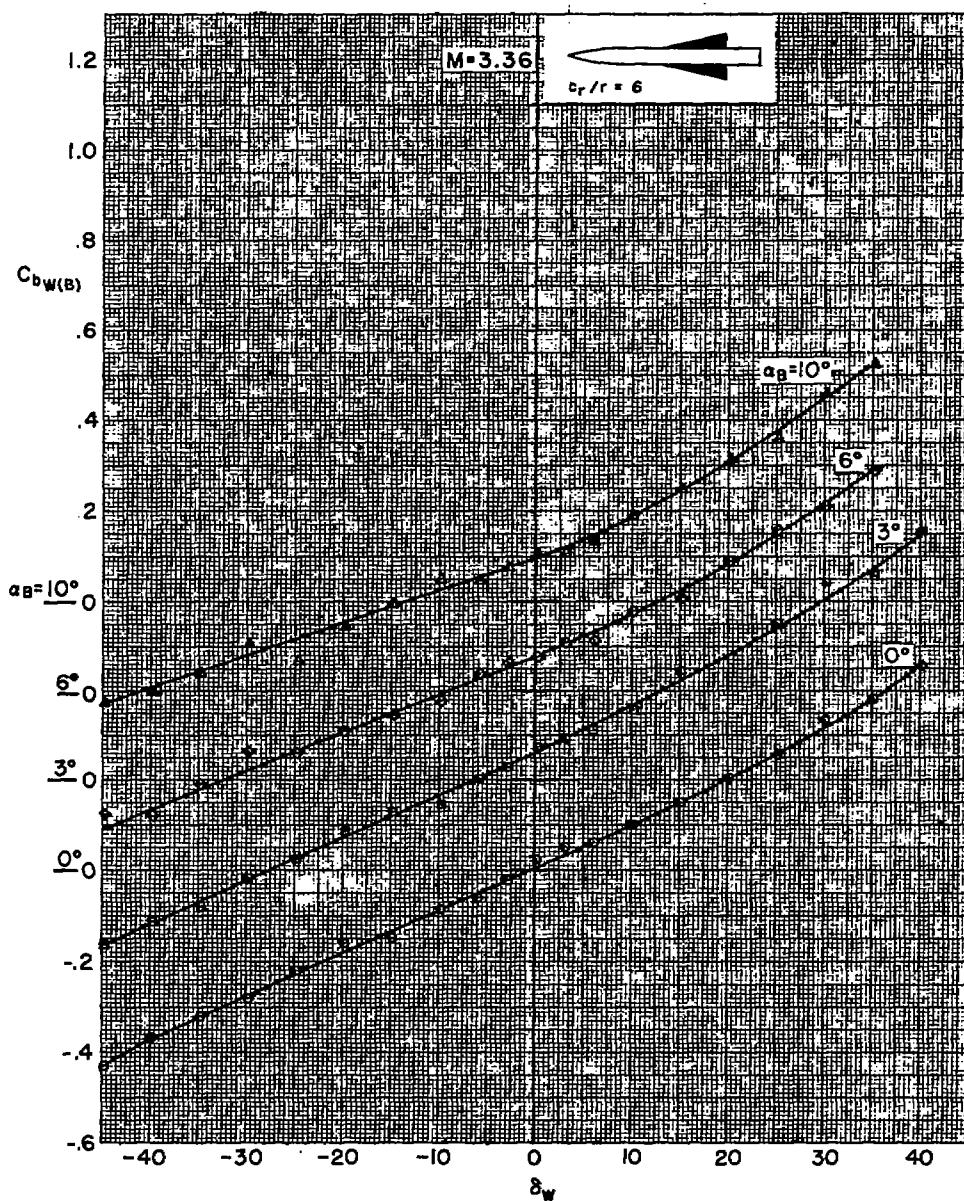
(d) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 6.- Continued.

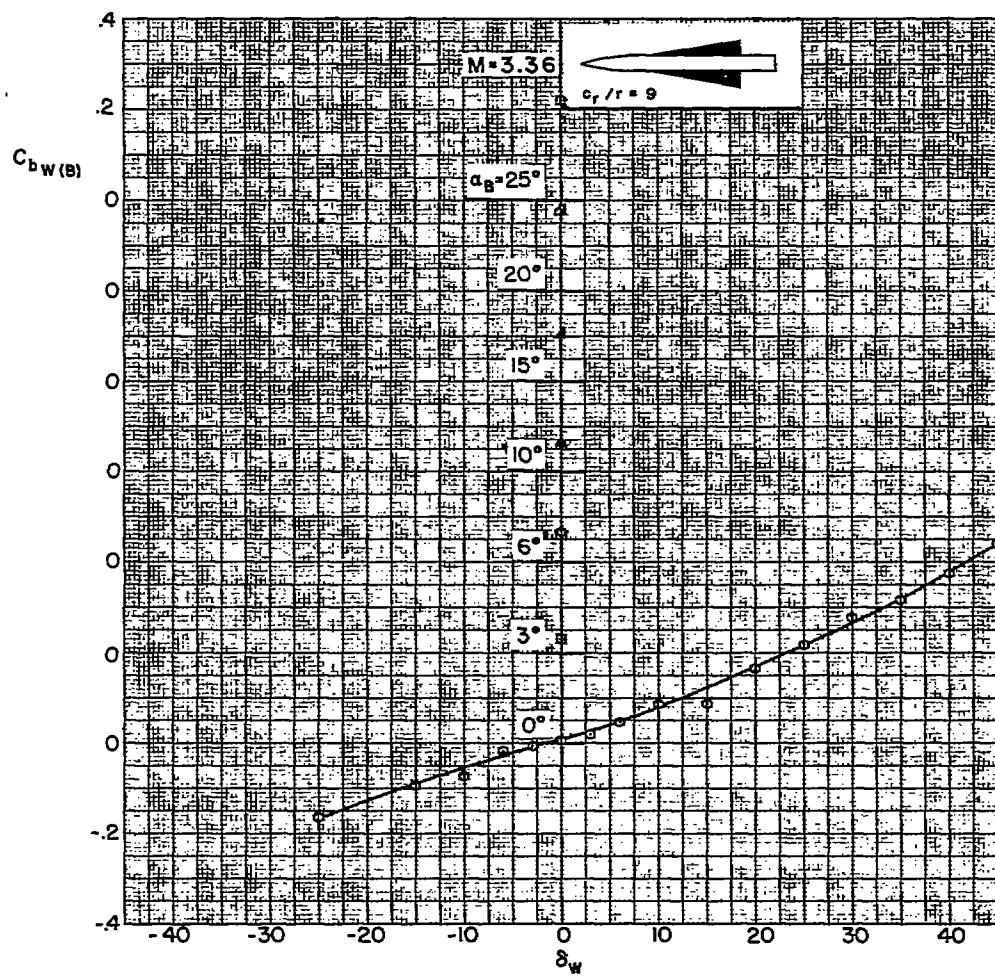
(e) $A = 2/3$ triangular wing, $r/s = 0.4$.

Figure 6.- Continued.

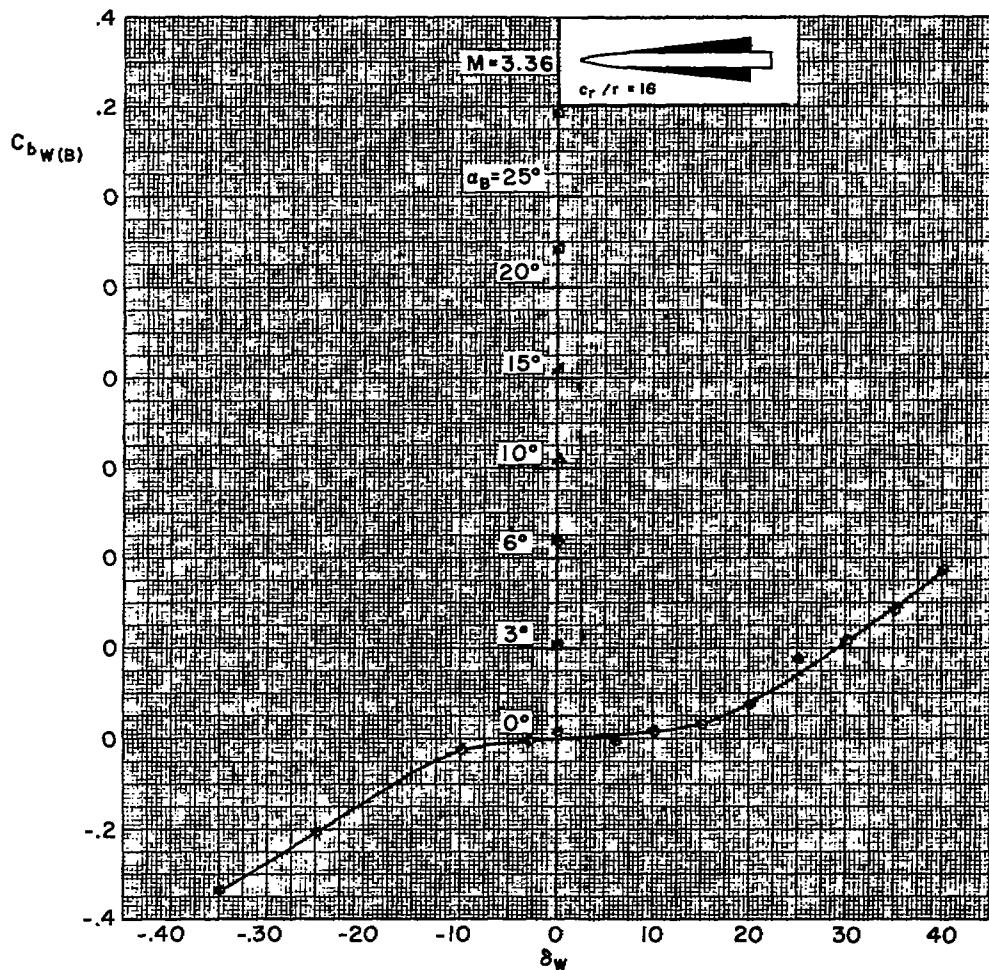
(f) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 6.- Continued.

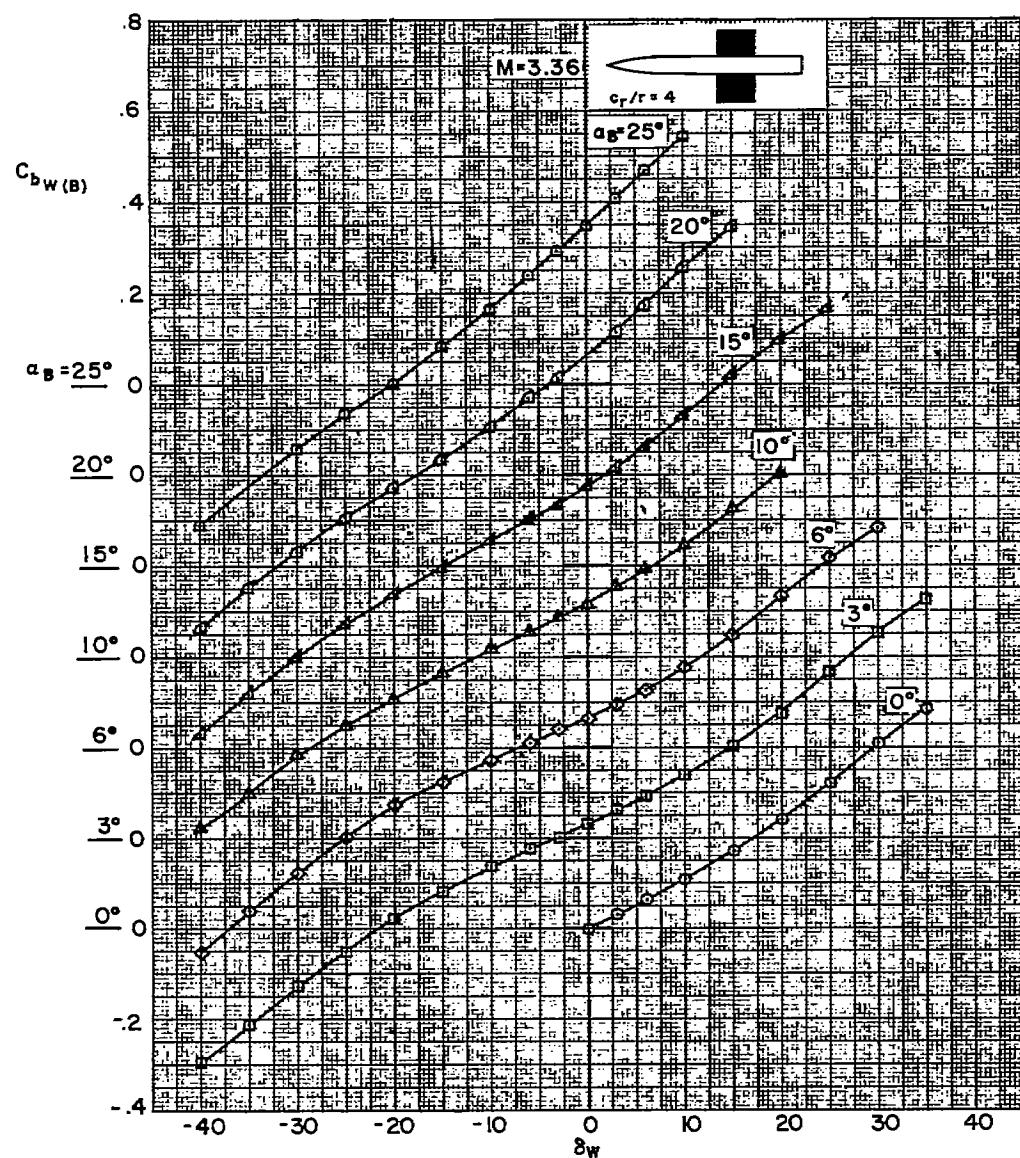
(g) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 6.- Continued.

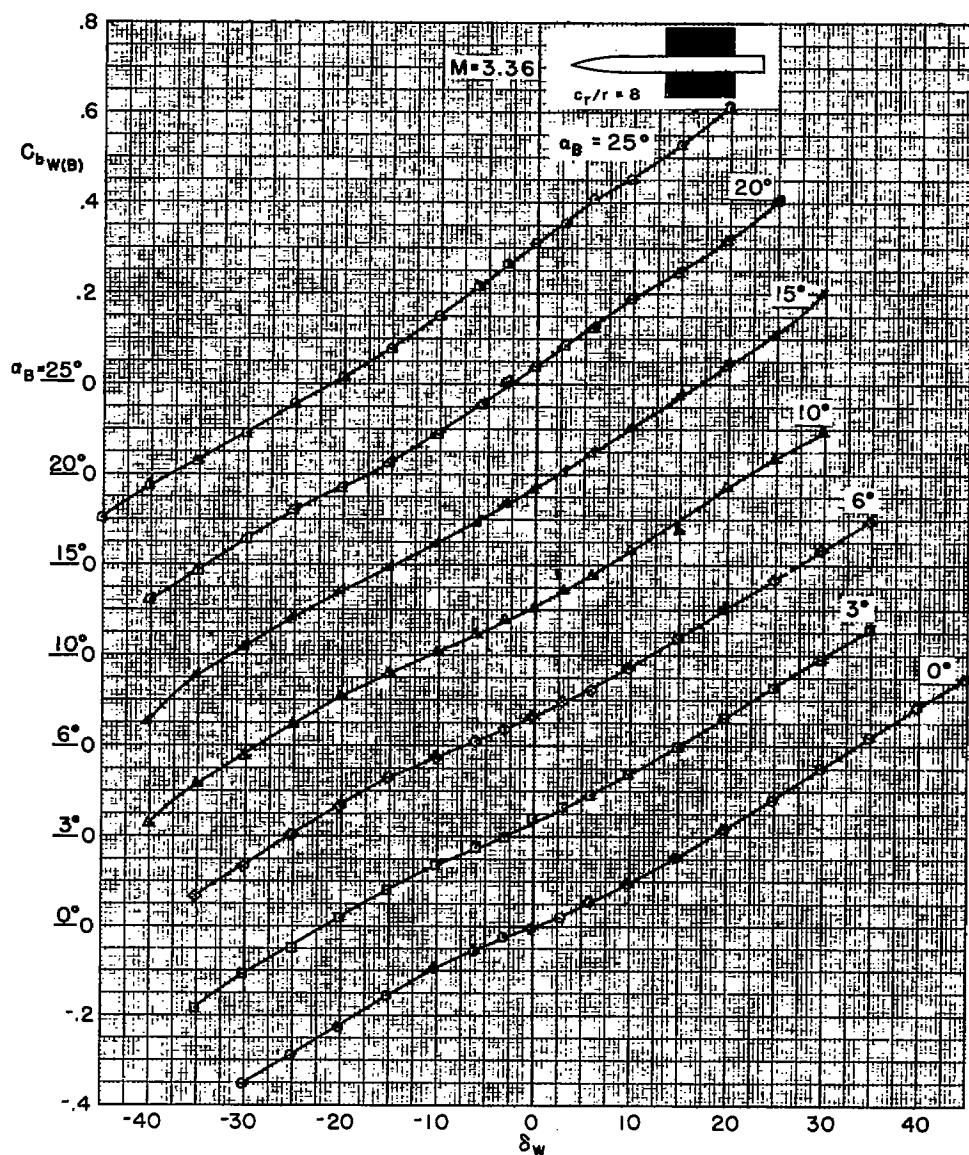
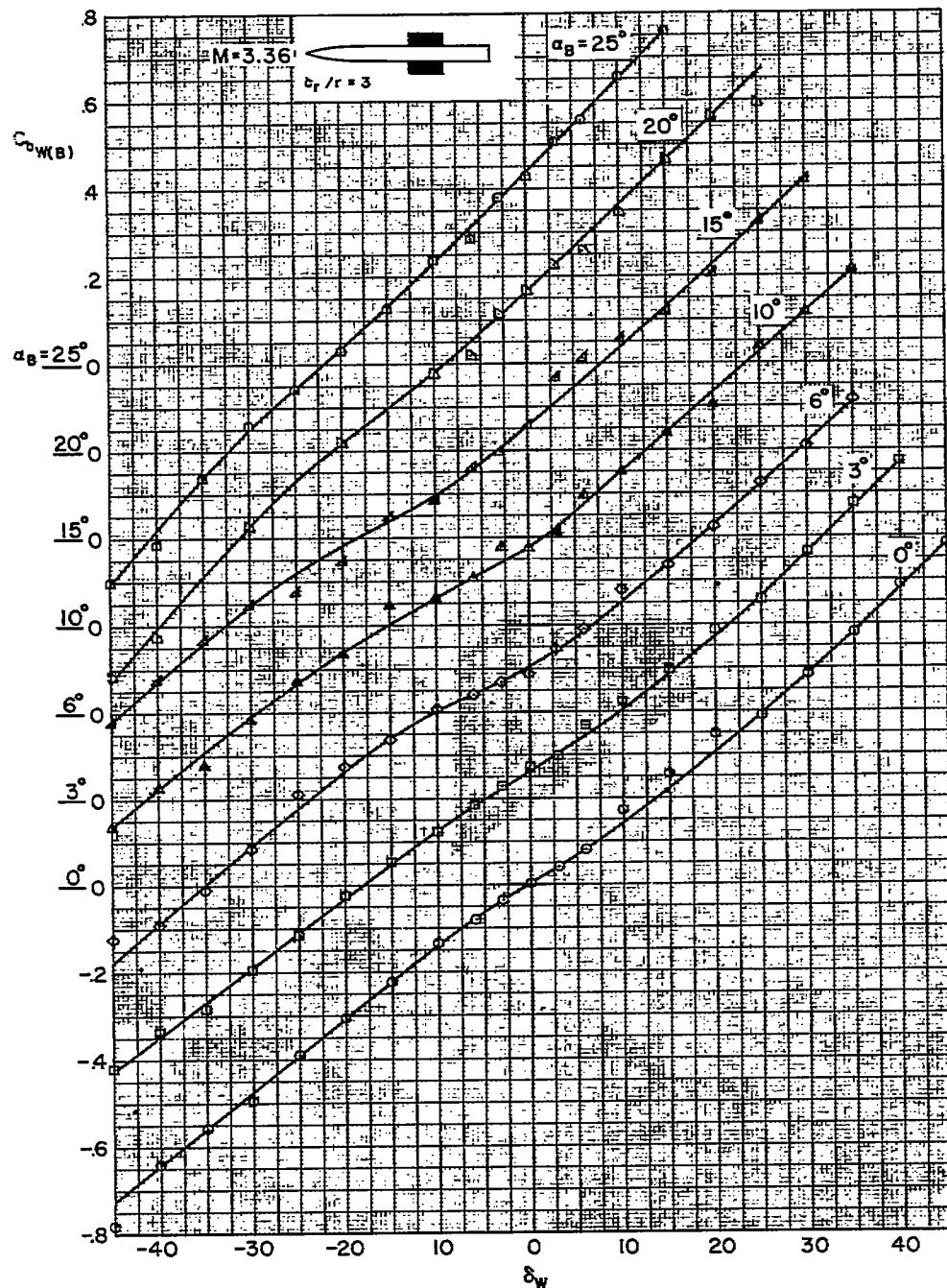
(h) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 6--Continued.



(i) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 6.- Concluded.

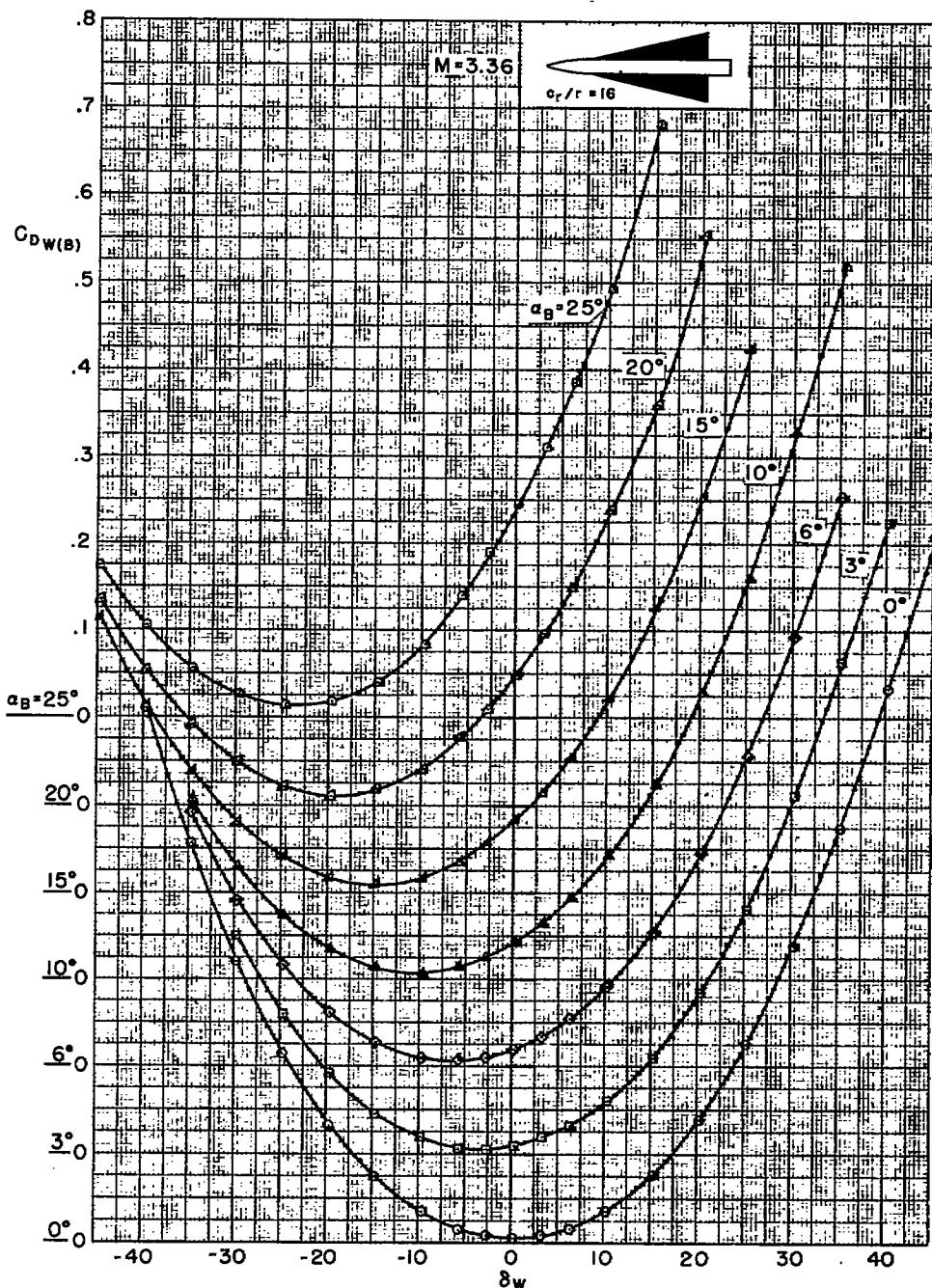
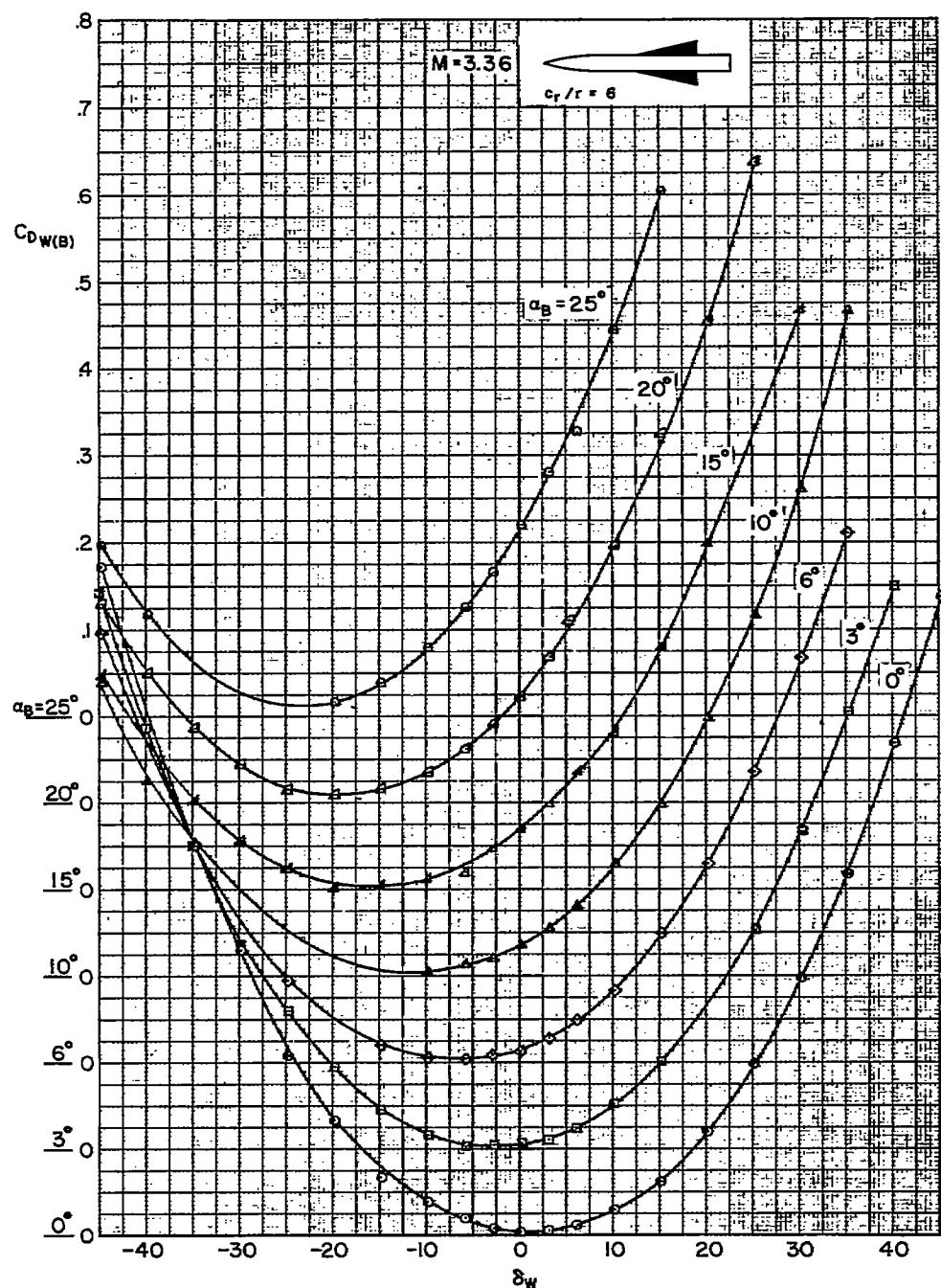
(a) $A = 1$ triangular wing, $r/s = 0.2$.

Figure 7.- Variation with deflection angle of drag coefficient for the wings in the presence of the body.



(b) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 7.- Continued.

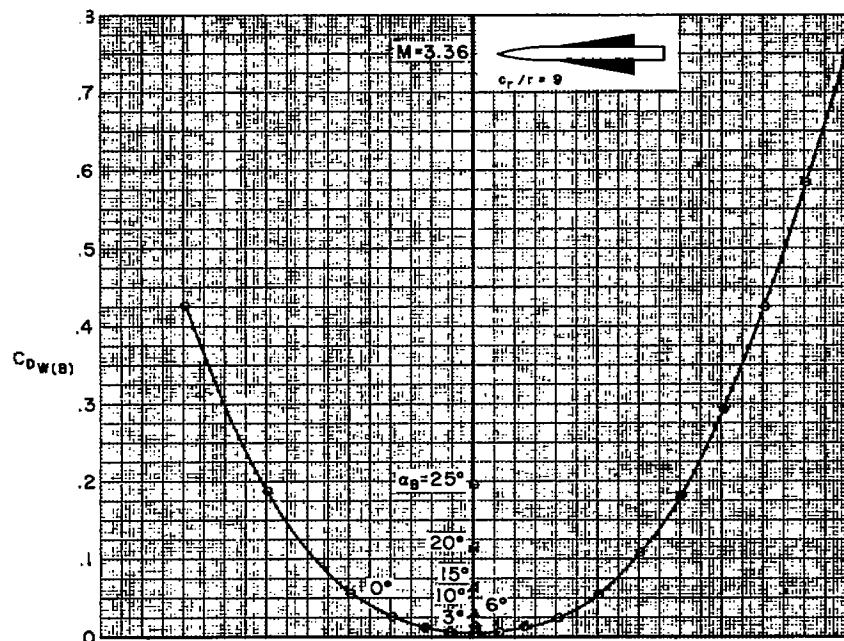
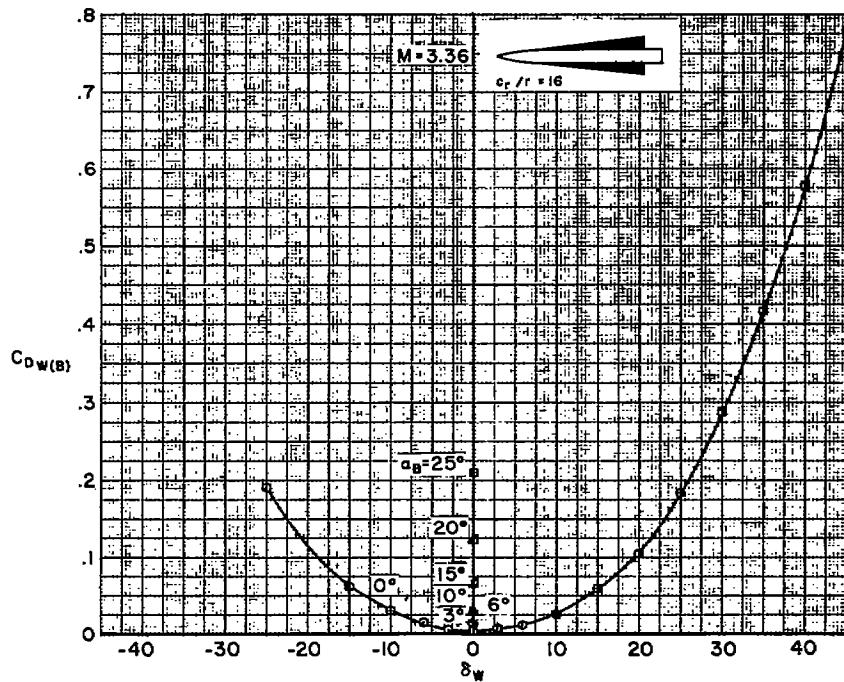
(c) $A = 2/3$ triangular wing, $r/s = 0.4$.(d) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 7.- Continued.

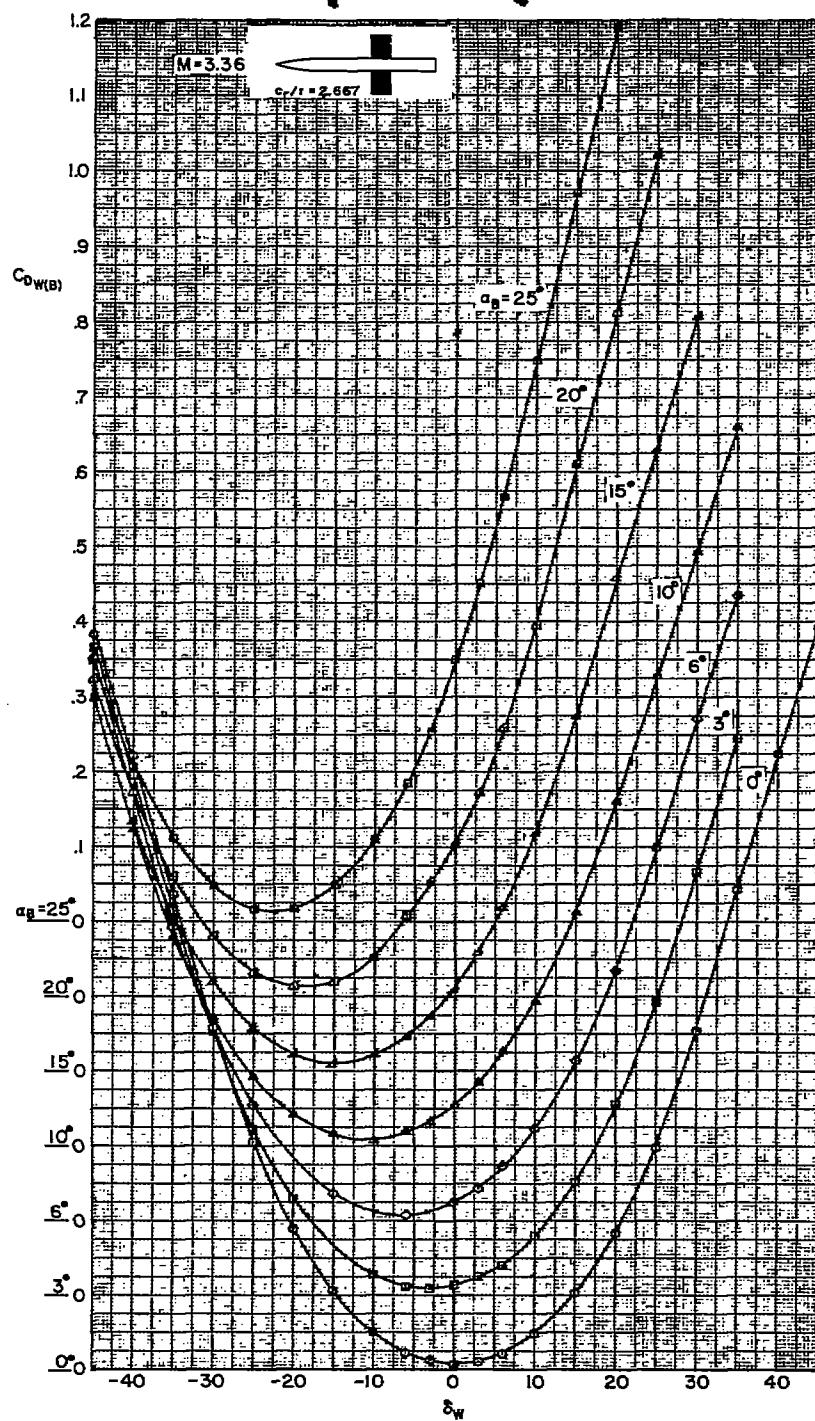
(e) $A = 3$ rectangular wing, $r/s = 0.2$.

Figure 7.- Continued.

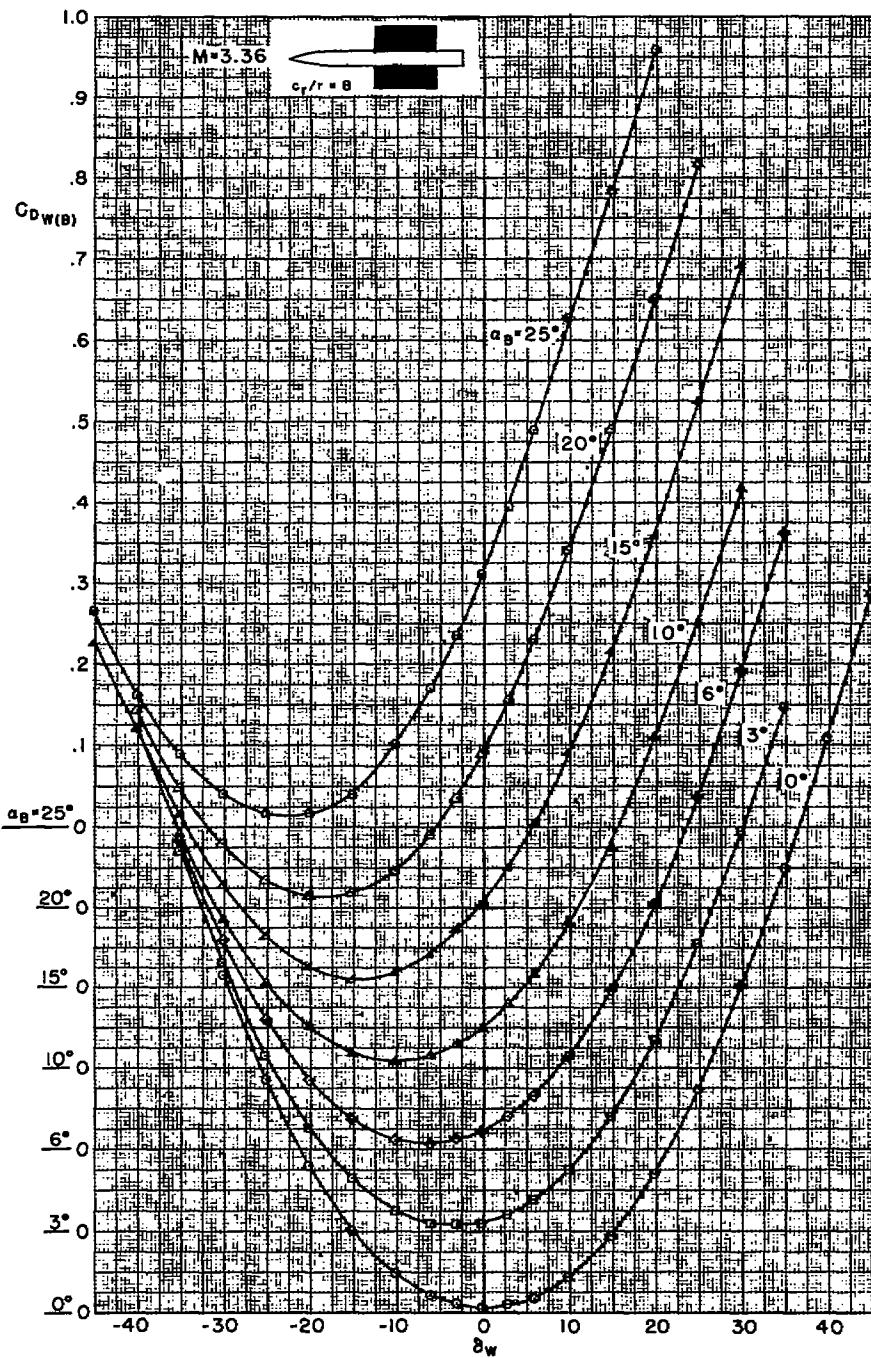
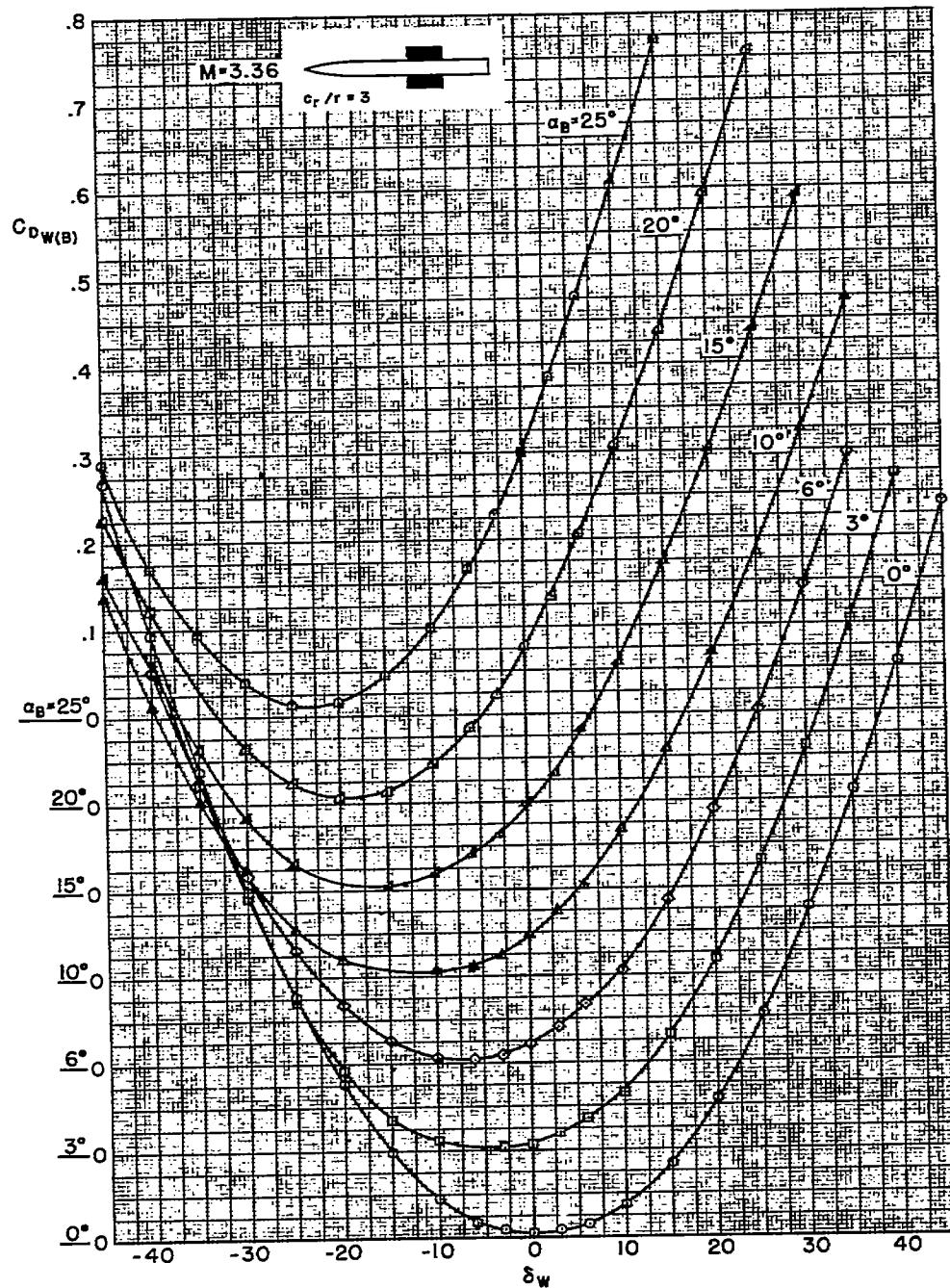
(f) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 7.- Continued.



(g) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 7.- Concluded.

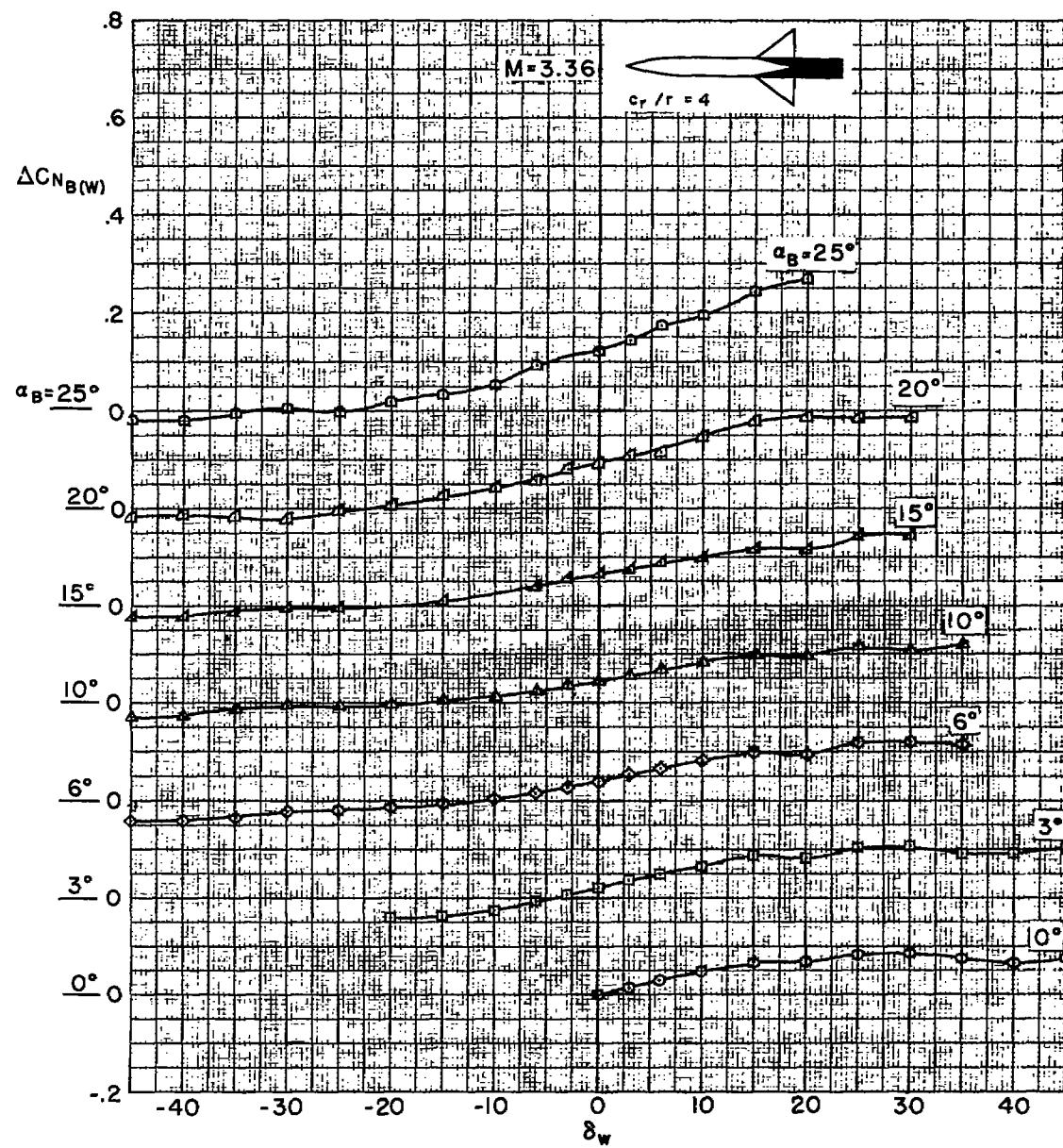
(a) $A = 4$ triangular wing, $r/s = 0.2$.

Figure 8.- Variation with deflection angle of interference normal-force coefficient for the body in the presence of the wings.

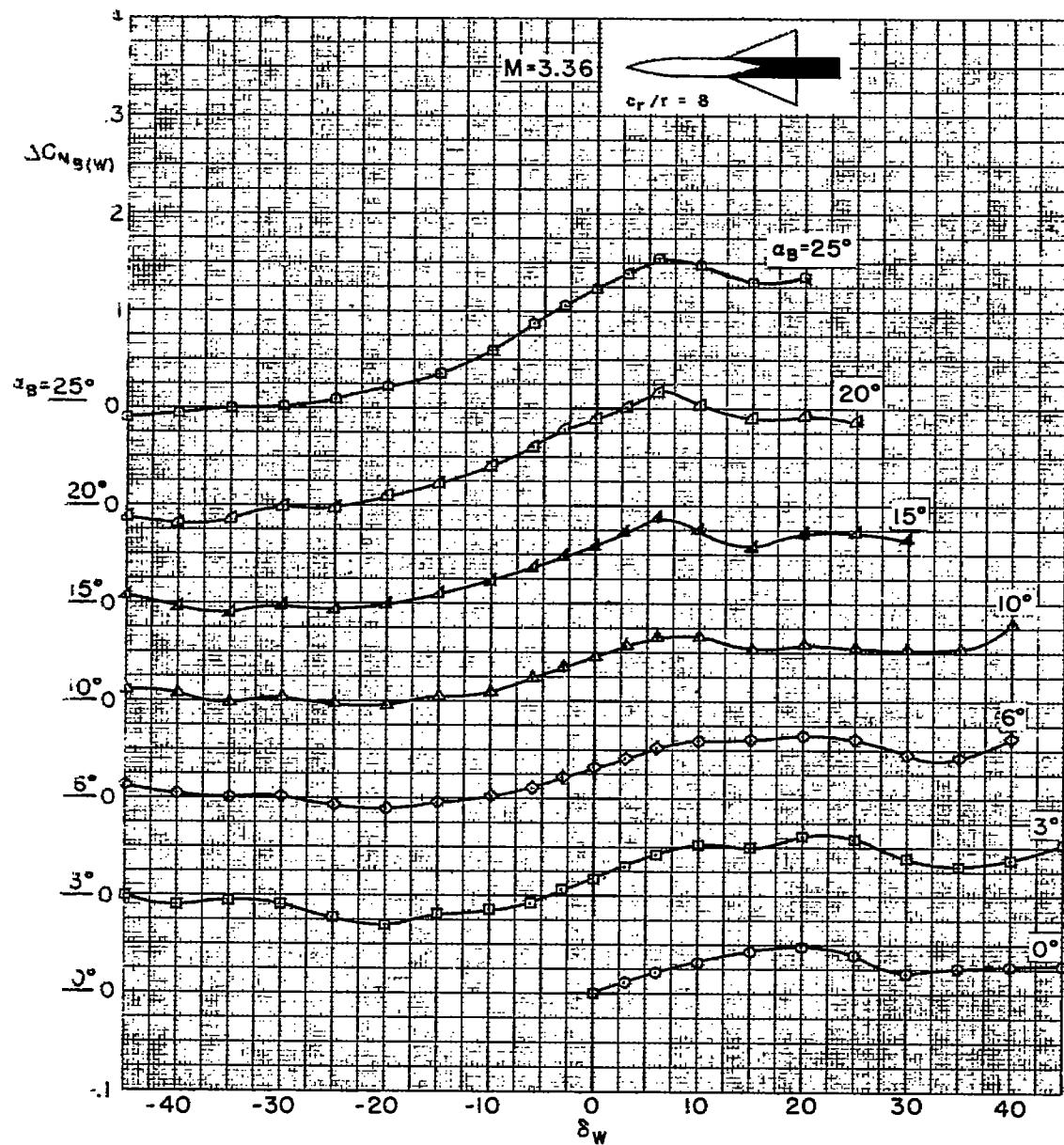
(b) $A = 2$ triangular wing, $r/s = 0.2$.

Figure 8.- Continued.

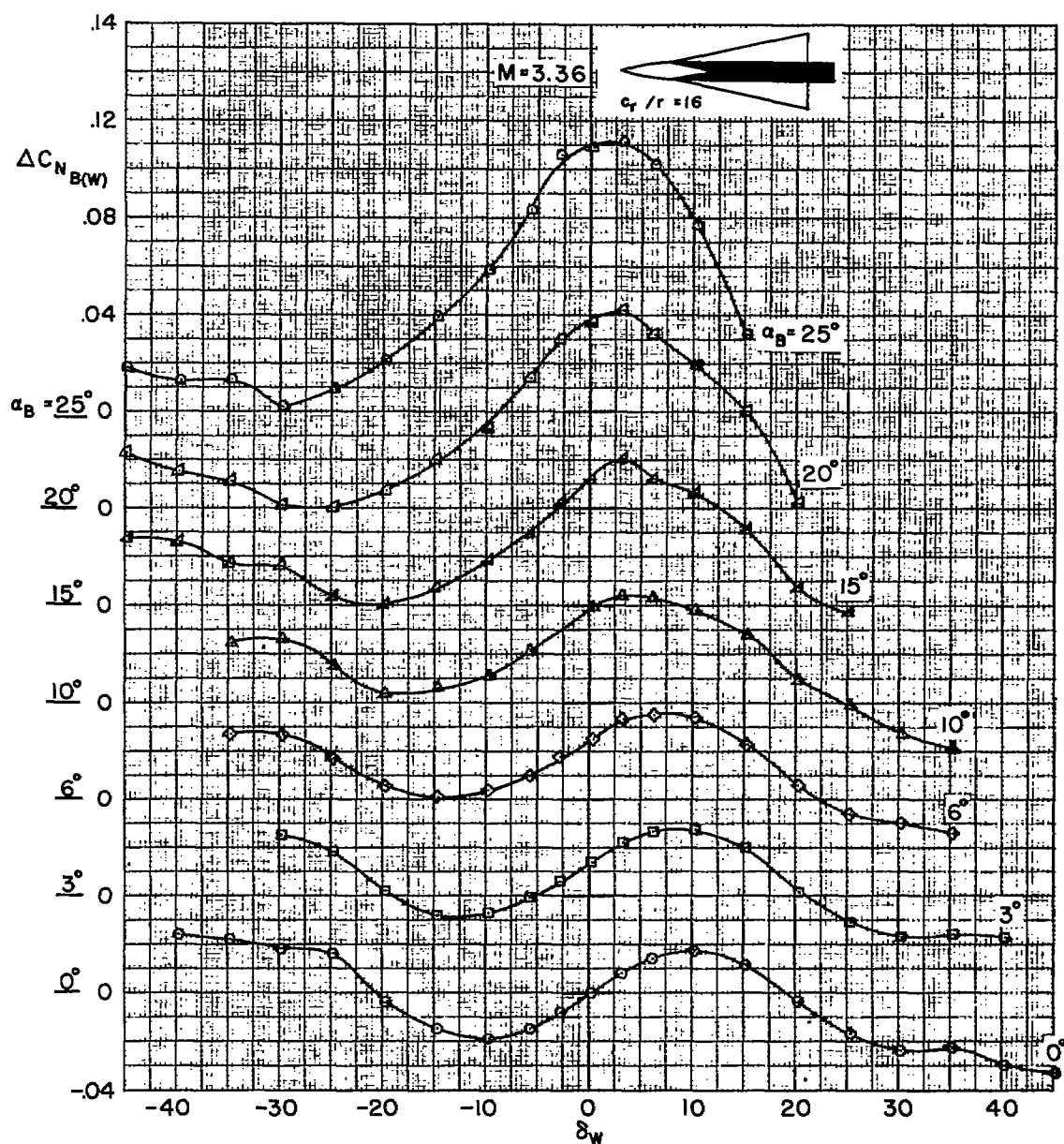
(c) $A = 1$ triangular wing, $r/s = 0.2$.

Figure 8.- Continued.

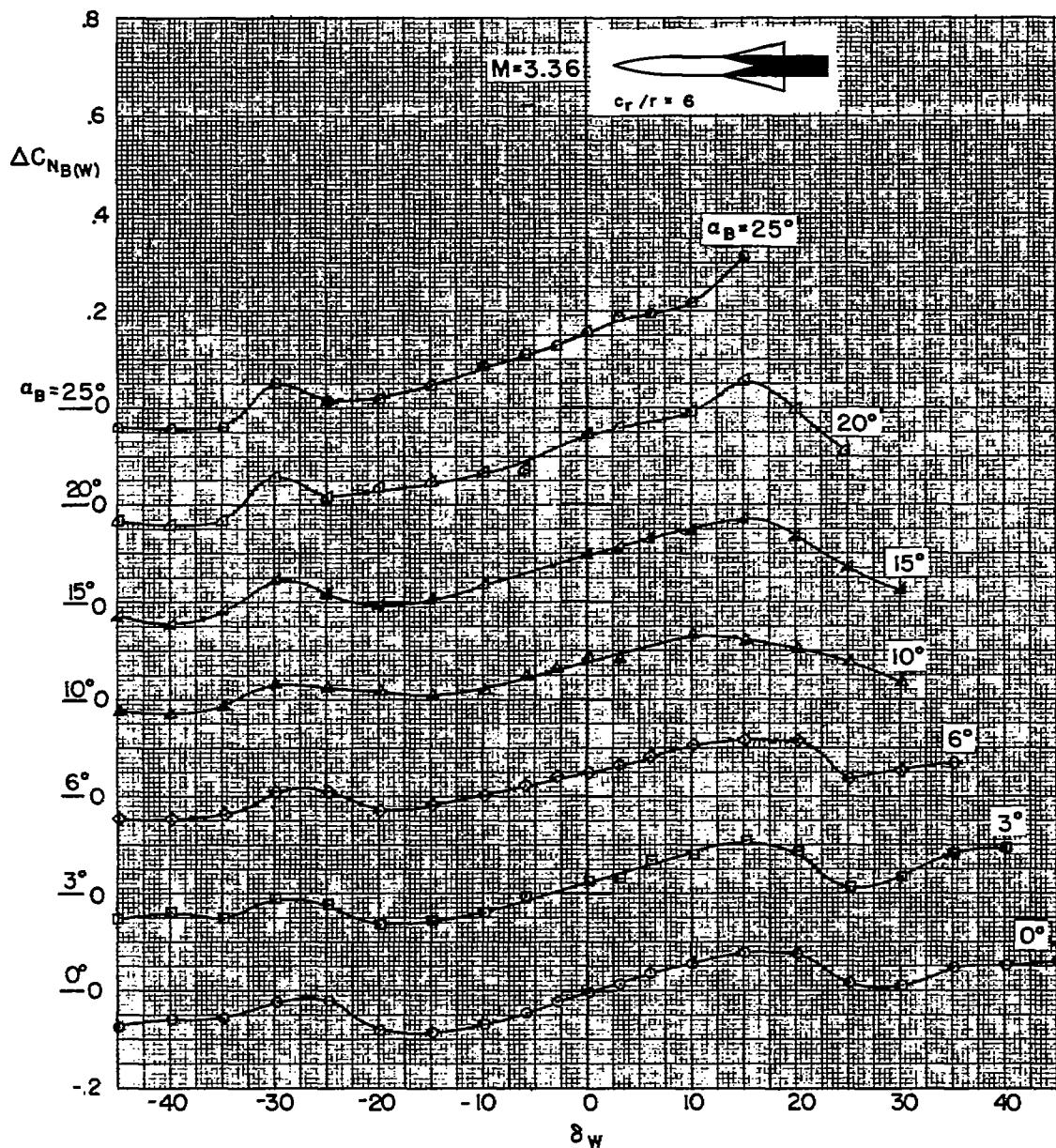
(d) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 8.- Continued.

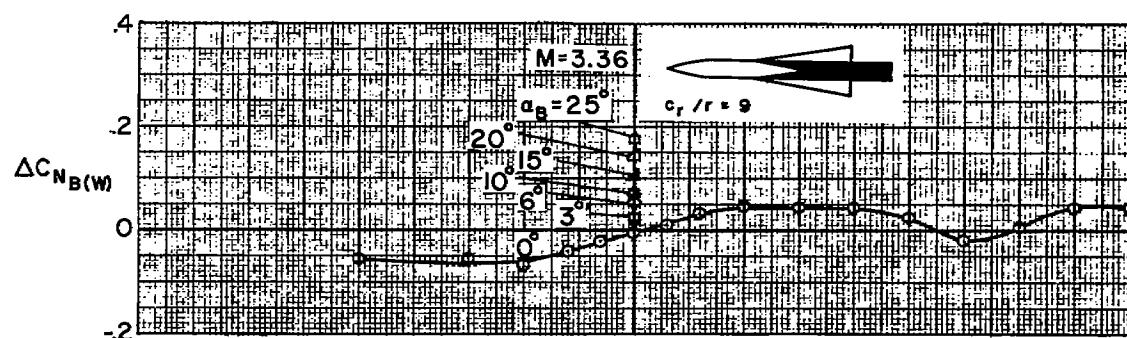
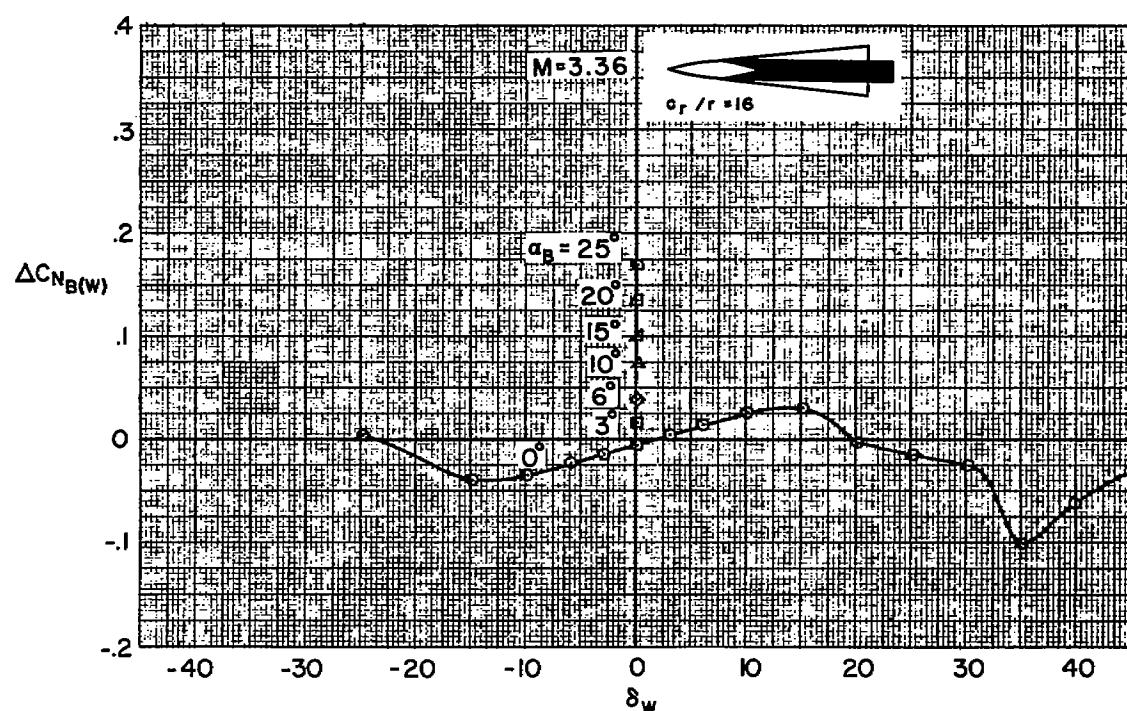
(e) $A = 2/3$ triangular wing, $r/s = 0.4$.(f) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 8.- Continued.

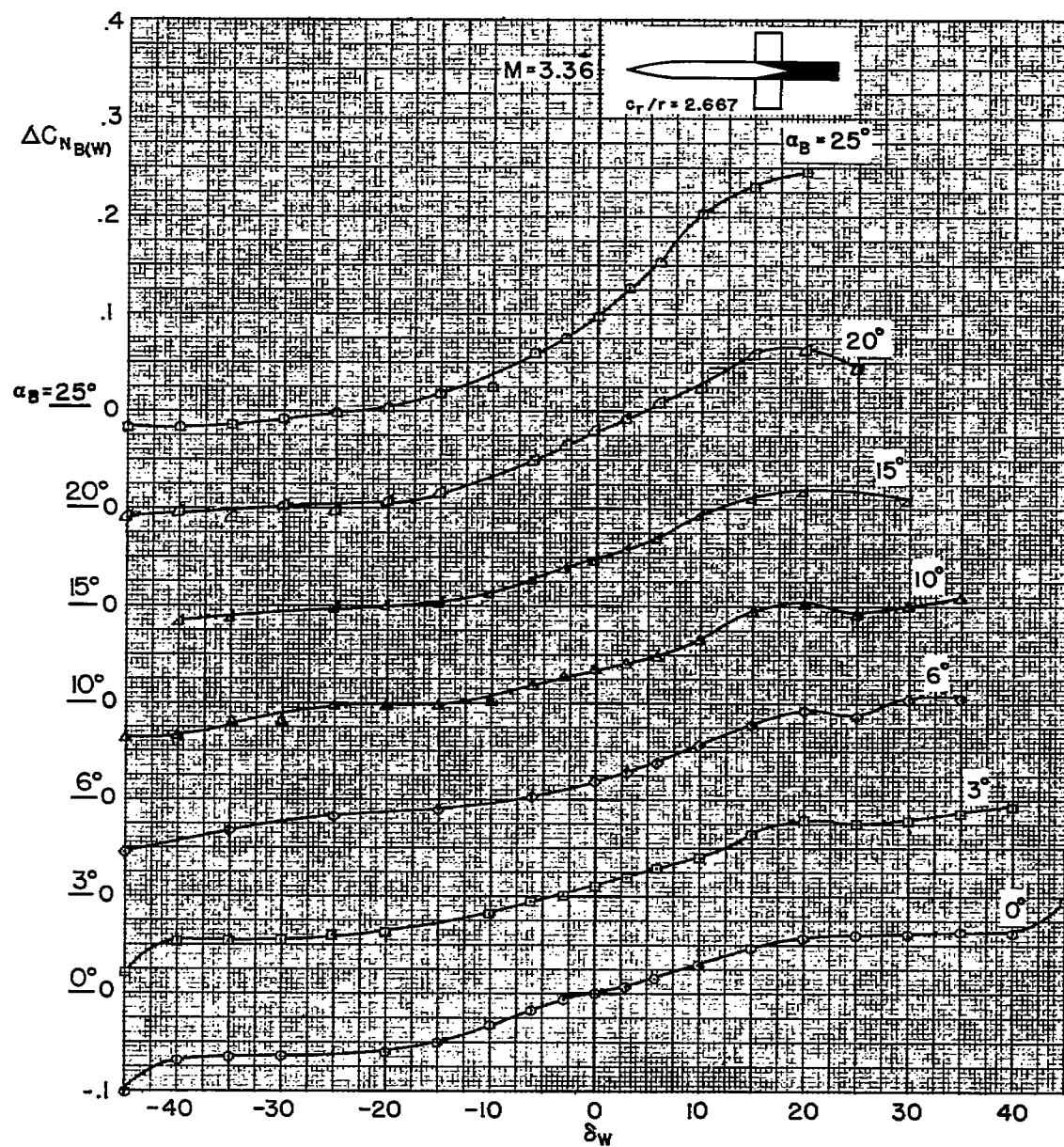
(g) $A = 3$ rectangular wing, $r/s = 0.2$.

Figure 8.- Continued.

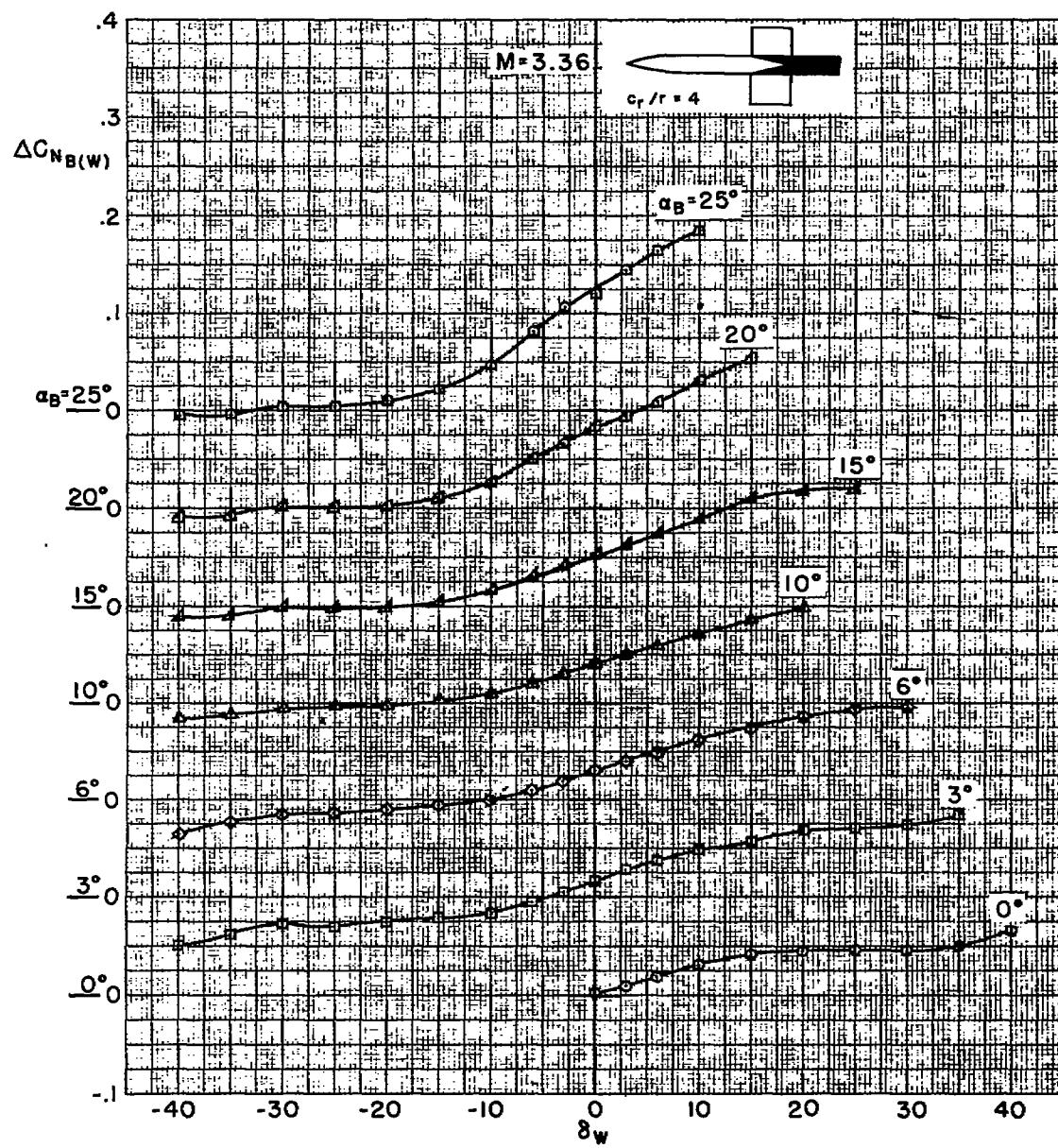
(h) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 8.- Continued.

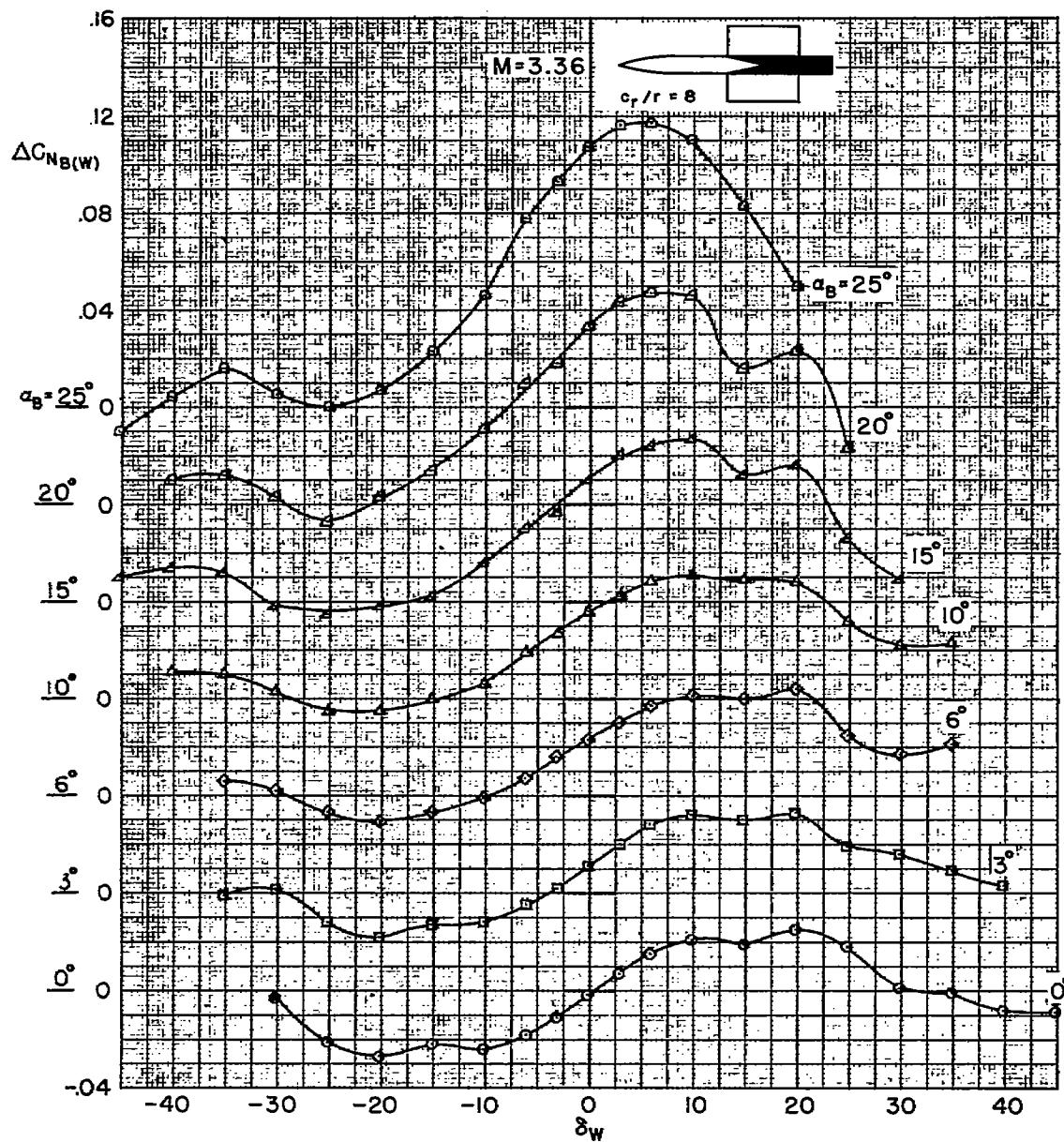
(i) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 8.- Continued.

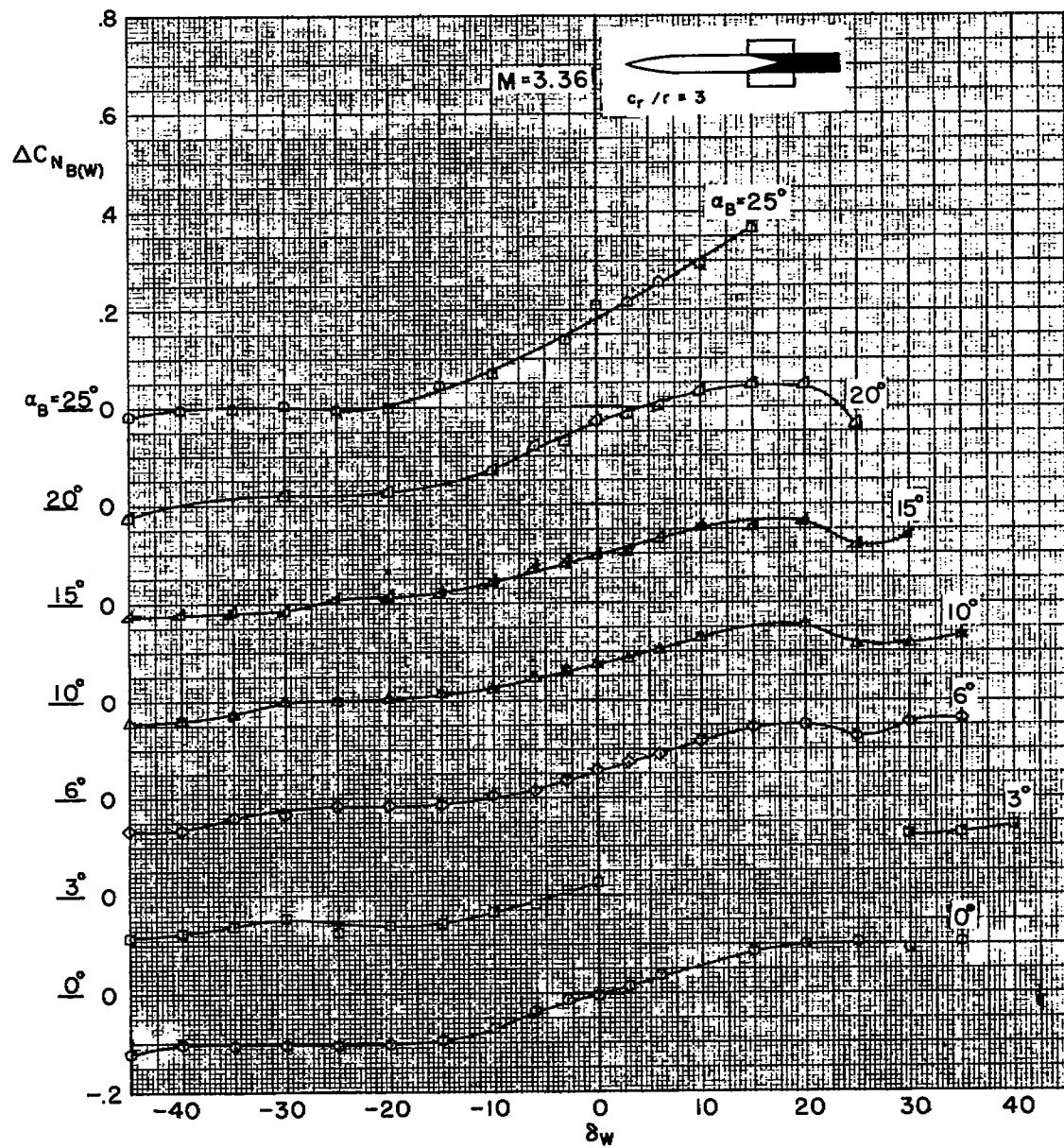
(j) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 8.- Concluded.

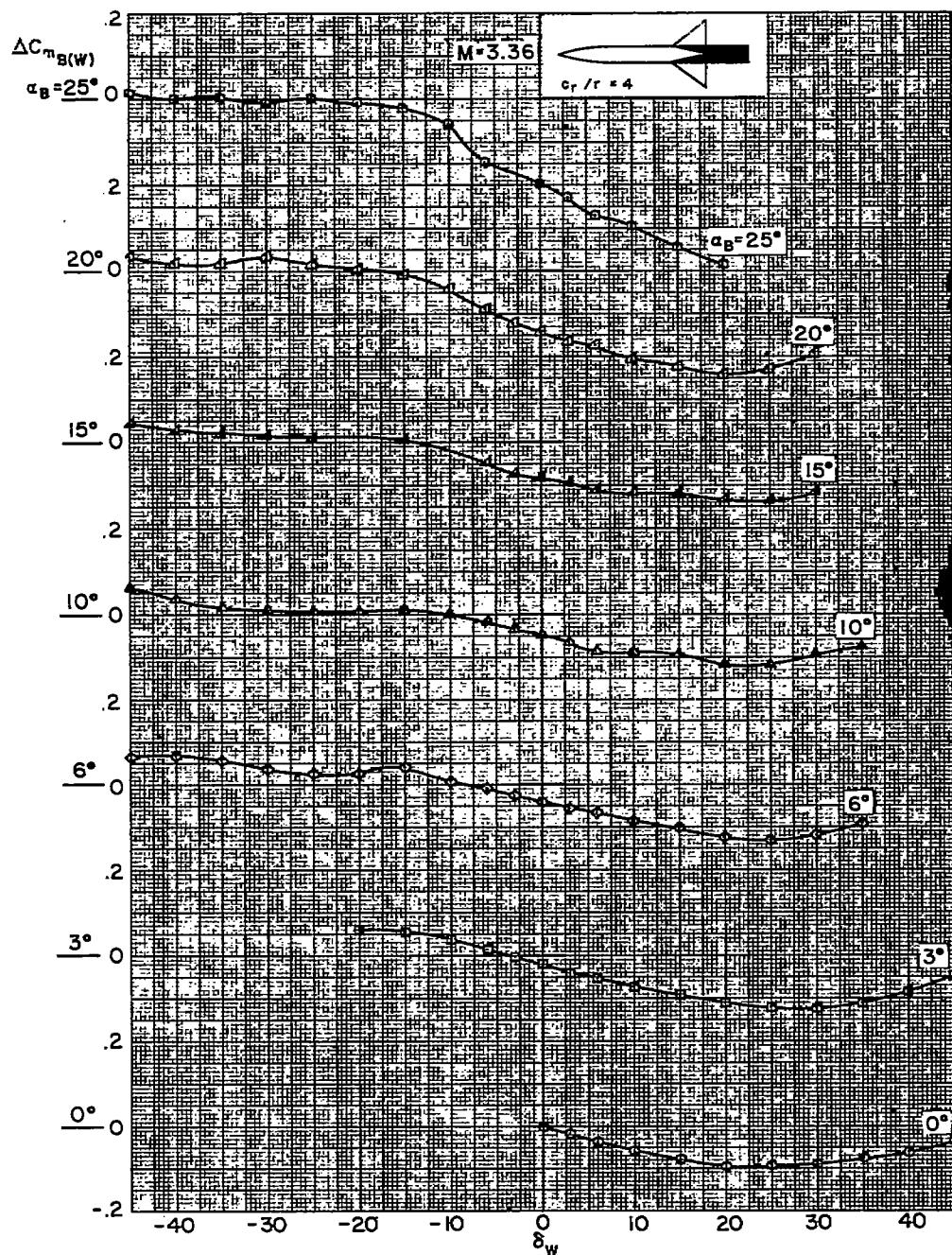
(a) $A = 4$ triangular wing, $r/s = 0.2$.

Figure 9.- Variation with deflection angle of interference pitching-moment coefficient for the body in the presence of the wings.

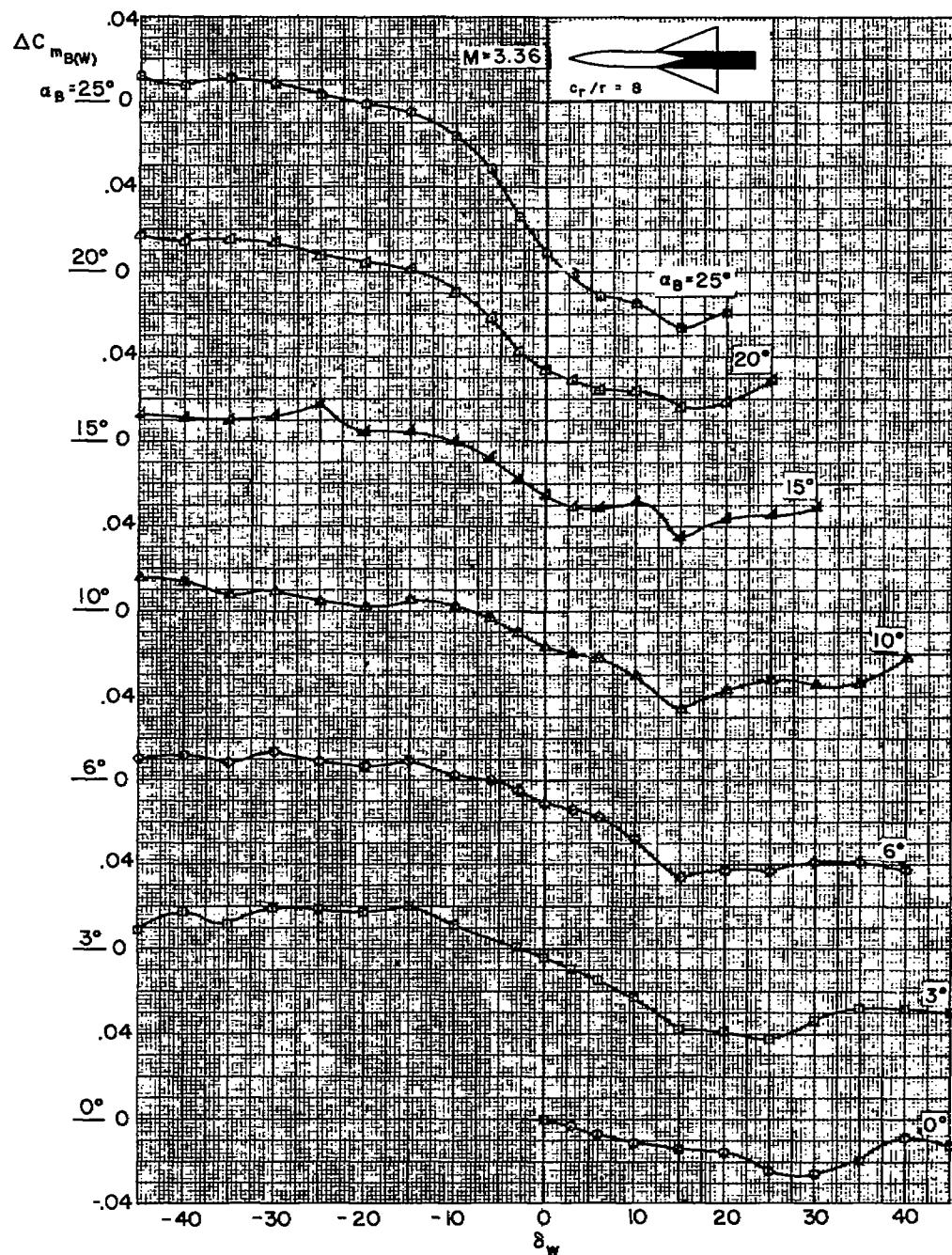
(b) $A = 2$ triangular wing, $r/s = 0.2$.

Figure 9.- Continued.

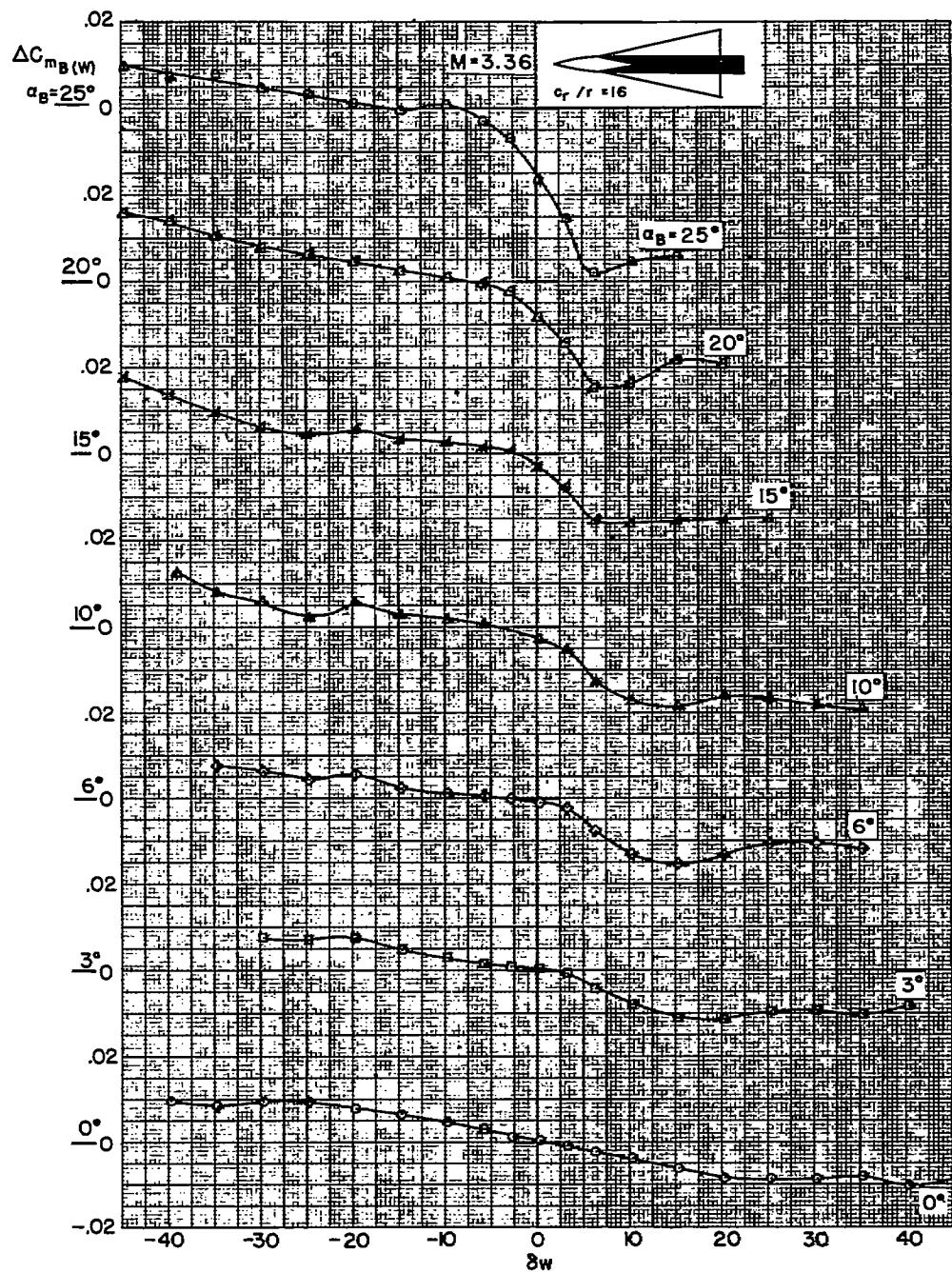
(c) $A = 1$ triangular wing, $r/s = 0.2$.

Figure 9.- Continued.

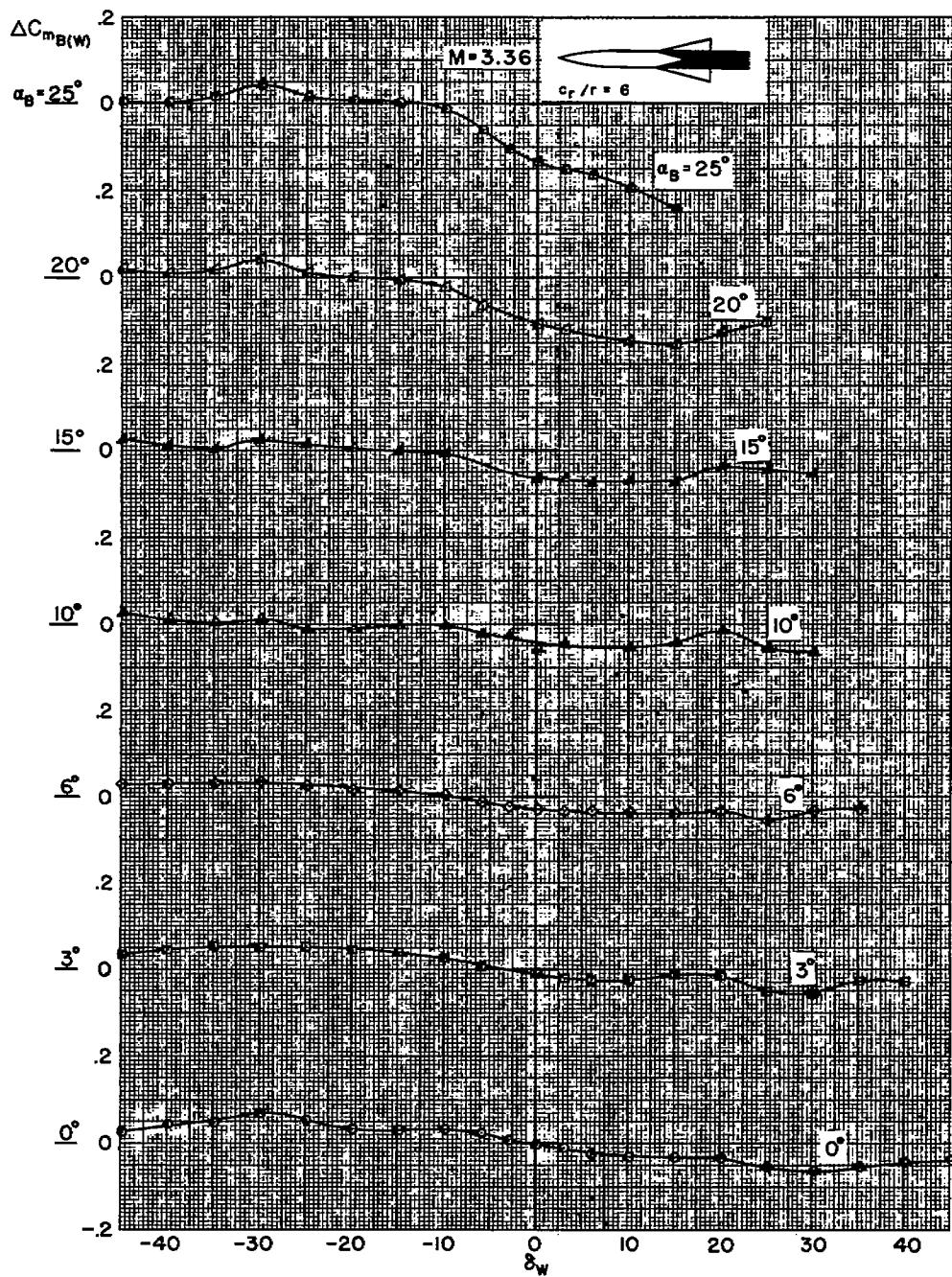
(d) $A = 1$ triangular wing, $r/s = 0.4$.

Figure 9.- Continued.

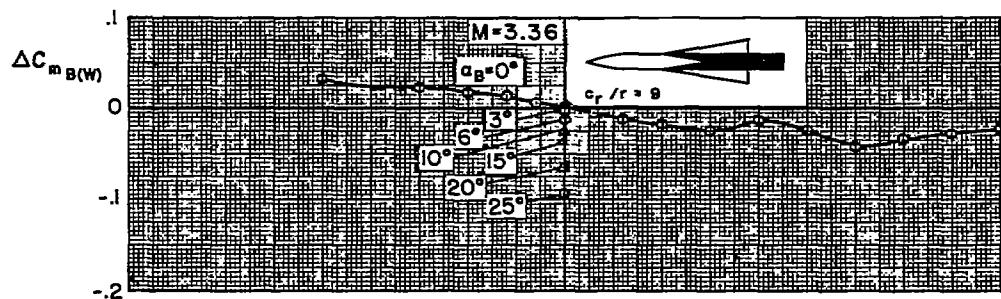
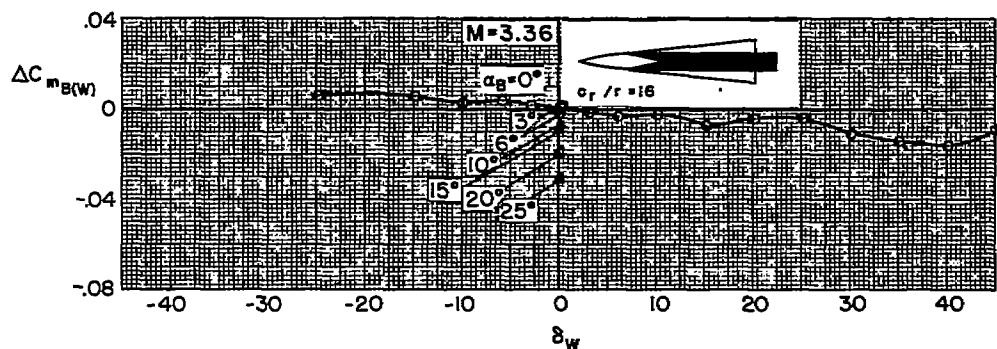
(e) $A = 2/3$ triangular wing, $r/s = 0.4$.(f) $A = 3/8$ triangular wing, $r/s = 0.4$.

Figure 9.- Continued.

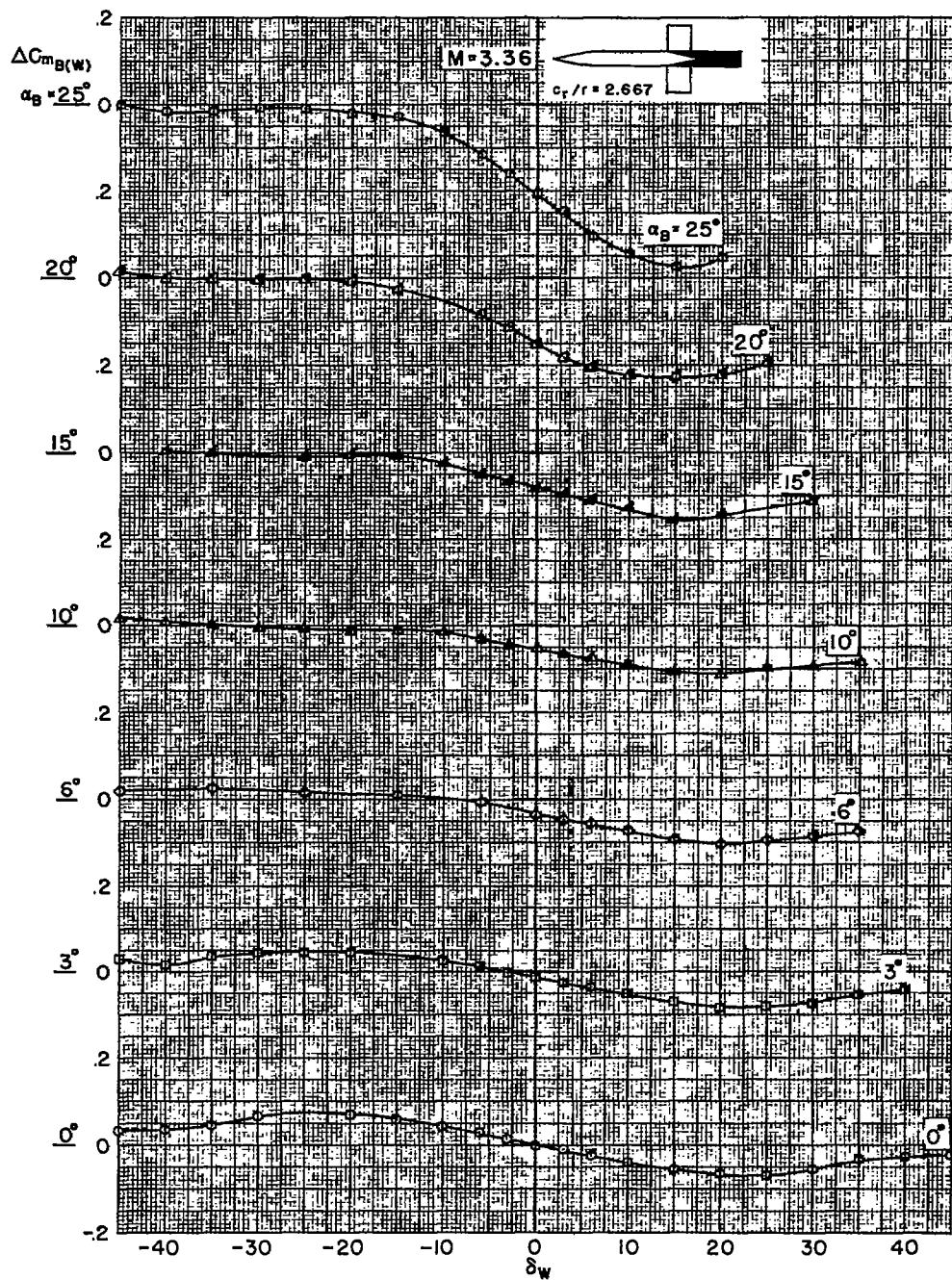
(g) $A = 3$ rectangular wing, $r/s = 0.2$.

Figure 9.- Continued.

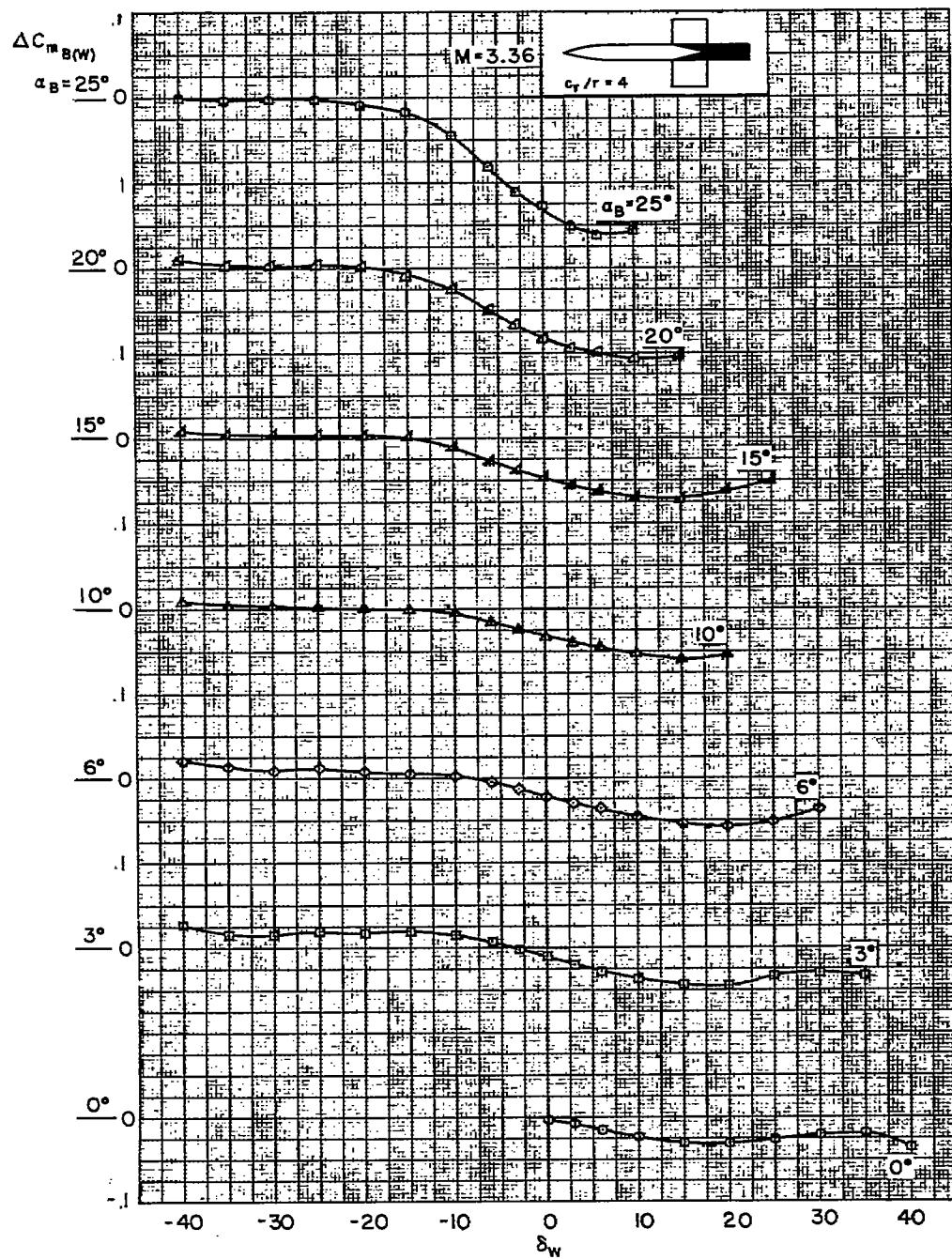
(h) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 9.- Continued.

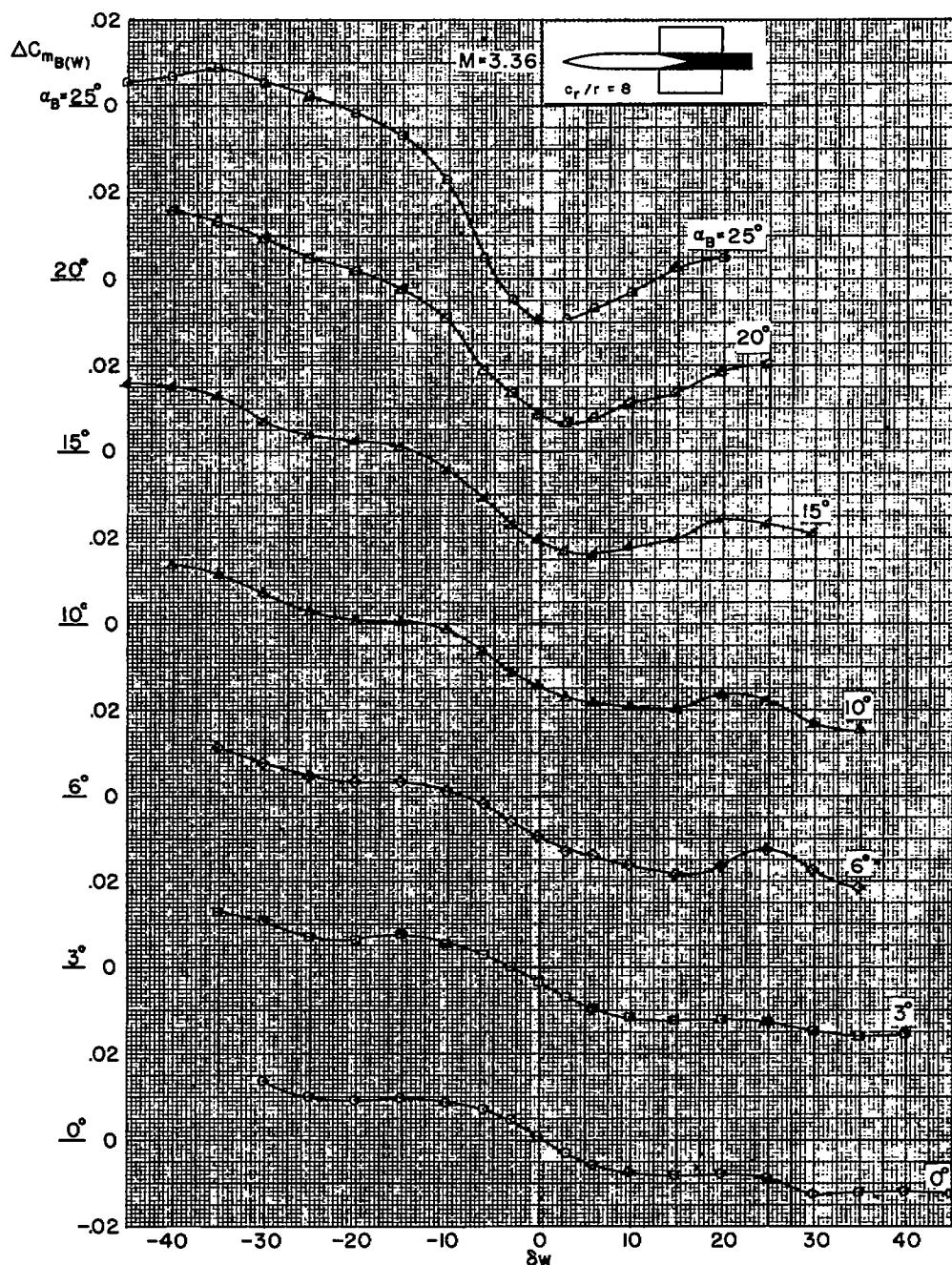
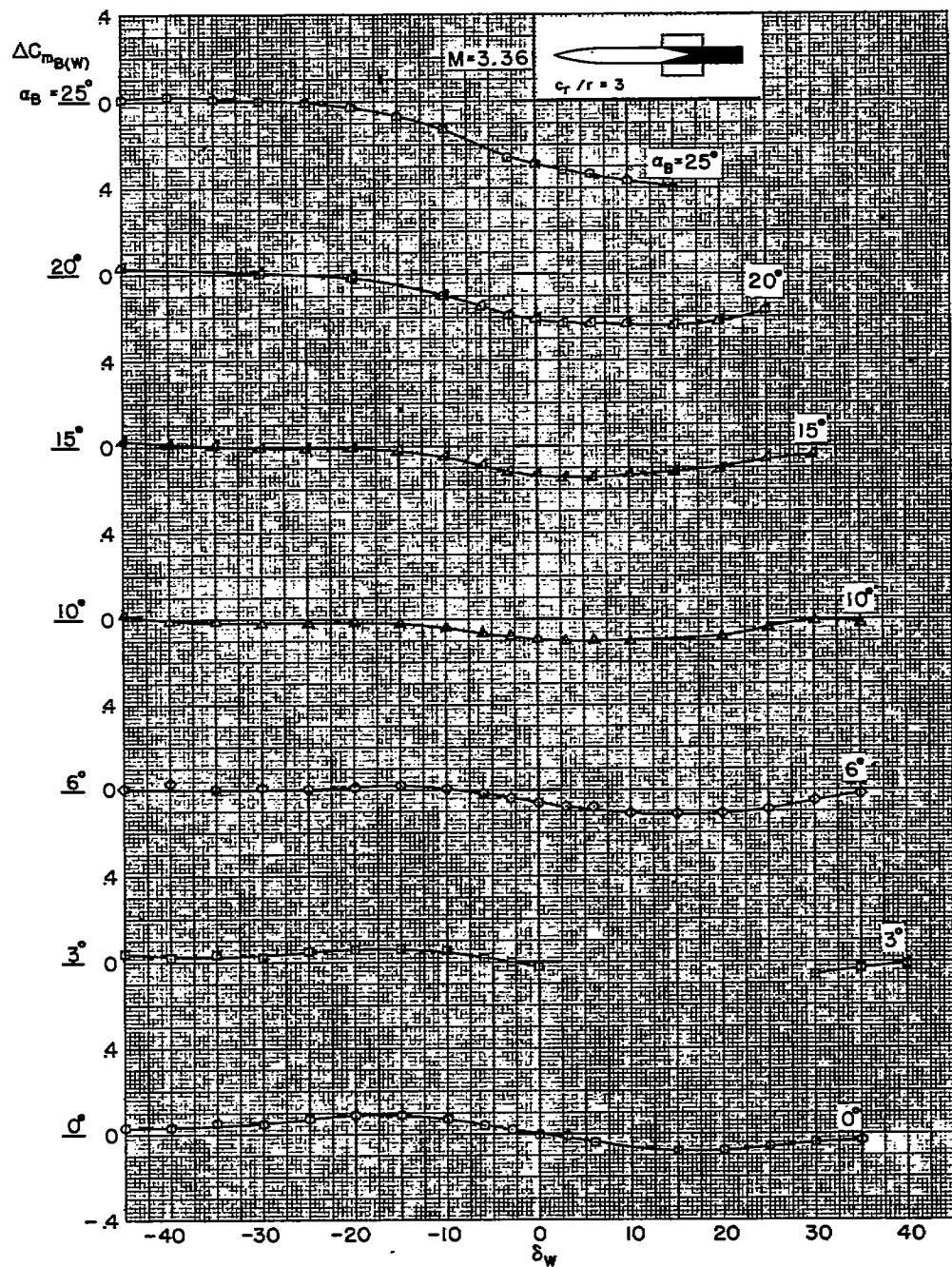
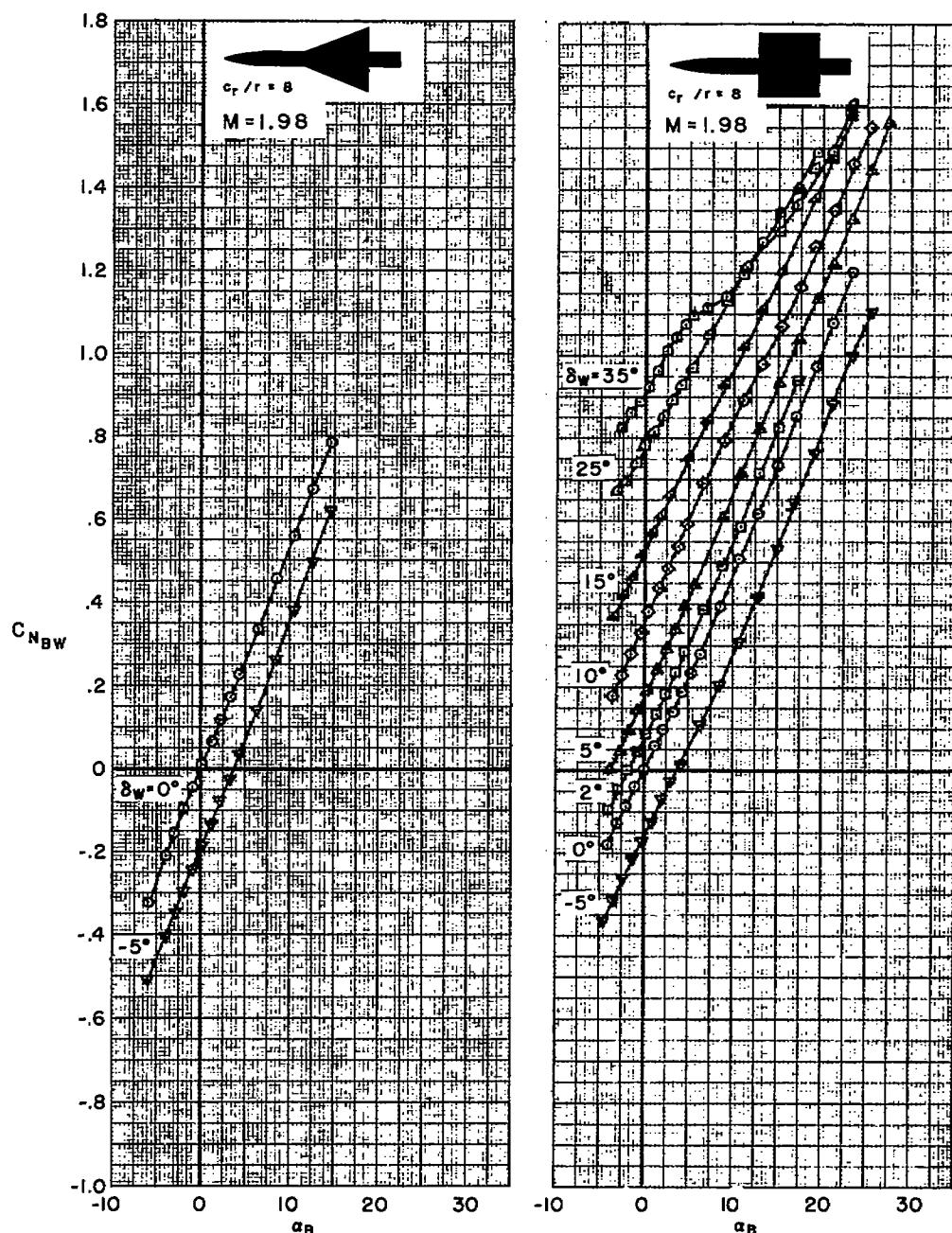
(i) $A = 1$ rectangular wing, $r/s = 0.2$.

Figure 9.- Continued.



(j) $A = 1$ rectangular wing, $r/s = 0.4$.

Figure 9.- Concluded.



(a) $A = 2$ triangular wing and body combination, $r/s = 0.2$. (b) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 10.- Variation with angle of attack of normal-force coefficient for the body-wing combinations.

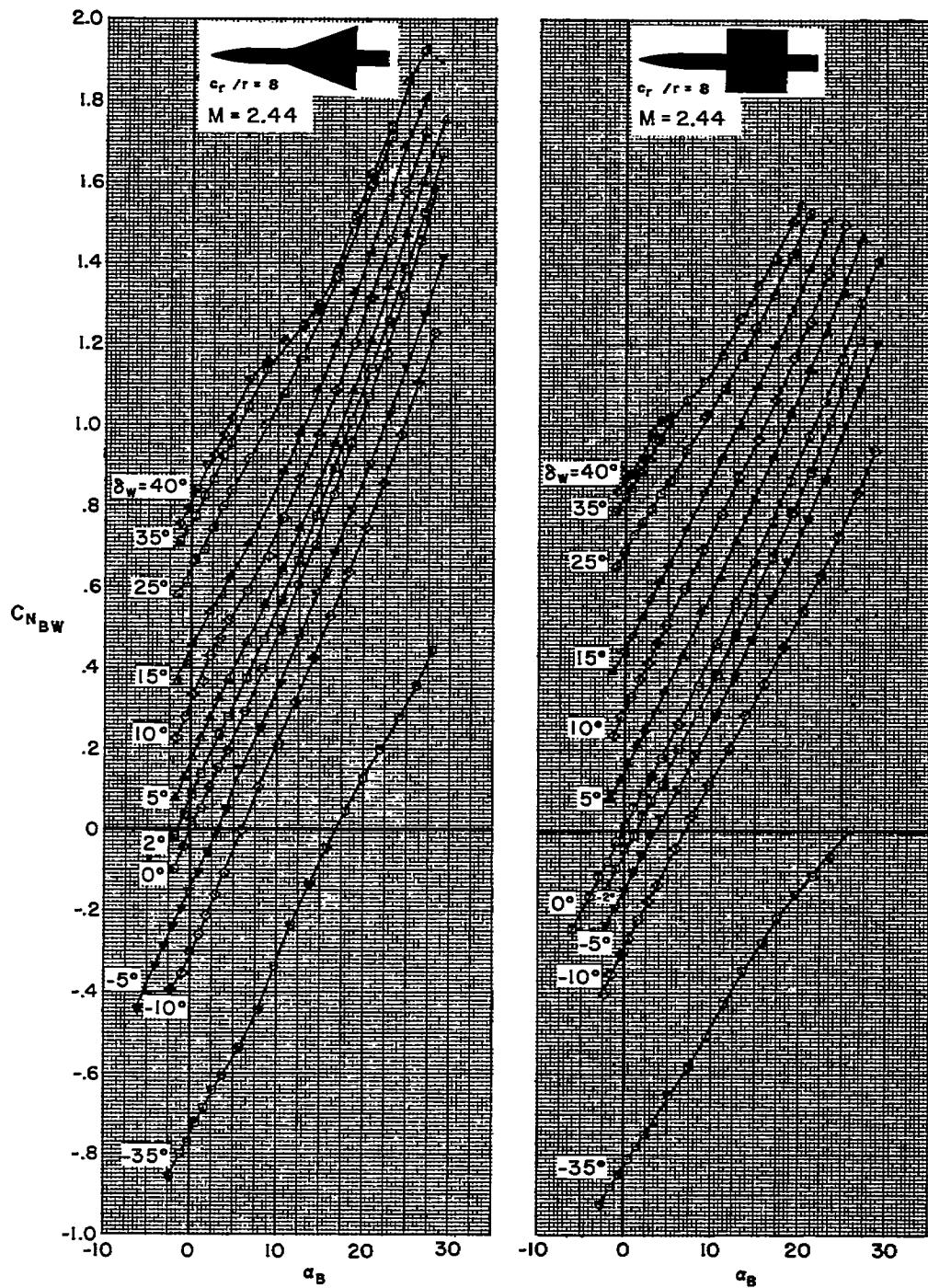
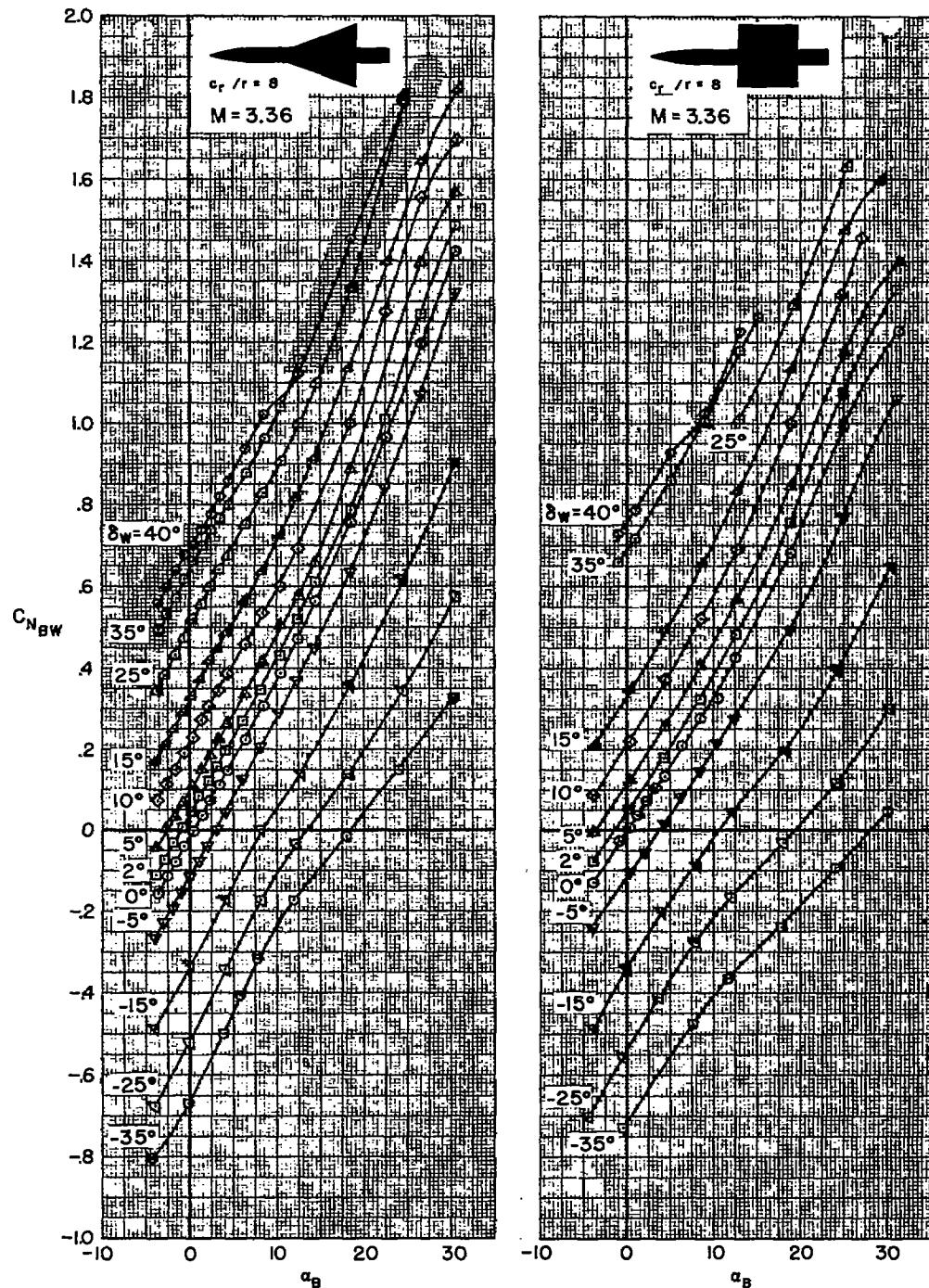
(c) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(d) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 10.- Continued.



(e) $A = 2$ triangular wing and (f) $A = 1$ rectangular wing and
body combination, $r/s = 0.2$. body combination, $r/s = 0.2$.

Figure 10.- Concluded.

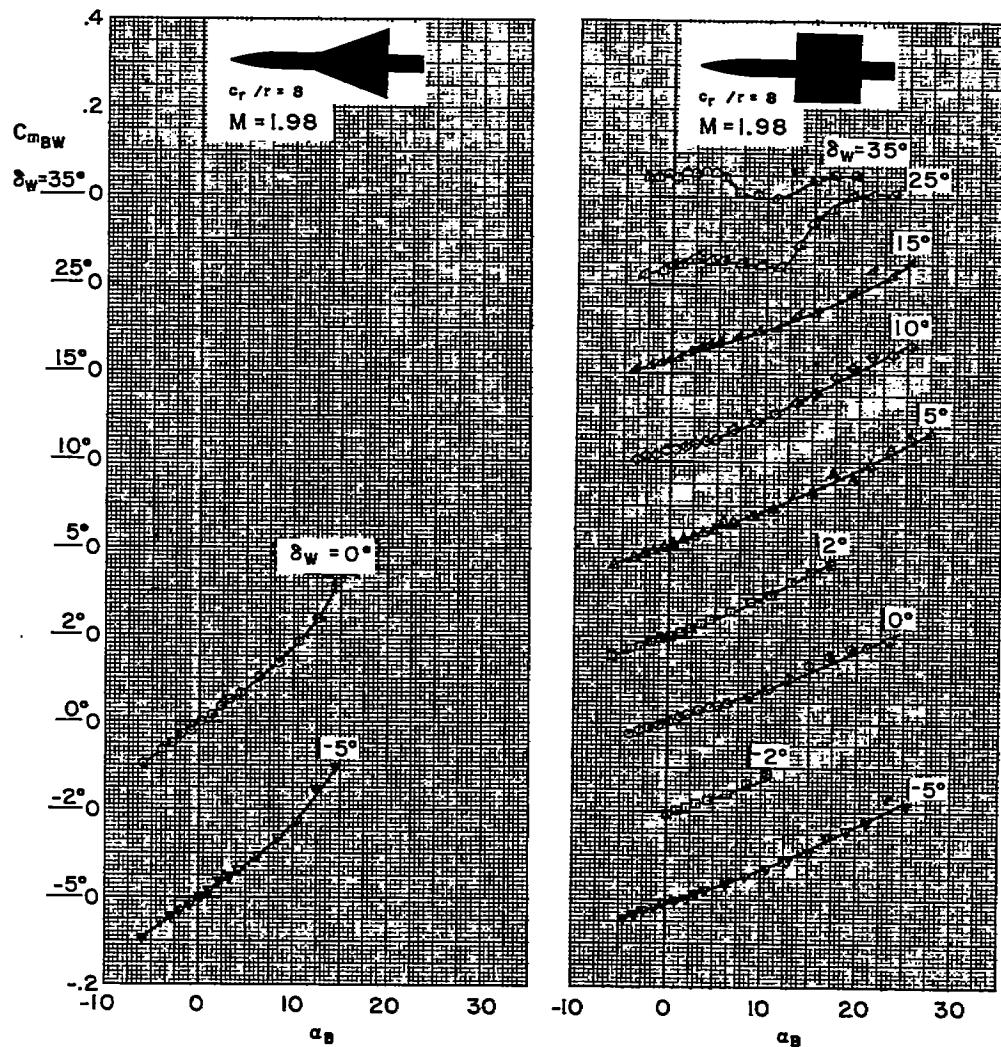


Figure 11.- Variation with angle of attack of pitching-moment coefficient for body-wing combinations.

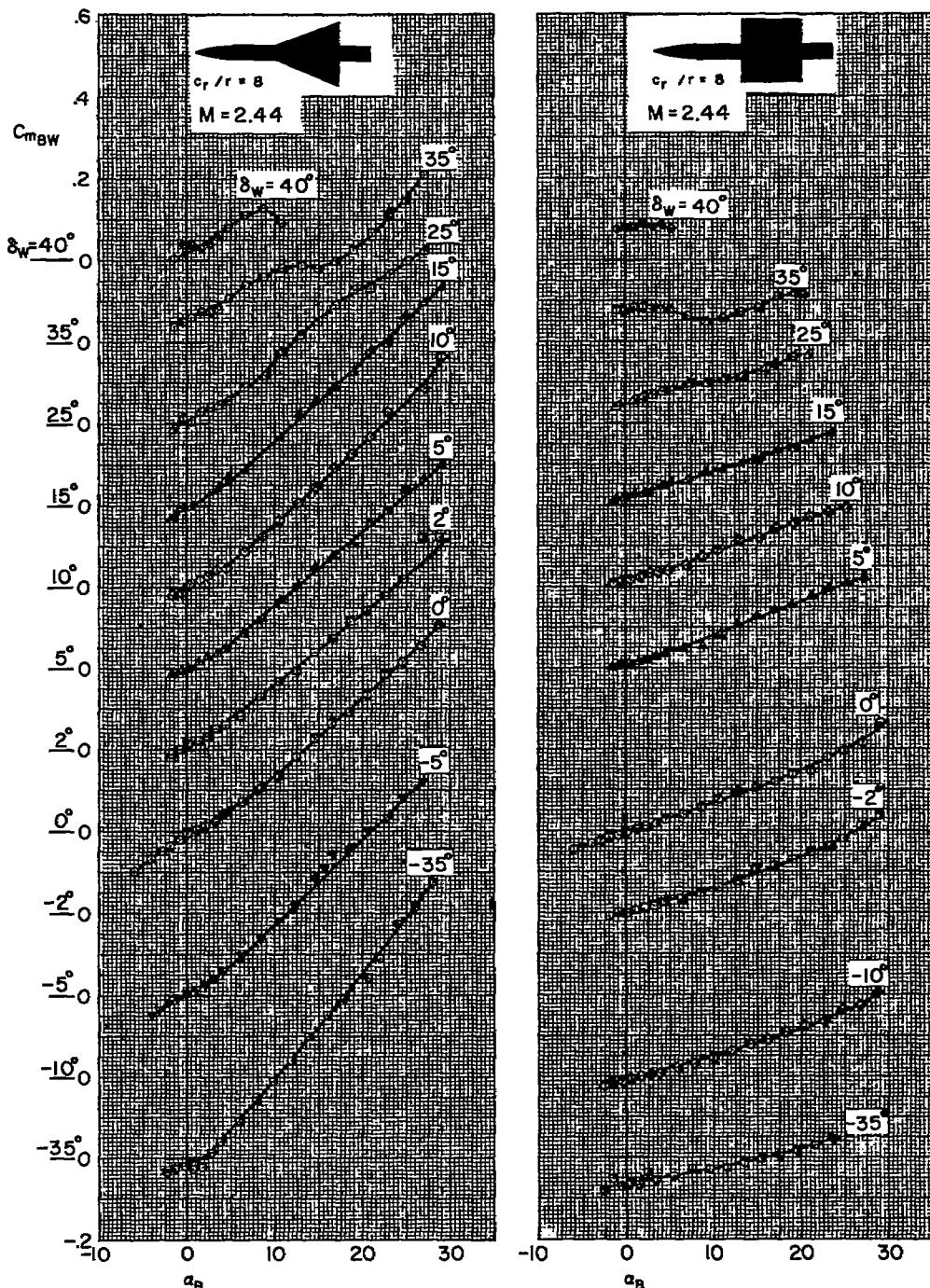
(c) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(d) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 11.- Continued.

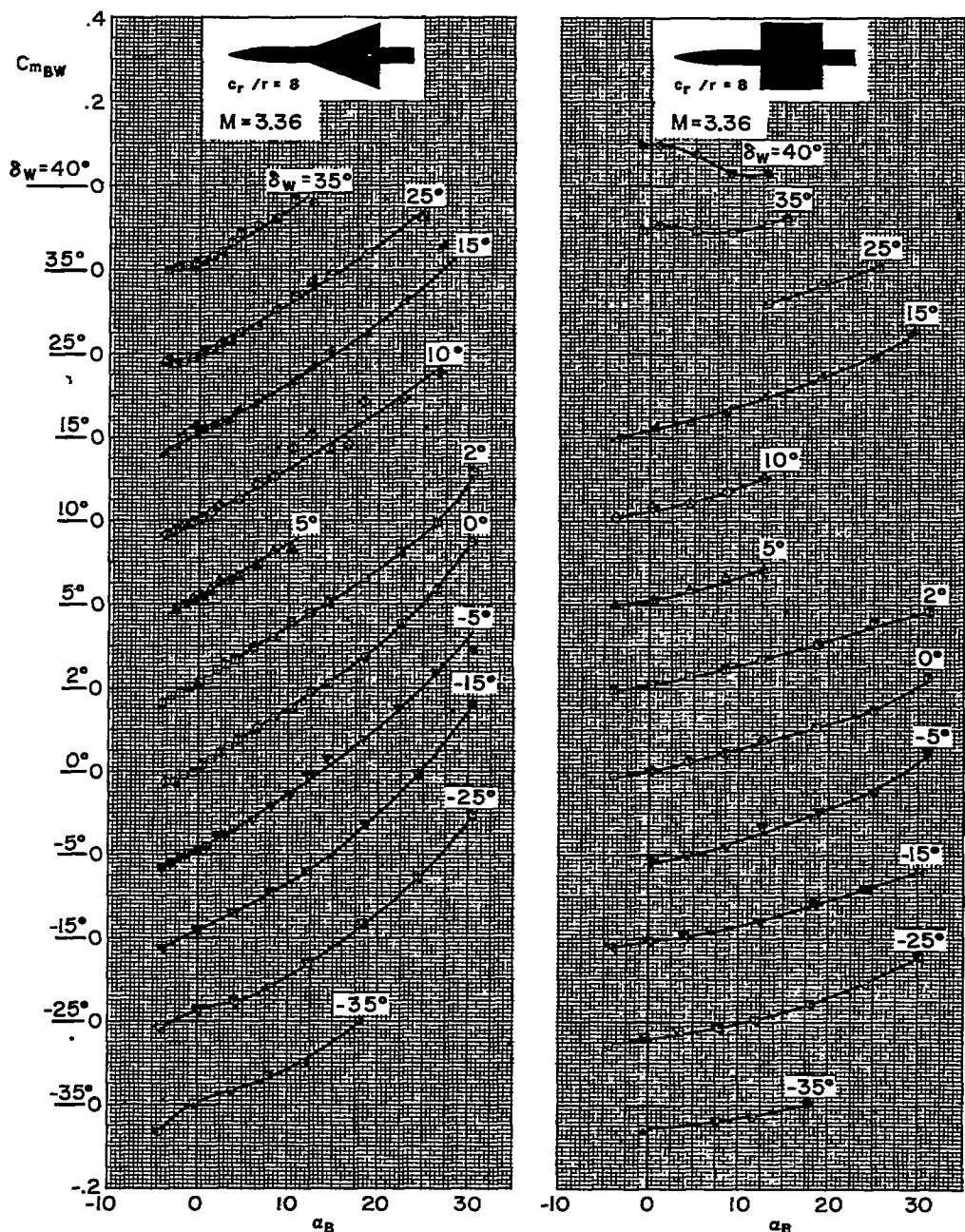
(e) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(f) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 11.- Concluded.

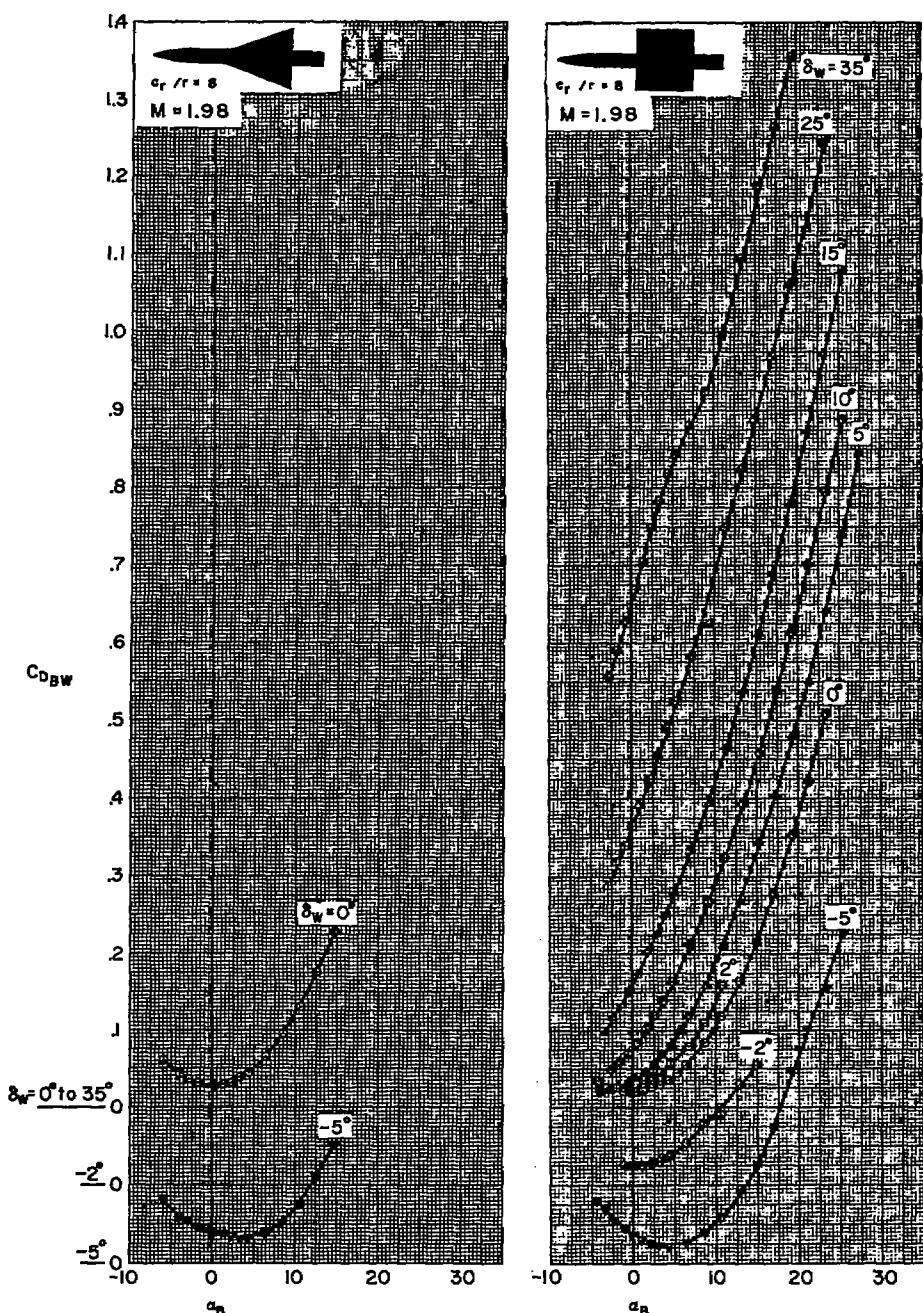


Figure 12.- Variation with angle of attack of drag coefficient for the body-wing combinations.

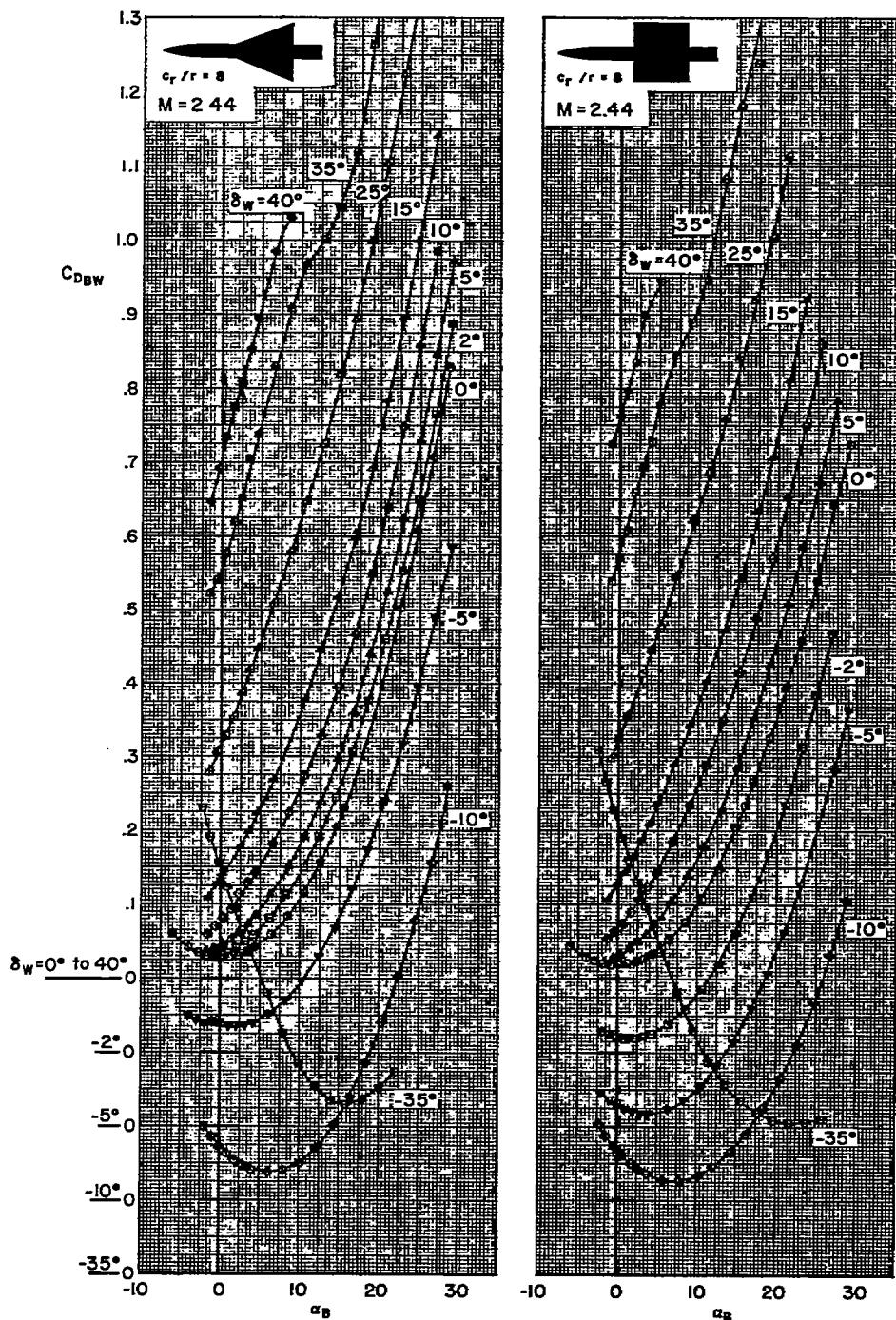
(c) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(d) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 12.- Continued.

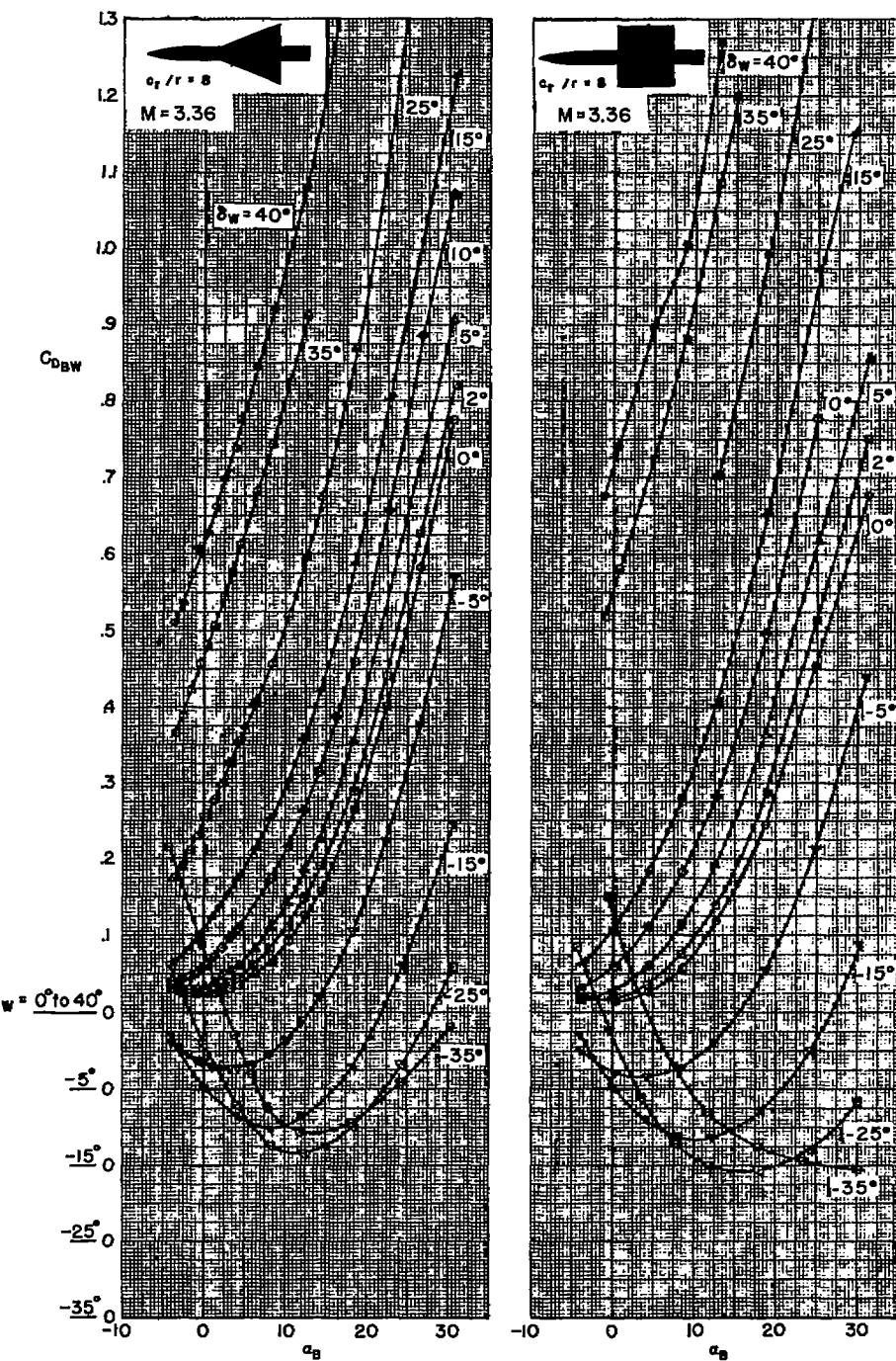
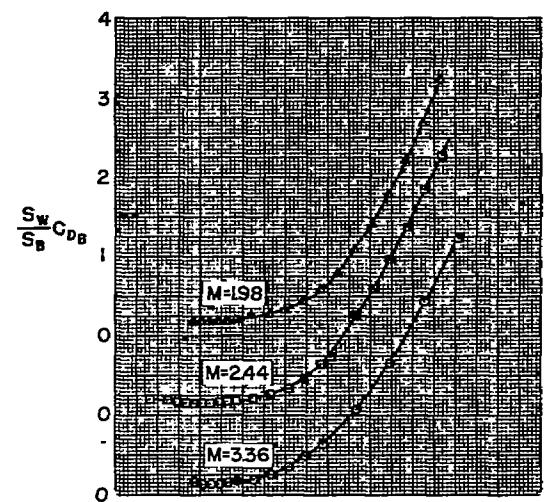
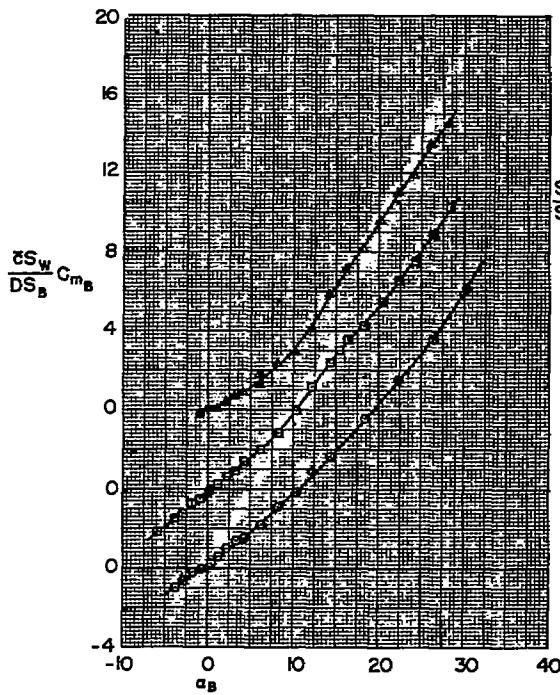
(e) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(f) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

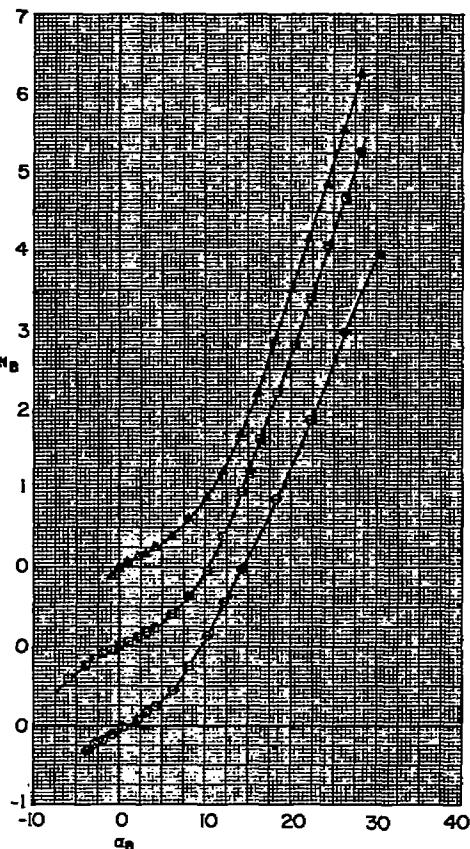
Figure 12.- Concluded.



(a) Drag.

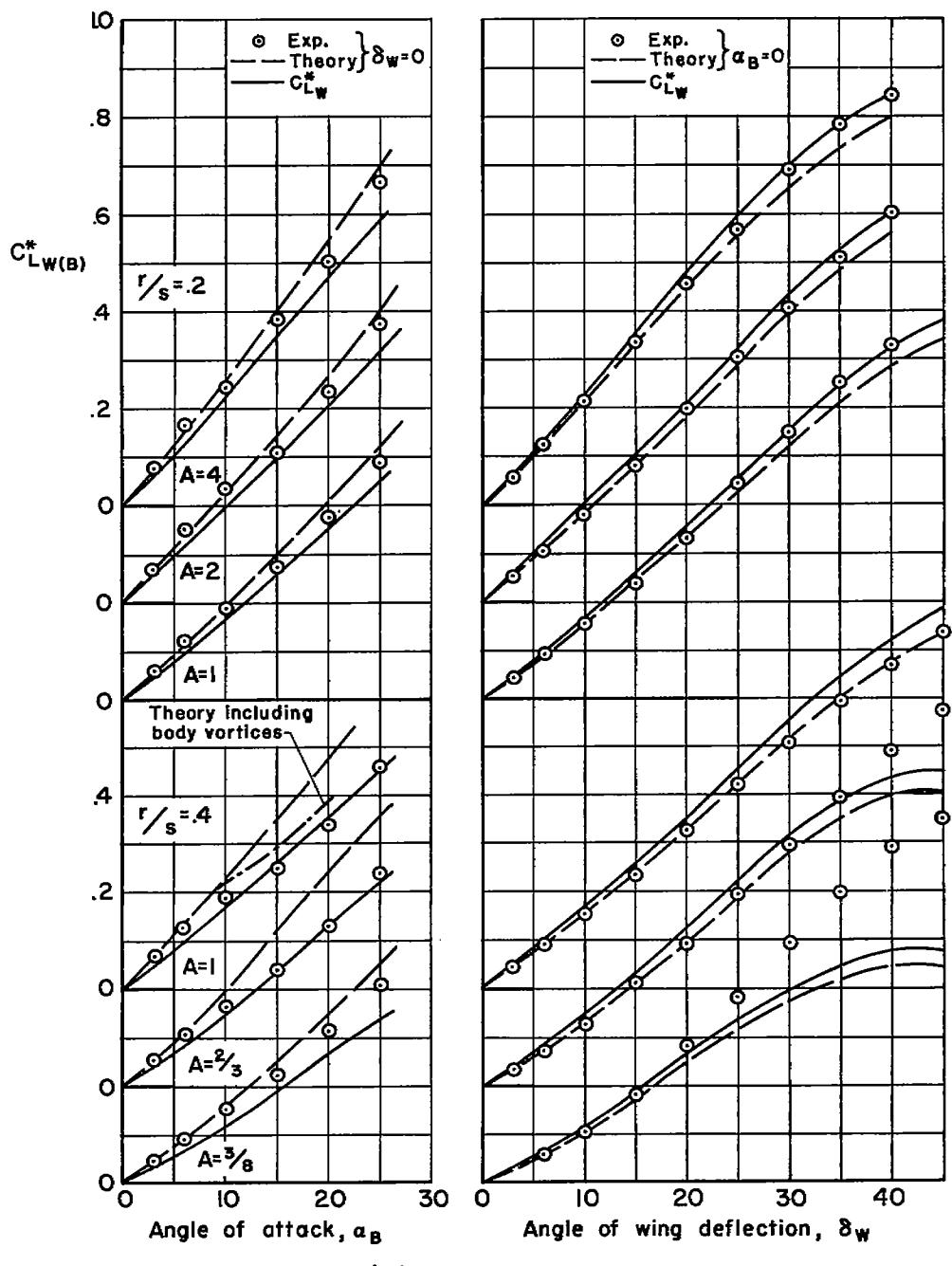


(b) Pitching moment.



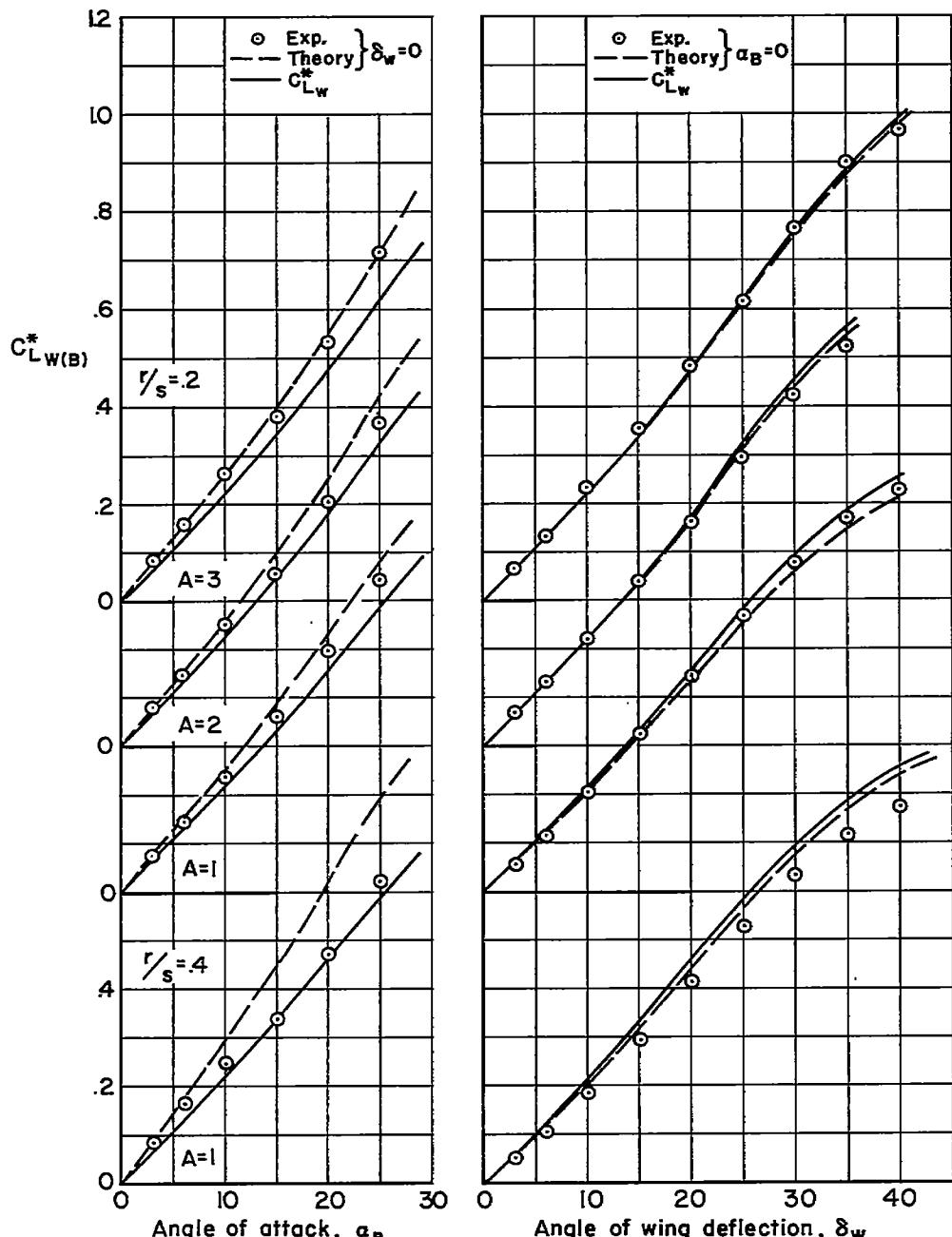
(c) Normal force.

Figure 13.- Variation with angle of attack of drag coefficient, pitching-moment coefficient and normal-force coefficient for the body alone.



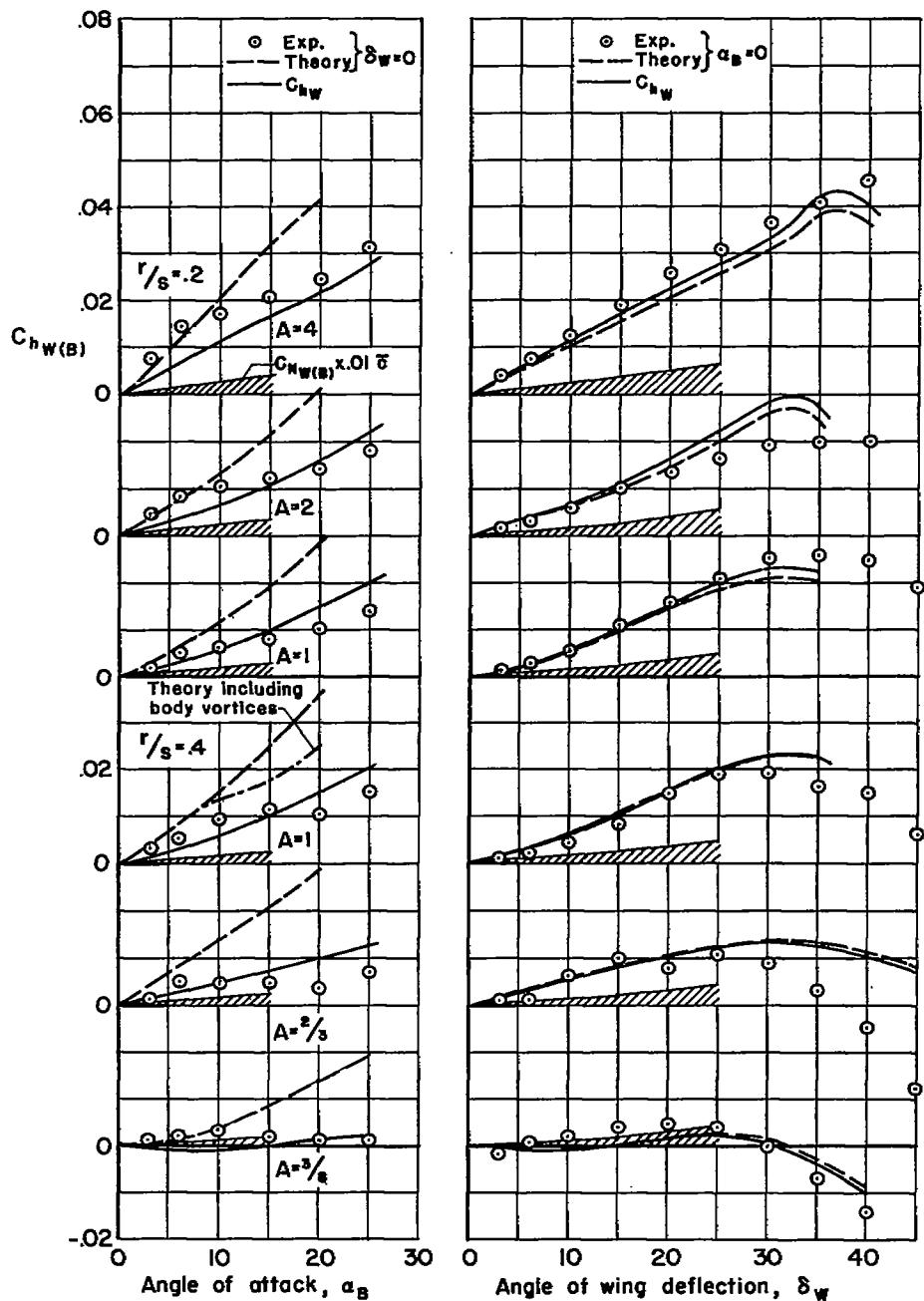
(a) Triangular.

Figure 14.- Comparison of theoretical and experimental lift coefficients for the wings in the presence of the body.



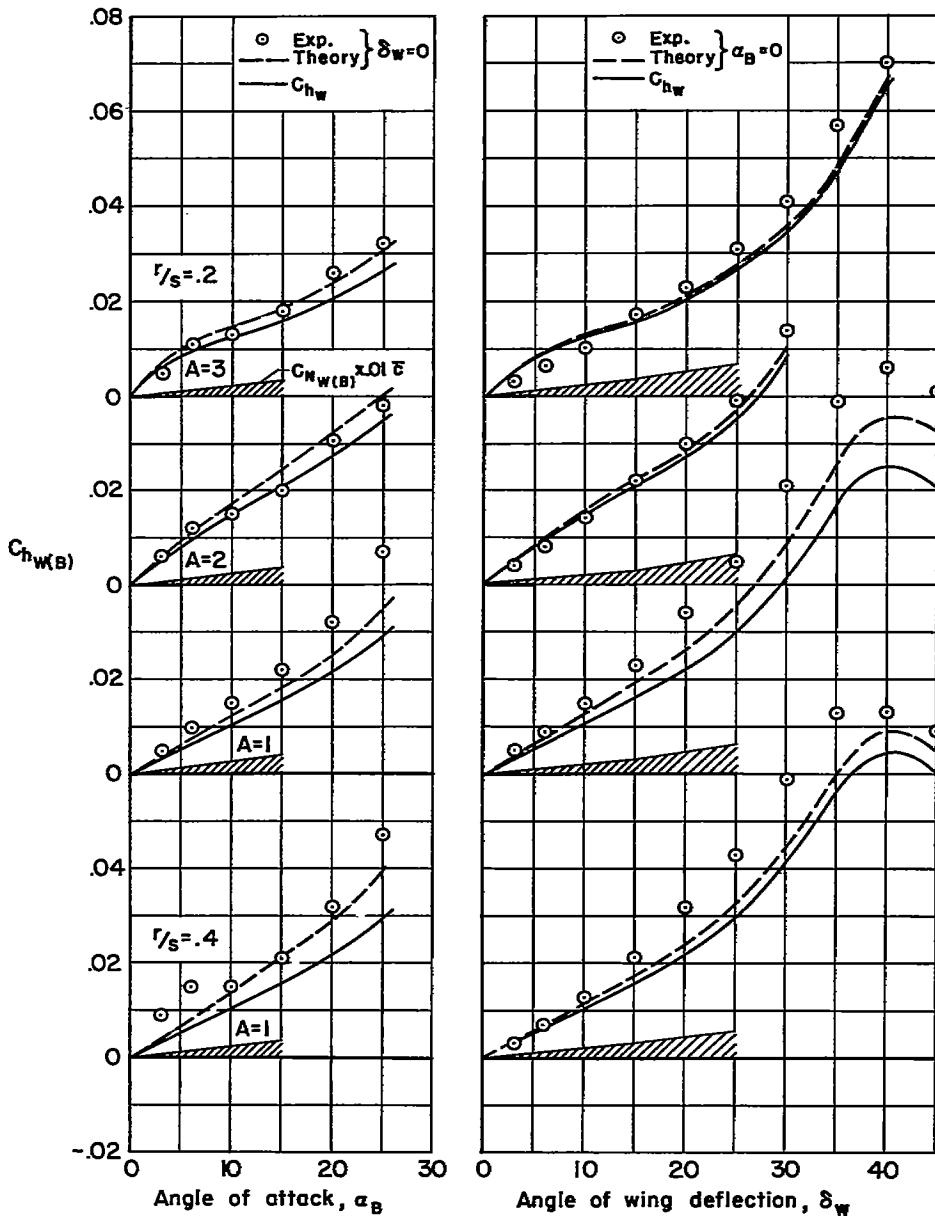
(b) Rectangular.

Figure 14.- Concluded.



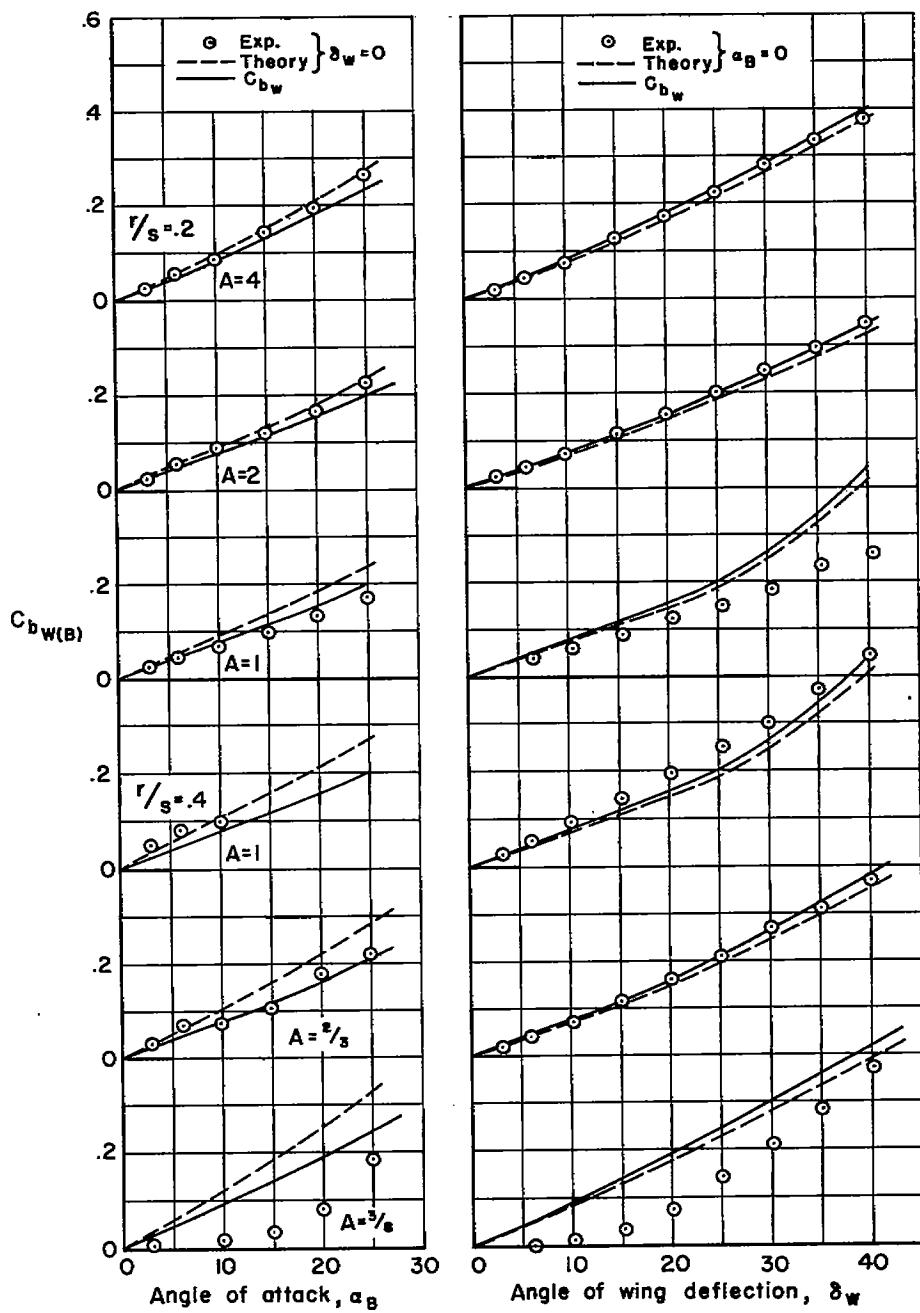
(a) Triangular.

Figure 15.- Comparison of theoretical and experimental hinge-moment coefficients for the wings in the presence of the body.



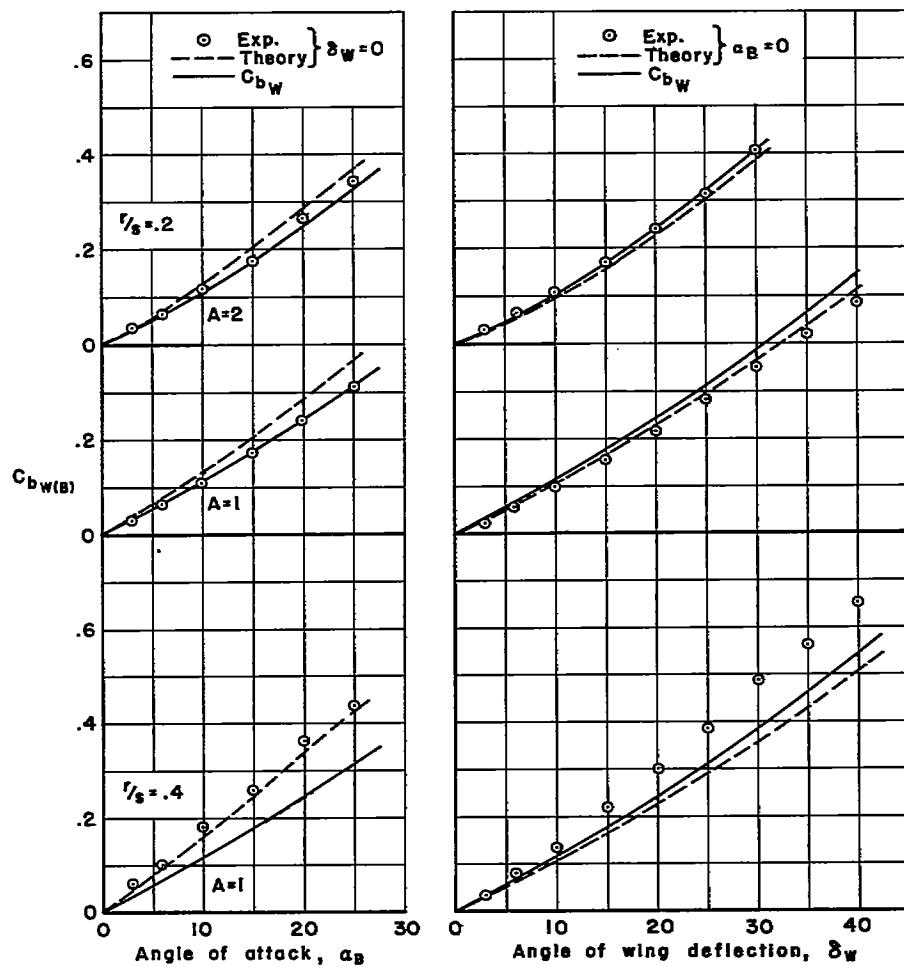
(b) Rectangular.

Figure 15.- Concluded.



(a) Triangular.

Figure 16.- Comparison of theoretical and experimental bending-moment coefficients for the wings in the presence of the body.



(b) Rectangular.

Figure 16.- Concluded.

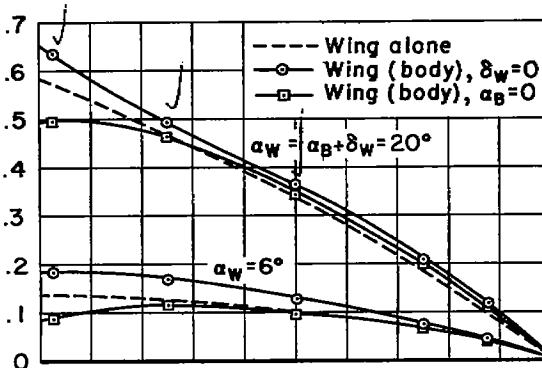
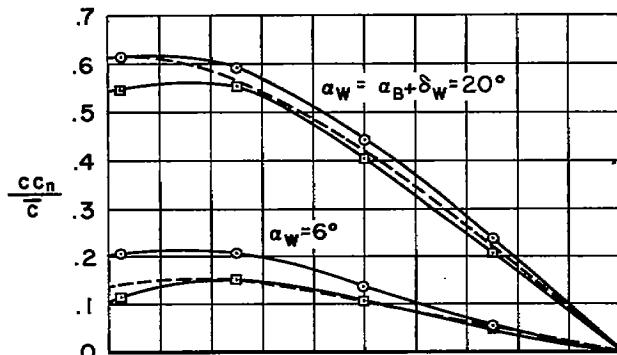
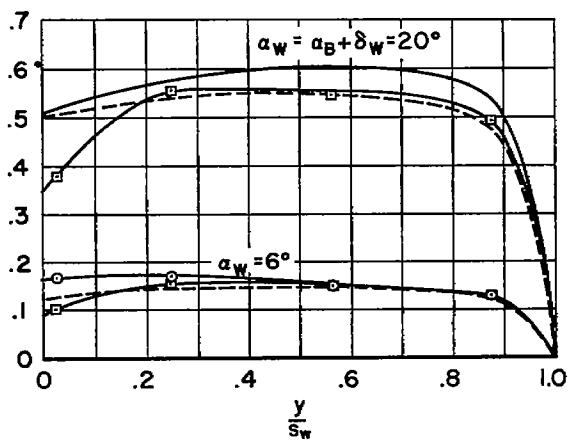
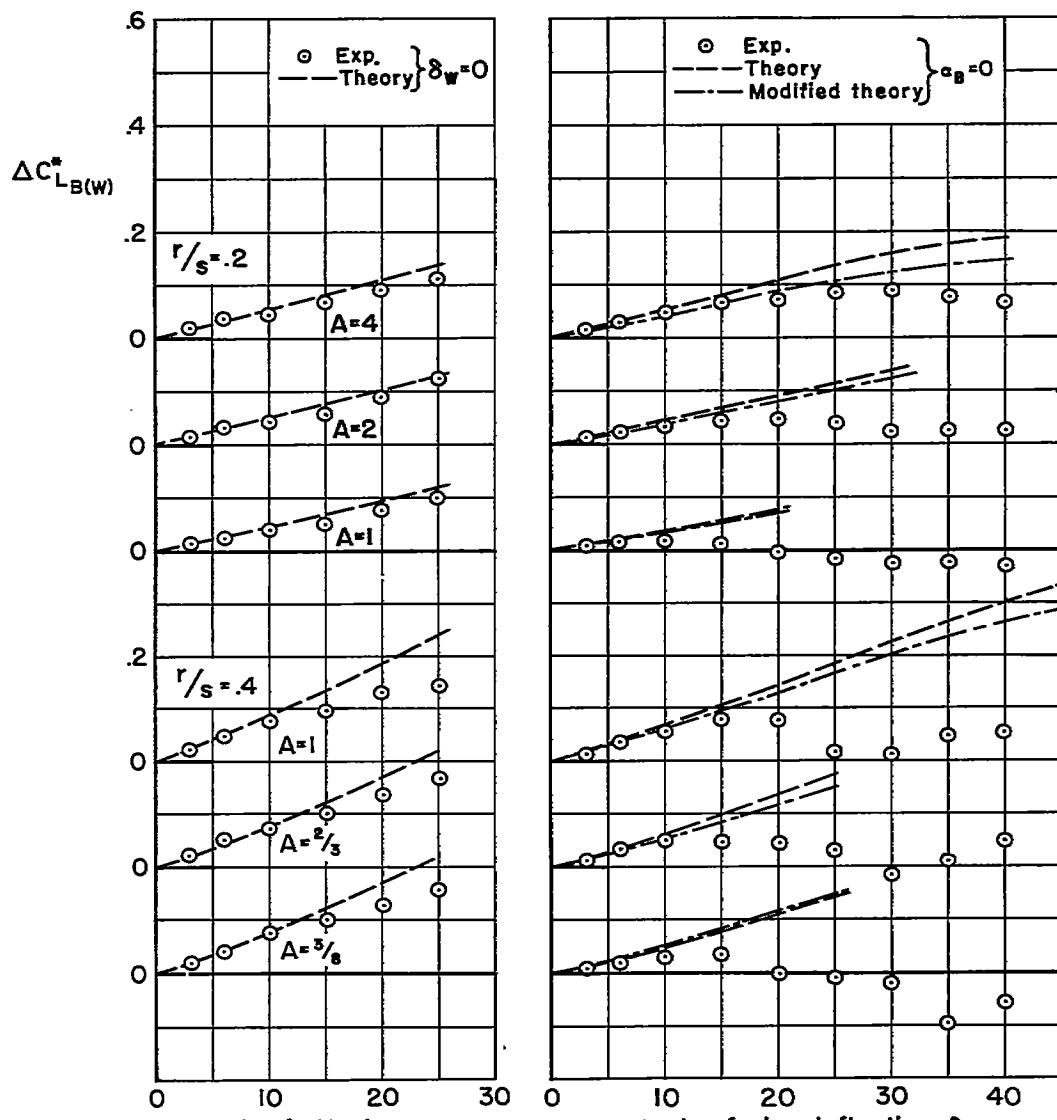
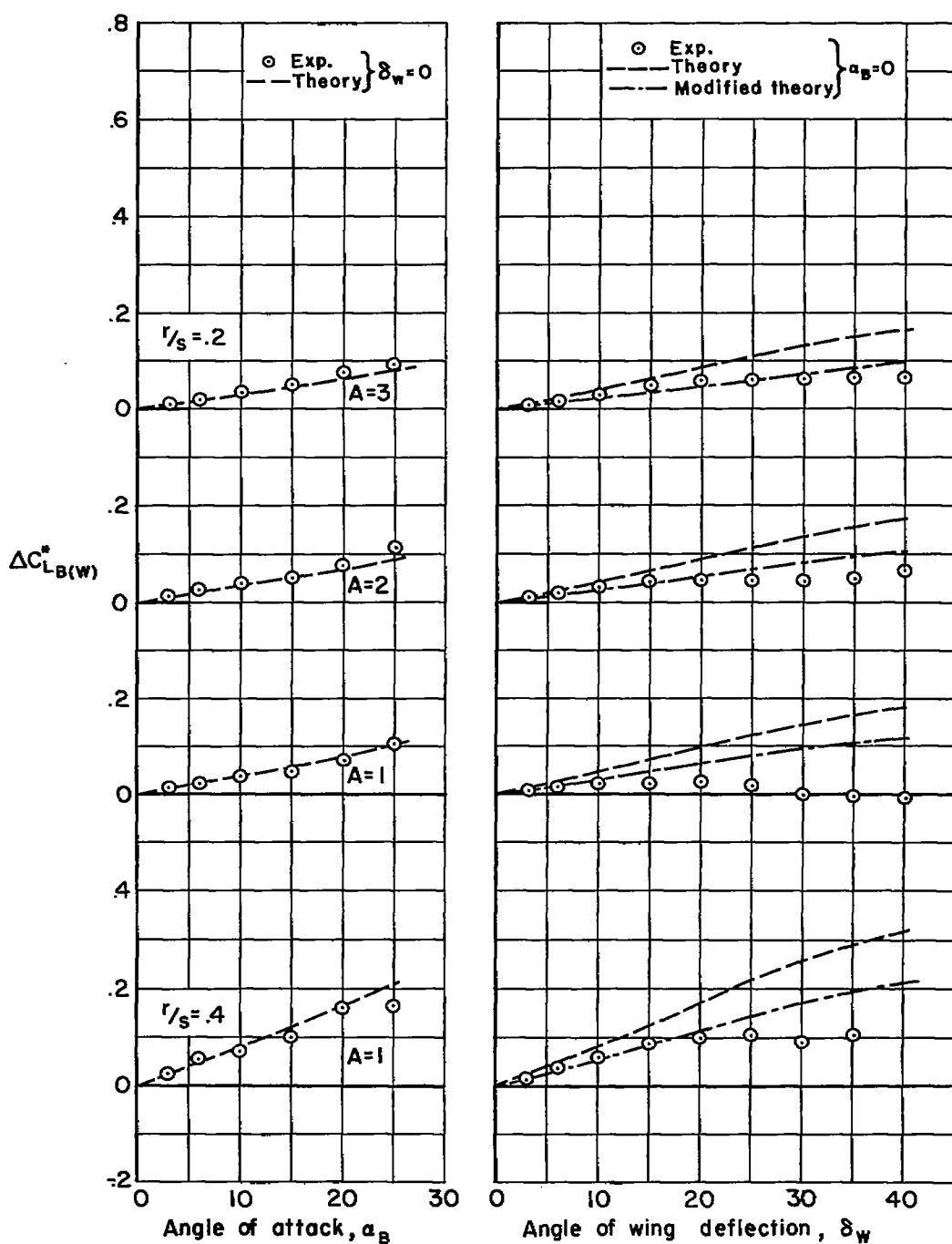
(a) $A = 2$ triangular wing, $r/s = 0.2$.(b) $A = 4$ triangular wing, $r/s = 0.2$.(c) $A = 2$ rectangular wing, $r/s = 0.2$.

Figure 17.- Comparison of span-loading coefficients for the wings in the presence of the body and for the wings alone.



(a) Triangular

Figure 18.- Comparison of theoretical and experimental interference lift coefficients for the body in the presence of the wings.



(b) Rectangular.

Figure 18.- Concluded.

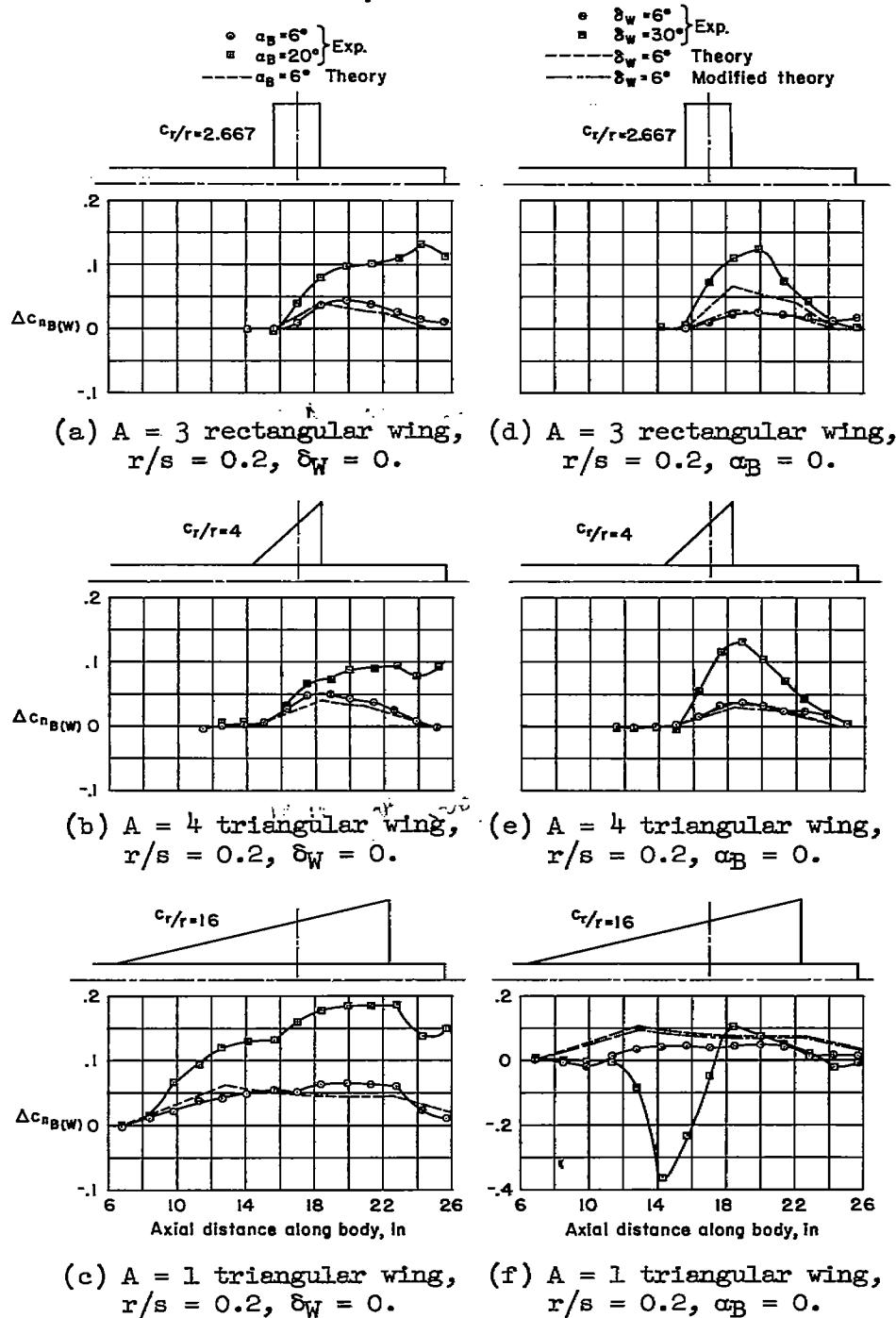
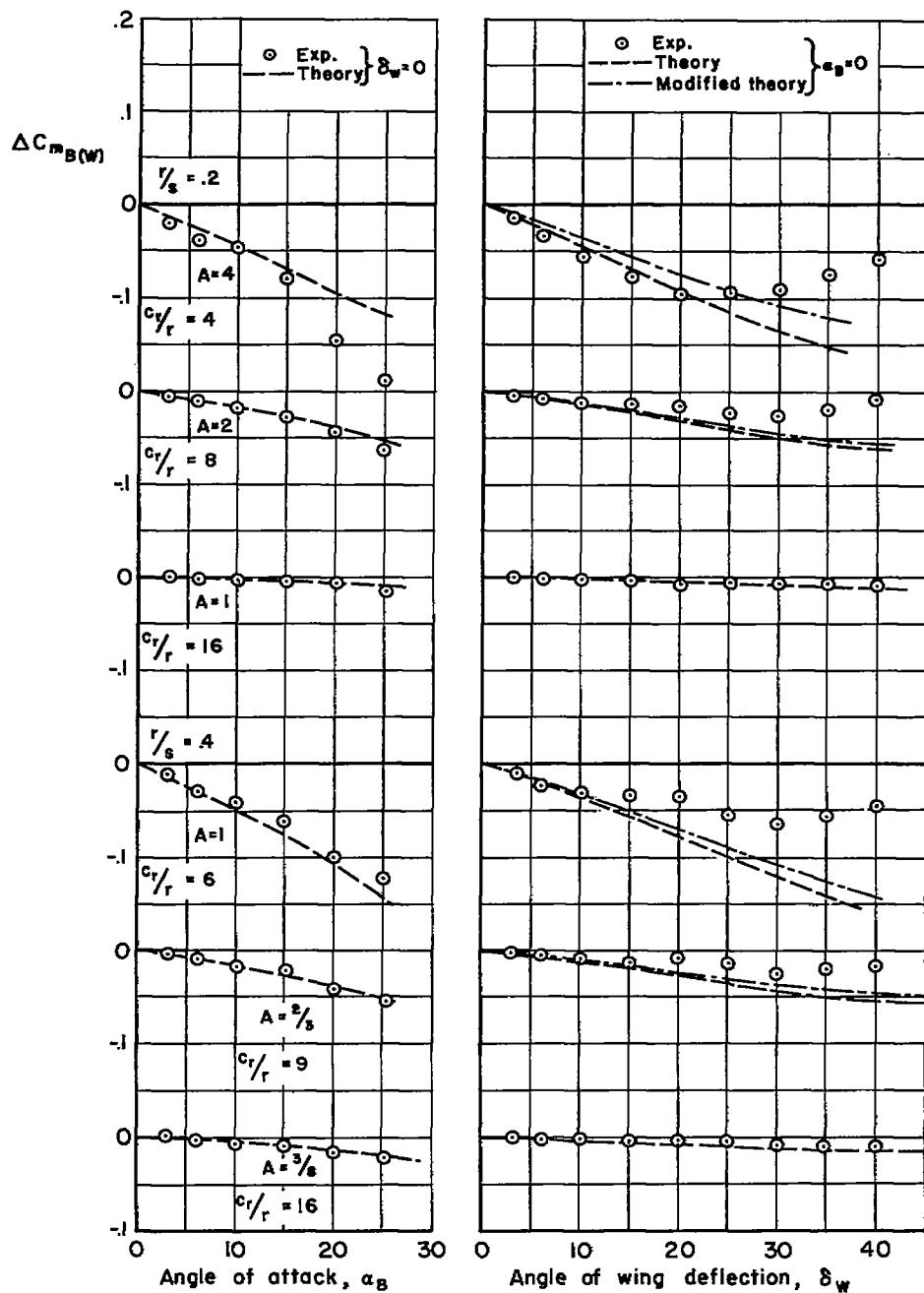
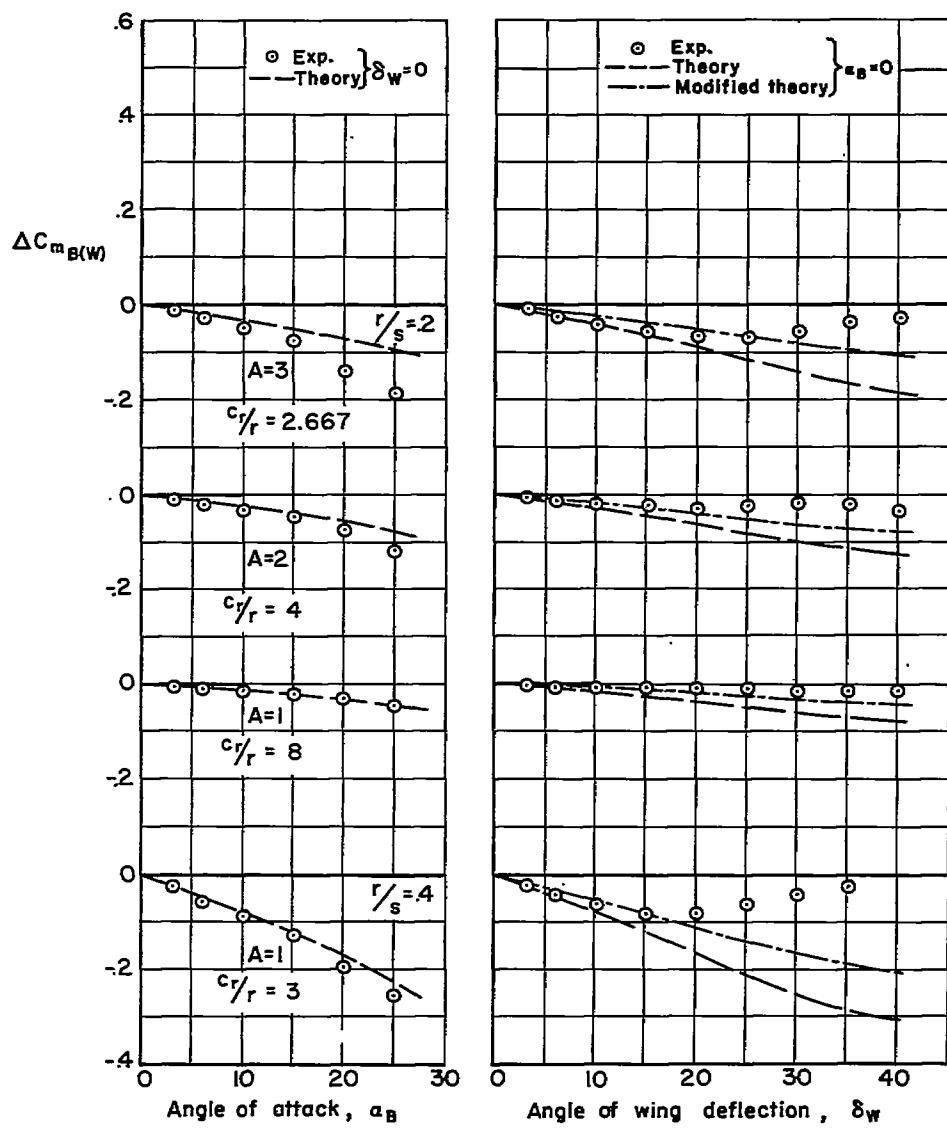


Figure 19.- Comparison of theoretical and experimental longitudinal interference loading coefficients of the body in the presence of the wings.



(a) Triangular.

Figure 20.- Comparison of theoretical and experimental interference pitching-moment coefficients for the body in the presence of the wings.



(b) Rectangular.

Figure 20.- Concluded.

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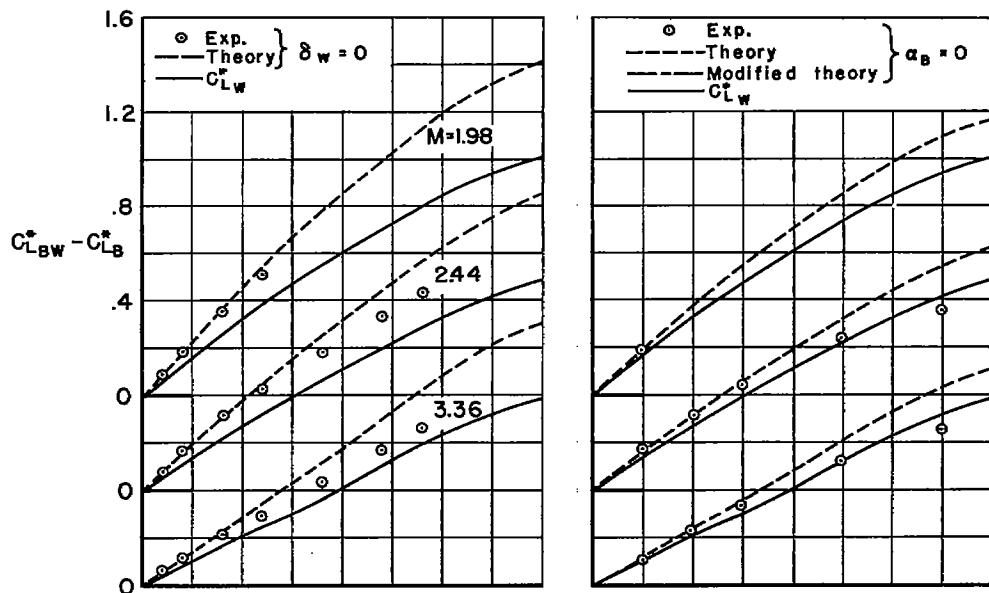
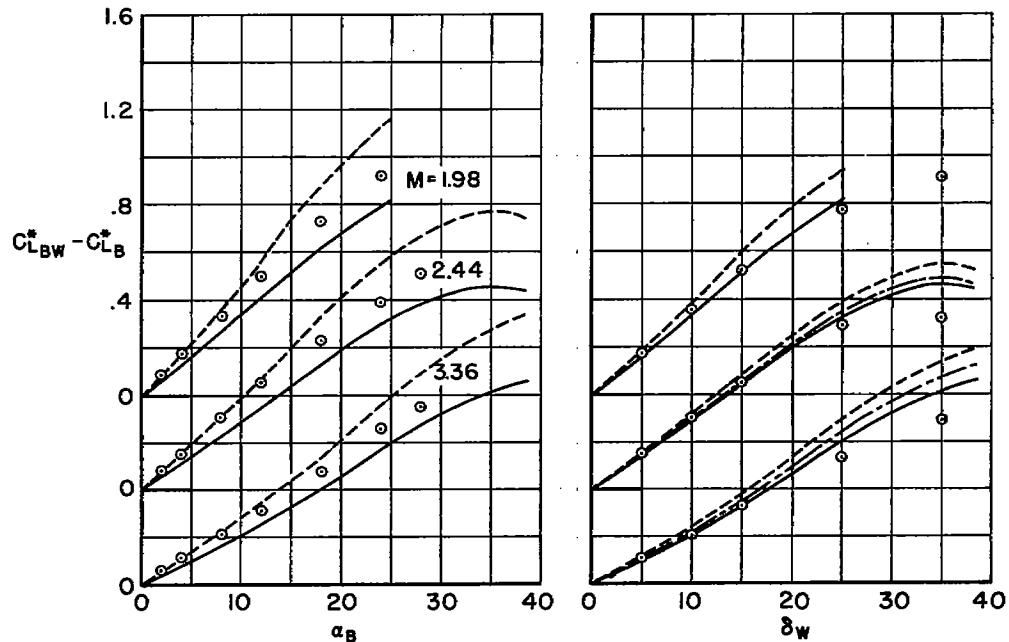
(a) $A = 2$ triangular wing and body combination, $r/s = 0.2$.(b) $A = 1$ rectangular wing and body combination, $r/s = 0.2$.

Figure 21.- Comparison of theoretical and experimental combined lift coefficients of two body-wing combinations.

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